

Independence at Dixon Dixon, CA Traffic Impact Analysis



Draft Report

Prepared For:

Lewis Management Corp.

July 2023

Prepared By:



WOOD RODGERS
BUILDING RELATIONSHIPS ONE PROJECT AT A TIME

**Independence at Dixon
Dixon, CA**

TRAFFIC IMPACT ANALYSIS

DRAFT REPORT

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July 2023

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EXECUTIVE SUMMARY

PROJECT DESCRIPTION

The proposed Project site is located on one (1) vacant parcel totaling 10.98 acres within the southwest corner of the intersection of State Route (SR) 113 and North Lincoln Street/Vaughn Road. The Project would gain access to the existing roadway network via one new residential driveway connection on North Lincoln Street and one new residential driveway connection on SR 113. The Project would develop 186 duplex/duet-style residential dwelling units.

INTERSECTION ADVERSE EFFECTS AND IMPROVEMENTS

The intersection of SR 113 & I-80 Ramps/Auction Lane is projected to operate at unacceptable LOS E under Existing PM peak hour conditions and Near-Term Plus Project AM peak hour conditions, and LOS F under Near-Term and Near-Term Plus Project PM peak hour conditions. However, this intersection is not projected to meet peak hour signal warrants under any study scenarios. Therefore, there would not be a significant adverse effect at the SR 113 & I-80 Ramps/Auction Lane intersection.

The remaining study intersections are projected to operate at acceptable LOS (LOS "D" or better) under all scenarios analyzed.

QUEUING ANALYSIS AND IMPROVEMENTS

The following queues are projected to exceed storage length:

SR 113 & North Lincoln Street/Vaughn Road:

- SBT – Near-Term Plus Project PM peak hour
- EBL – Near-Term PM peak hour, Near-Term Plus Project AM and PM peak hour

SR 113 & Regency Parkway/Industrial Way:

- NBT – Existing, Near-Term, and Near-Term Plus Project AM and PM peak hour
- SBT – Near-Term Plus Project PM peak hour

It is recommended to adjust the signal timings to provide additional green time at SR 113 & North Lincoln Street/Vaughn Road intersection for the eastbound left-turn and southbound-through movements, and at the SR 113 & Regency Parkway/Industrial Way intersection for the southbound through movement.

The northbound through 95th percentile queue at the SR 113 & Regency Parkway/Industrial Way intersection blocks the adjacent left-turn pocket under all study conditions, and the Project adds up to five (5) feet of queueing over Near-Term conditions. Signal timing adjustments are not projected to significantly shorten this queue. There is no room to extend the existing northbound left-turn pocket at SR 113 & Regency Parkway/Industrial Way because it is currently back-to-back with another left-turn pocket directly to the south. There is no feasible improvement that can be recommended at this location. Therefore, there would be a significant adverse effect on the northbound queueing of SR 113 & Regency Parkway/Industrial Way that cannot be addressed.

PROJECT ACCESS AND CIRCULATION

Based upon a review of the Project site, the sight distance at the Project Driveways, emergency access, and site internal circulation are considered adequate.

There are no proposed pedestrian path connections between the Project and directly adjacent parcels. Bicycles would access the surrounding Class II Bicycle Lane network on SR 113 and North Lincoln Street directly from the Project site. The Project would construct pedestrian sidewalks along

Project frontage on SR 113 and North Lincoln Street. Pedestrians could access the Gretchen Higgins Elementary School from the Project site via multiple paths that contain sidewalks, curb ramps, and bicycle lanes along the entire route.

SAFETY EVALUATION

Collision data indicated that a total 28 collisions occurred at the study facilities over the last five years. The severity of most collisions involved property damage only, followed by complaint of pain. The most common collision types were rear-end collisions, followed by sideswipe type collisions.

The most common primary collision factors were unsafe speed, followed by automobile right-of-way and improper turning. It is unlikely that the addition of Project traffic would contribute to an increased collision rate at the study facilities.

ADVERSE EFFECTS ON PEDESTRIAN AND BICYCLE FACILITIES

The Project would not eliminate or adversely affect an existing bikeway or pedestrian facility in a way that would discourage its use. The Project would not interfere with the implementation of a planned bikeway as shown in the General Plan. Furthermore, the Project would not provide inadequate access for bicyclists and pedestrians, that would result in unsafe conditions, including unsafe bicycle/pedestrian, bicycle/motor vehicle, or pedestrian/motor vehicle conflicts. The Project would provide adequate access for bicyclists and pedestrians. Therefore, the project is not anticipated to have any significant adverse effects on bicycle or pedestrian facilities.

VEHICLE MILES TRAVELED ANALYSIS

VMT analysis was performed for the Project site by DKS Associates utilizing the City's TDM. Project home-based VMT per capita was found to be 16, which falls below the City threshold of significance of 18.5 VMT per capita, as reported to City staff by DKS via email on May 30, 2023. Therefore, the Project can be assumed to have less than significant VMT impacts.

I. INTRODUCTION

This report has been prepared to present the results of the Traffic Impact Analysis (TIA) performed by Wood Rodgers, Inc. (Wood Rodgers) for the proposed Independence at Dixon development (Project) located in the city of Dixon, California (City). The Project location is shown in **Figure 1**. This analysis has been performed to determine any significant adverse effects the proposed Project may cause on surrounding transportation facilities and identify potential improvement measures.

I.1 PROJECT DESCRIPTION

The proposed Independence at Dixon Project site is located on one (1) vacant parcel totaling 10.98 acres within the southwest corner of the intersection of State Route (SR) 113 and North Lincoln Street/Vaughn Road. The Project would gain access to the existing roadway network via one new driveway connection on North Lincoln Street and one new driveway connection on SR 113. The Project would develop 186 duplex/duet-style residential dwelling units. **Figure 2** shows the Project site plan.

The Lincoln Square Project was previously proposed at this location and included a residential component of 102 detached single-family lots and a gas station with convenience store located on an adjacent parcel. The gas station would consist of a 4,500 square foot convenience store, a 5,789 square foot fueling canopy with 16 fueling positions, and a 2,613 square foot car wash. However, the newly proposed Independence at Dixon Project no longer includes the gas station or adjacent parcel, which is moving forward as a separate project. The Independence at Dixon Project consists of 186 residential dwelling units compared to the 102 residential dwelling units proposed under the Lincoln Square Project, and so it is projected that the new Project will generate more residential trips than Lincoln Square.

I.2 STUDY AREA

Study facilities include the intersections described below.

I.2.1 Intersections

Study intersections were selected based on where 50 or more peak hour Project trips were projected to be added, consistent with direction provided in the *Lincoln Square Project Design Review – 3rd Submittal Memorandum* (City of Dixon, January 27, 2022). The following six (6) existing and proposed study intersections were analyzed in this TIA:

1. SR 113 & I-80 Ramps/Auction Lane
2. SR 113 & Dorset Drive
3. SR 113 & North Lincoln Street/Vaughn Road
4. SR 113 & Regency Parkway/Industrial Way
5. Project Driveway 1 & North Lincoln Street (proposed)
6. SR 113 & Project Driveway 2 (proposed)

The locations of the above study intersections are shown in **Figure 1**.



Legend

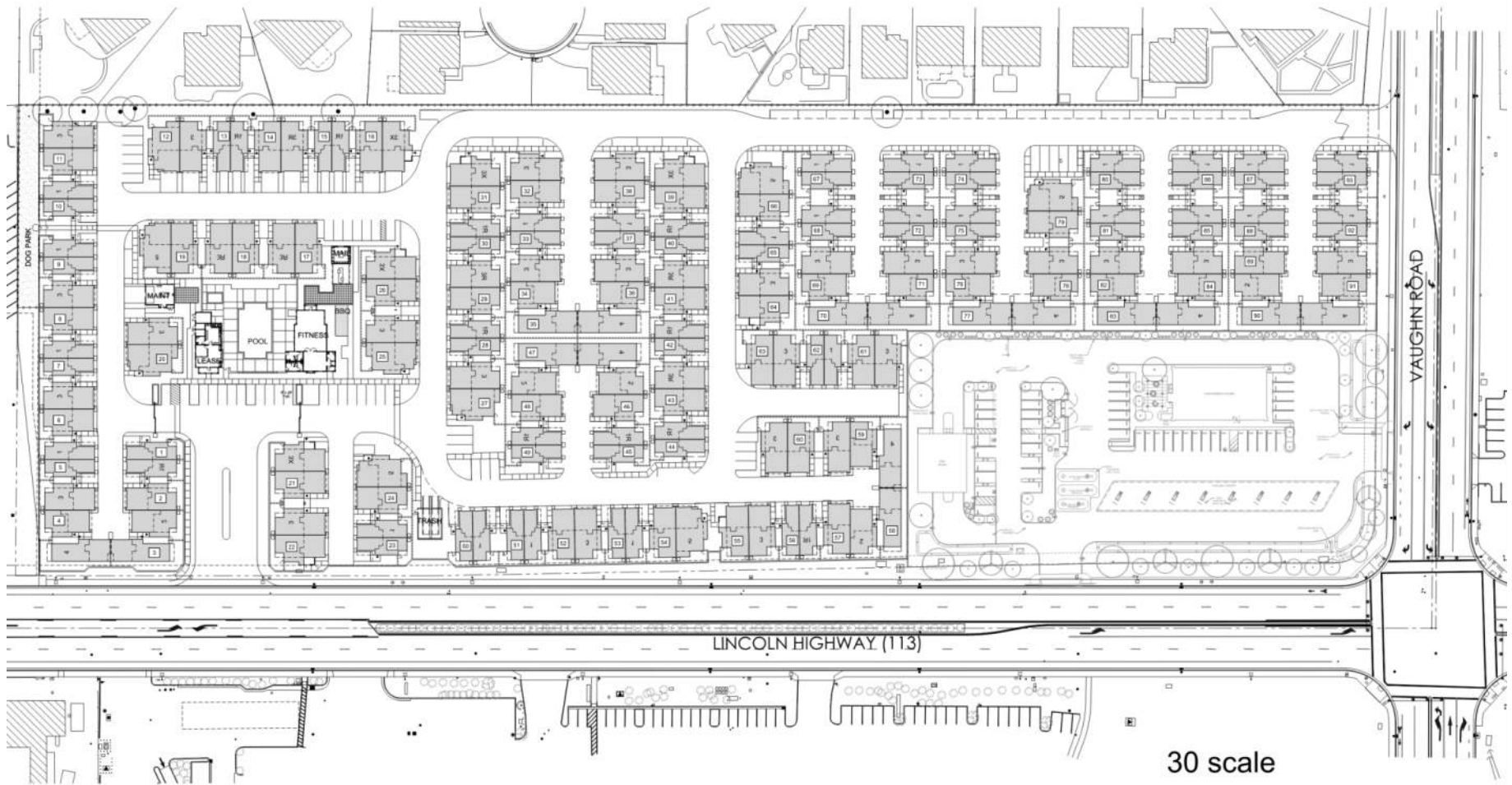
- Ⓝ Study Intersections
- Project Driveways
- Project Location

Project Location and Study Facilities
 Independence at Dixon TIA
 Dixon, CA
 July 2023

Figure 1



Figure 2. Project Site Plan



I.3 ANALYSIS SCENARIOS

The six study intersections were evaluated under weekday AM and PM peak hour conditions for the following scenarios:

- **Existing Conditions:** Existing traffic volumes from collected traffic counts.
- **Near-Term Conditions:** Traffic from existing traffic volumes plus volumes from approved and anticipated development at the time of completion of the project.
- **Near-Term plus Project Conditions:** Near-Term traffic volumes plus traffic projected to be generated by the proposed Project.

Cumulative year conditions were not evaluated because the Project is consistent with the General Plan zoning and density, and based on the recommendation from City Staff contained in comments dated February 28, 2022.

I.4 ANALYSIS METHODS

Traffic operations in this TIA have been quantified through the determination of "Level of Service" (LOS). Level of Service is a qualitative measure of traffic operating conditions, whereby a letter grade "A" through "F" is assigned to an intersection or roadway segment, representing progressively worsening traffic operations. LOS "A" represents free-flow conditions with little to no delays, while LOS "F" represents jammed or grid-lock conditions.

I.4.1 Intersections

Intersection LOS has been calculated for all intersection control types using methods documented in the Transportation Research Board Publication *Highway Capacity Manual, 6th Edition (HCM 6)* (Transportation Research Board, 2016). The calculated intersection delays correspond to the LOS designations shown in **Table 1**, which were derived from Exhibits 19-8 and 20-2 of *Highway Capacity Manual, 6th Edition* (HCM 6th Edition).

Table 1. HCM 6th Edition Based Intersection LOS Thresholds

| Level of Service | Description | Intersection Control Delay (seconds/vehicle) | |
|------------------|---|--|---------------------|
| | | Unsignalized | Signalized |
| A | Free-flow conditions with negligible to minimal delays. | delay ≤ 10.0 | delay ≤ 10.0 |
| B | Good progression with slight delays. | 10.0 < delay ≤ 15.0 | 10.0 < delay ≤ 20.0 |
| C | Relatively higher delays. | 15.0 < delay ≤ 25.0 | 20.0 < delay ≤ 35.0 |
| D | Somewhat congested conditions with longer but tolerable delays. | 25.0 < delay ≤ 35.0 | 35.0 < delay ≤ 55.0 |
| E | Congested conditions with significant delays. | 35.0 < delay ≤ 50.0 | 55.0 < delay ≤ 80.0 |
| F | Jammed or grid-lock type operating conditions. | delay > 50.0 | delay > 80.0 |

Source: HCM 6th Edition Exhibit 19-8 and 20-2.

HCM 6th Edition reports were generated to determine the delay and LOS at the unsignalized intersections in Synchro software. Synchro Intersection reports were generated to determine the delay and LOS at the signalized intersections, since the HCM 6th Edition does not support U-turns for signalized intersections. U-turn volumes at the signalized study intersections were non-negligible, so it was necessary to account for the U-turns using the Synchro Intersection reports.

I.5 LEVEL OF SERVICE STANDARDS AND SIGNIFICANT ADVERSE EFFECT CRITERIA

I.5.1 Intersection Level of Service Significant Adverse Effect Criteria

The *City of Dixon General Plan 2040 (adopted May 2021)* states that Dixon aims to have all intersections achieve at least LOS “D”.

Per the *2022 Final Dixon TIA Guidelines*, the following thresholds were used to determine if the proposed Project would create significant adverse effects related to intersections:

- **Signalized Intersections:** A project is considered to have a significant effect if it would:
 - Result in a signalized intersection operating at an acceptable LOS (LOS “D” or better) to deteriorate to an unacceptable LOS; or
 - Increase the average delay by more than two (2) seconds at a signalized intersection that is operating at an unacceptable LOS without the project.
- **Unsignalized Intersections:** A project is considered to have a significant effect if it would:
 - Result in an unsignalized intersection movement/approach operating at an acceptable LOS to deteriorate to an unacceptable LOS, and also cause the intersection to meet a traffic signal warrant; or
 - For an unsignalized intersection that meets a signal warrant under existing or background conditions, increase the delay by more than two (2) seconds at a movement/approach that is operating at an unacceptable LOS without the project.

SR 113 (North First Street) is a Caltrans facility. Caltrans published the *Guide for the Preparation of Traffic Impact Studies* (December 2002) which states the following:

“Caltrans endeavors to maintain a target LOS at the transition between LOS “C” and LOS “D” on State highway facilities, however, Caltrans acknowledges that this may not be always feasible and recommends that the lead agency consult with Caltrans to determine the appropriate target LOS”

Based on the above, the minimum LOS standard for all Caltrans facilities was assumed to be LOS “D”.

I.5.2 Pedestrian and Bicycle Significant Adverse Effect Criteria

Per the *2022 Final Dixon TIA Guidelines*, the following thresholds were used to determine if the proposed Project would create significant adverse effects related to bicycle and pedestrian facilities:

- **Pedestrian and bicycle facilities:** A project is considered to have a significant effect if it would:
 - Eliminate or adversely affect an existing bikeway or pedestrian facility in a way that would discourage its use;
 - Interfere with the implementation of a planned bikeway as shown in the General Plan; or
 - Fail to provide adequate access for bicyclists and pedestrians, resulting in unsafe conditions, including unsafe bicycle/pedestrian, bicycle/motor vehicle, or pedestrian/motor vehicle conflicts.

I.6 REPORT ORGANIZATION

The remainder of this report is divided into the following chapters:

- **Chapter 2: Existing Conditions** – Describes existing conditions and operations of the study area intersections, transit system, pedestrian facilities, and bicycle facilities.
- **Chapter 3: Near-Term Conditions** – Describes projected conditions and operations of study area facilities under Near-Term future (year 2024) conditions.

- **Chapter 4: Near-Term Plus Project Conditions** – Describes the methods used to estimate and distribute Project generated traffic and the resulting study area operations under Near-Term Plus Project conditions.
- **Chapter 5: Project Adverse Effects and Improvements** – Describes the projected significant adverse effects at study area facilities and presents potential improvements.
- **Chapter 6: Queueing Analysis and Improvements** – Describes the projected queues at the study area facilities for all analysis scenarios.
- **Chapter 7: Site Access and Circulation** – Describes site access and on-site circulation for the Project site.
- **Chapter 8: Safety Evaluation** – Describes the collision history and potential safety issues within the study area.
- **Chapter 9: Adverse Effects on Bicycle and Pedestrian Facilities** – Describes potential effects the proposed Project will have on pedestrian and bicycle facilities and summarizes planned improvements in the study area.
- **Chapter 10: Vehicle Miles Traveled Analysis** – Describes Project impact on Vehicle Miles Traveled (VMT).

2. EXISTING CONDITIONS

This chapter describes the Existing roadway network, transit services, pedestrian facilities, and bicycle facilities within the study area. It also presents Existing traffic volumes at study facilities and traffic operations under Existing weekday AM and PM peak hour conditions.

2.1 EXISTING ROADWAY NETWORK

This section provides descriptions of the study area roadways.

SR 113 is a four-lane north-south arterial, also called North First Street, within the study area. This portion of SR 113 provides connectivity between residential areas, commercial areas, and industrial areas in Dixon. The posted speed limit for SR 113 is 35-45 miles per hour (mph).

Interstate 80 (I-80) is an east-west freeway that runs along the western edge of Dixon and connects Dixon with the city of Vacaville to the southwest and the city of Davis to the northeast. In the vicinity of the project area, I-80 has six lanes. I-80 forms an interchange with SR 113 in the northern region of Dixon. The posted speed limit on I-80 is 65 mph.

Auction Lane is a north-south unpaved road adjacent to the interchange of I-80 with SR 113. Auction Lane connects to SR 113 at the southern terminus of Auction Lane. The roadway provides access from SR 113 to undeveloped land in the northeast region of Dixon. Auction Lane does not have a posted speed limit.

Dorset Drive is a four-lane local roadway west of SR 113 and a four-lane arterial east of SR 113. Dorset Drive provides a connection from SR 113 to the Walmart Supercenter and other commercial uses. The roadway generally runs east-west, but curves north approximately 400-feet east of SR 113. Dorset Drive has a posted speed limit of 35 mph east of SR 113. The speed limit is not posted west of SR 113.

North Lincoln Street is a minor arterial/major collector that runs east-west in the vicinity of Project area and transitions to north-south west of the Project area. The roadway has four lanes in the area adjacent to the Project. North Lincoln Street connects residential areas with commercial land uses along the western edge of Dixon. North Lincoln Street transitions to Vaughn Road east of SR 113. The posted speed limit on North Lincoln Street is 35 mph.

Vaughn Road is a two-lane east-west arterial that runs between SR 113 in the City of Dixon to Runge Road in Solano County. Vaughn Road transitions to North Lincoln Street west of SR 113. Vaughn Road provides access for commercial and industrial areas. Vaughn Road extends past the Dixon city limits to the undeveloped land to the east. The posted speed limit on Vaughn Road is 45 mph.

Regency Parkway is a two-lane, north-south minor arterial/major collector that runs between Industrial Way and Martin Court in the City of Dixon. Regency Parkway transitions to Industrial Way east of SR 113. Regency Parkway connects residential areas with SR 113 and North Lincoln Street. Regency Parkway has a posted speed limit of 30 mph.

Industrial Way is a two-lane, east-west collector. Industrial Way transitions to Regency Parkway west of SR 113. The roadway provides access to industrial and commercial uses in the northeast region of Dixon. Industrial Way has a posted speed limit of 30 mph.

2.2 PEDESTRIAN FACILITIES

Sidewalks are generally provided along all roadways in the study area including SR 113, Dorset Drive, North Lincoln Street, Vaughn Road, Regency Parkway, and Industrial Way, with the exception of Auction Lane which is unpaved. There is no sidewalk provided along the northern edge of Vaughn Road east of SR 113. The sidewalk along both sides of SR 113 terminates just north of Dorset Drive. Four striped crosswalks with corresponding pedestrian push buttons are provided at the

intersections of SR 113 with Dorset Drive, North Lincoln Street/Vaughn Road, and Regency Parkway/Industrial Way. The interchange intersection of the I-80 Ramps and SR 113 does not provide pedestrian facilities such as sidewalks or crosswalks.

2.3 BICYCLE FACILITIES

Within the study area, Class II bicycle lanes are provided on both sides of SR 113. Class II bicycle lanes are provided on both sides of Regency Parkway, North Lincoln Street, Vaughn Road, and Dorset Drive. No bicycle facilities are provided for Industrial Way, Auction Lane, or the I-80 Ramps.

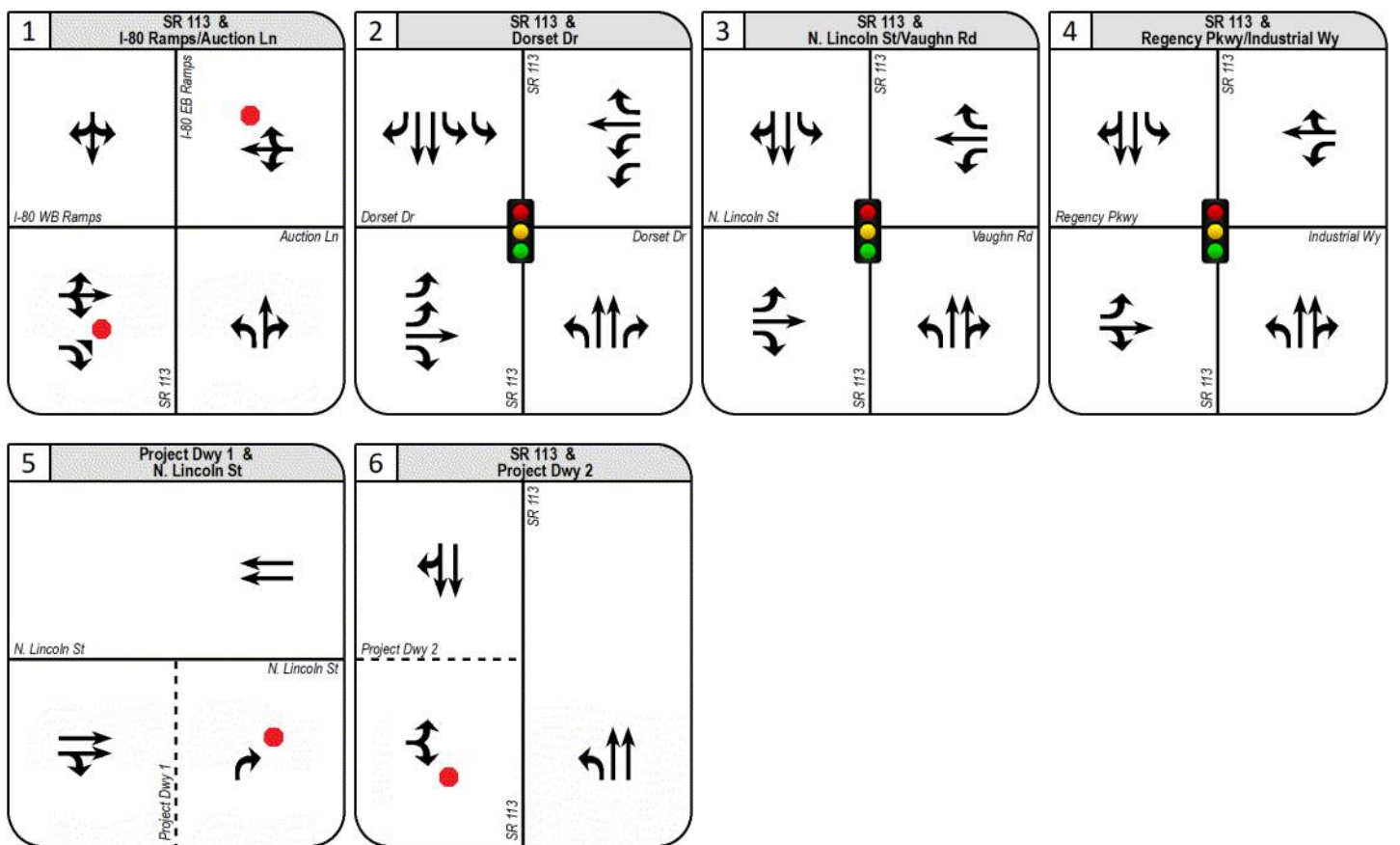
2.4 EXISTING TRANSIT SERVICE

Within Dixon city limits, the City operates a dial-a-ride transit system called Read-Ride which provides curb-to-curb transit service. The Read-Ride service operates Monday through Friday, from approximately 7:00 AM to 4:00 PM. For transit service to and from regional destinations outside of Dixon, Fairfield and Suisun Transit (FAST) runs an express bus service called the Blue Line. Currently, the Blue Line has limited hours that only cater to traditional commuting times and does not run on Sundays. The Blue Line picks up at the Dixon Park & Ride Station, and connects Dixon with Sacramento's Capitol Mall, UC Davis, Solano Town Center in Fairfield, transportation centers in Fairfield and Vacaville, and the Pleasant Hill BART station. The Dixon Park & Ride Station is located on Market Lane, just west of Pitt School Road which is roughly 1.5 miles from the proposed Project site.

2.5 EXISTING INTERSECTION TRAFFIC VOLUMES AND LANE GEOMETRICS

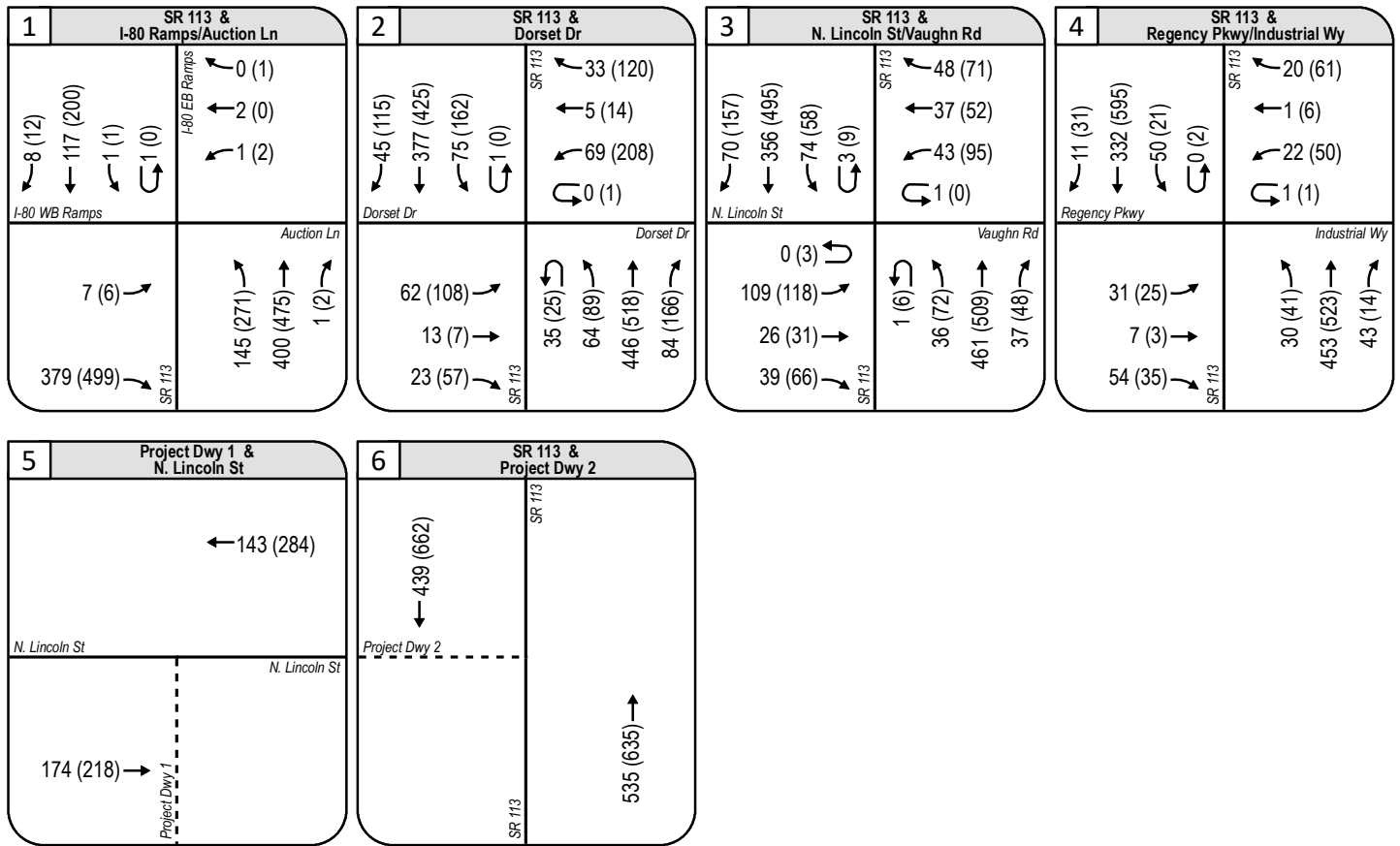
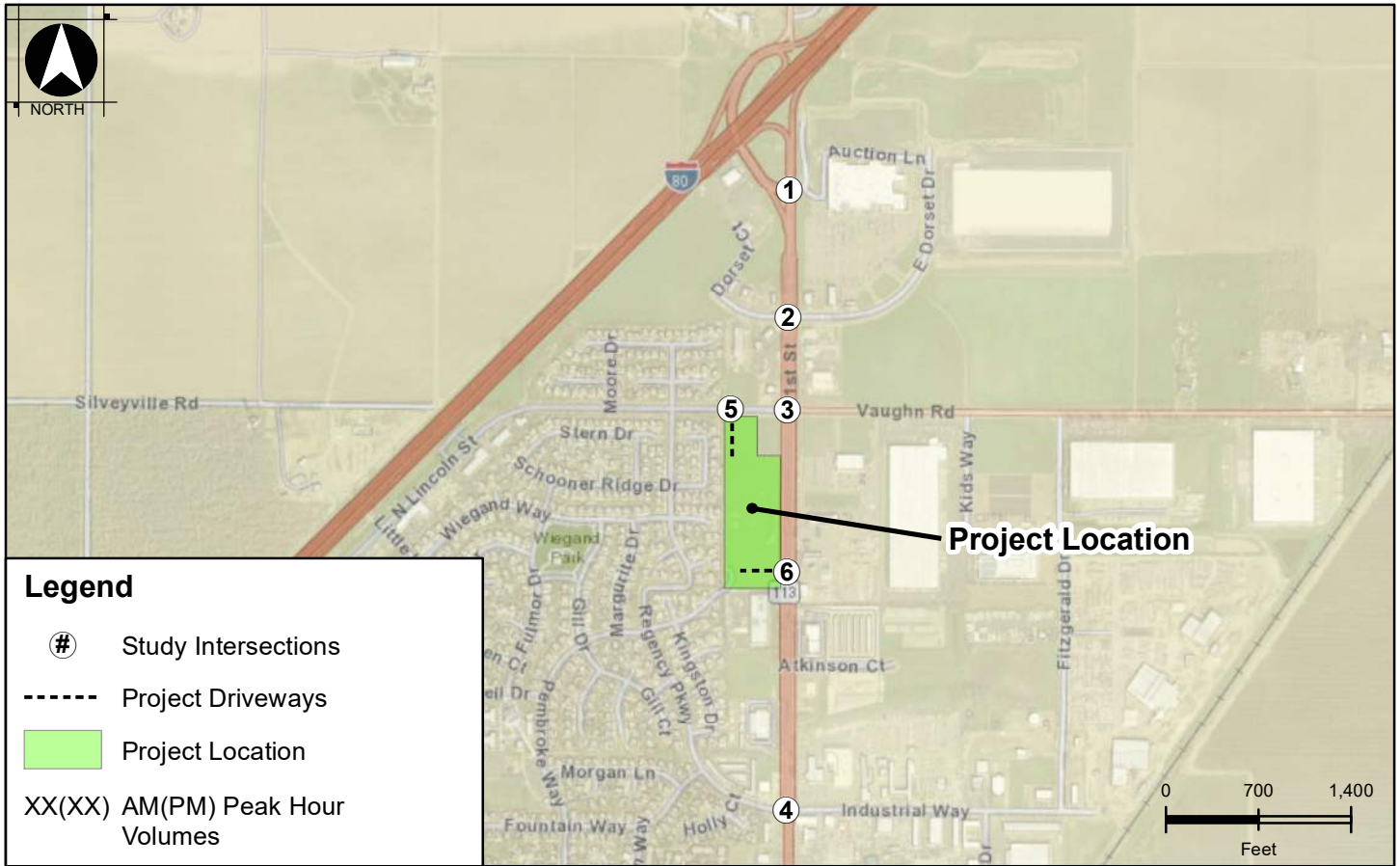
Intersection traffic operations were evaluated for the weekday AM and PM peak hours. The AM peak hour is defined as the highest one hour of traffic flow counted between 7:00 AM and 9:00 AM on a typical weekday. The PM peak hour is defined as the highest one hour of traffic flow counted between 4:00 PM and 6:00 PM on a typical weekday. AM and PM peak hour traffic counts for the four (4) existing study intersections were collected on Wednesday, January 12, 2022. To account for possible growth that has occurred since January 2022, new peak hour traffic counts were collected at the SR 113 & North Lincoln Street/Vaughn Road intersection on Tuesday April 11, 2023. The new 2023 counts were found to be higher than the 2022 counts by 0.83% during the AM peak hour and by 7.12% during the PM peak hour. 2022 Traffic counts at other study intersections were increased accordingly to obtain Existing (2023) conditions traffic volumes. Traffic count data is provided in **Appendix A**.

Figure 3 illustrates Existing intersection lane geometrics and control for the study area intersections #1 through #4. **Figure 3** also shows "Plus Project" intersection lane geometrics and control for the Project Driveway intersections (#5 and #6). **Figure 4** depicts Existing conditions turning movements volumes for AM and PM weekday peak hours.



Intersection Lane Geometrics and Control
 Independence at Dixon TIA
 Dixon, CA
 July 2023

Figure 3



Existing Intersection Turning Movement Volumes
 Independence at Dixon TIA
 Dixon, CA
 July 2023

Figure 4



2.6 EXISTING INTERSECTION OPERATIONS

Table 2 presents Existing study intersection traffic operations under Existing intersection lane geometrics and control (illustrated in **Figure 3**) and Existing traffic volumes (illustrated in **Figure 4**). All study intersection traffic operations were calculated using Synchro 11 software.

Table 2. Existing Intersection Operations

| # | Intersection | Control Type | LOS Criteria | Peak Hour | Delay (sec) ² | LOS ² | Peak Hour Signal Warrant Met? | |
|---|---|-------------------|--------------|-----------|----------------------------------|------------------|-------------------------------|--|
| 1 | SR 113 & I-80 Ramps/Auction Lane | TWSC ¹ | D | AM | 28.9 (Mvt: WBL/T/R, Vol: 3) | D | No | |
| | | | | PM | 45.2 (Mvt: EBL/T, Vol: 6) | E | No | |
| 2 | SR 113 & Dorset Drive | Signal | D | AM | 23.7 | C | N/A | |
| | | | | PM | 27.6 | C | | |
| 3 | SR 113 & North Lincoln Street/Vaughn Road | Signal | D | AM | 24.1 | C | | |
| | | | | PM | 25.2 | C | | |
| 4 | SR 113 & Regency Parkway/Industrial Way | Signal | D | AM | 15.6 | B | | |
| | | | | PM | 19.4 | B | | |
| <p><i>Notes:</i> ¹ TWSC = Two-Way Stop-Controlled ² For TWSC, the worst approach/movement delay and LOS is reported: Mvt = Worst-Case Movement, Vol = Worst-Case Movement Volume. Average intersections delay is reported for Signalized intersections. HCM 6th Edition reports were generated to determine the delay and LOS at the TWSC intersections. Synchro Intersection reports were generated to determine the delay and LOS at the signalized intersections, as HCM 6th Edition does not support U-turns. BOLD = Unacceptable LOS</p> | | | | | | | | |

As shown in **Table 2**, the intersection of SR 113 & I-80 Ramps/Auction Lane is currently operating at unacceptable LOS E during the PM peak hour. All other study intersections are currently operating at acceptable LOS conditions (LOS “D” or better) during the weekday AM and PM peak hours. Synchro software intersection LOS output reports are included in **Appendix B**. The SR 113 & I-80 Ramps/Auction Lane intersection does not meet peak hour signal warrants for the AM and PM peak hours. The signal warrant worksheets are provided in **Appendix C**.

3. NEAR-TERM CONDITIONS

This chapter describes the Near-Term conditions roadway network, traffic volumes, and traffic operations at study facilities.

3.1 NEAR-TERM ROADWAY NETWORK

The City of Dixon Five Year Capital Improvement Program (adopted June 13, 2017) does not identify any capital improvement projects at or around the study area facilities. Therefore, the following analysis assumes that the Existing intersection lane geometry and control type is the same for Near-Term conditions (see **Figure 3**).

3.2 NEAR-TERM VOLUMES

Near-Term conditions were developed by adding volumes from approved and anticipated development (background projects) to the existing traffic counts. Near-Term conditions represent the traffic conditions in the year 2024, which is the estimated “opening day” year for the Project. The list of background projects was provided by City staff and are listed below:

- Southwest Specific Plan Area (Phases 1 – 3)
 - 817 additional single-family dwelling units
 - 131 multifamily dwelling units
 - 23 acres community commercial plus 21,000 square-foot commercial (357 retail jobs).
- Valley Glen Development
 - 316-single-family dwelling units
- Heritage Commons Development
 - 44 multifamily dwelling units
- Park Lane Development
 - 121 single-family dwelling units
- 500,000 square-foot warehouse (217 industrial jobs) in northern Dixon area
- 2,100 square-foot drive-thru pad (2 retail jobs) in northern Dixon area
- 3,000 square-foot dispensary (3 retail jobs) in northern Dixon area
- 4,200 square-foot restaurant (3 retail jobs) in northern Dixon area

The City’s on-call traffic modeling consultant, DKS Associates (DKS), prepared a Near-Term conditions scenario in the City’s travel demand model (TDM) that contained all the background projects listed above. DKS provided TDM turning movement volumes at all study intersections from both Existing and Near-Term TDM scenarios. Volumes from approved and anticipated projects were obtained by taking the difference of the Existing and Near-Term TDM scenario turning movement volumes.

In addition to the projects above, traffic from the proposed gas station and convenience store adjacent to the Project site (previously studied in the *Lincoln Square Traffic Impact Report* (Wood Rodgers, March 2022)) was included under Near-Term conditions. The background projects are illustrated in **Appendix D. Figure 5** provides the weekday AM and PM peak hour Near-Term traffic volumes at the study intersections.

3.3 NEAR-TERM INTERSECTION OPERATIONS

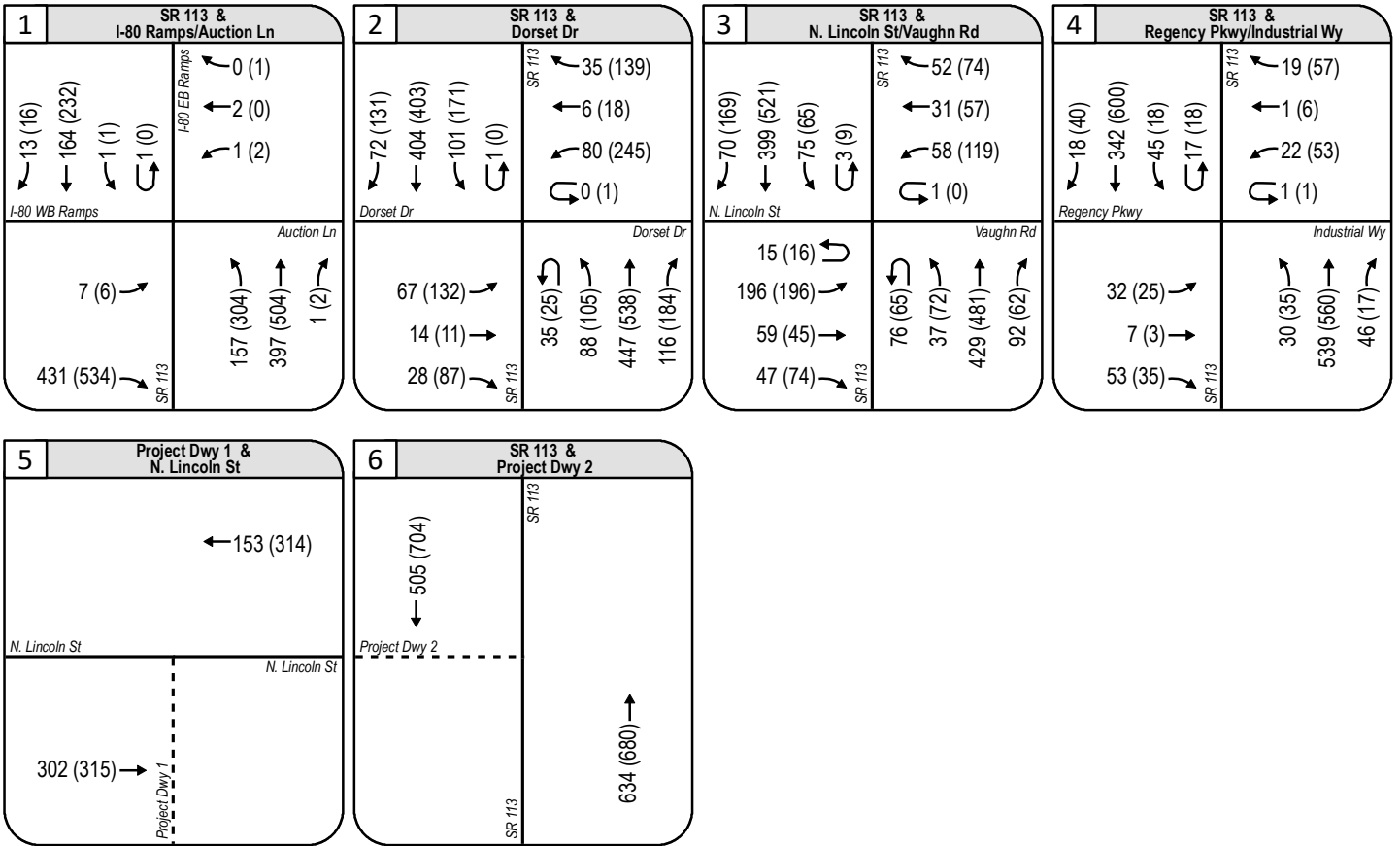
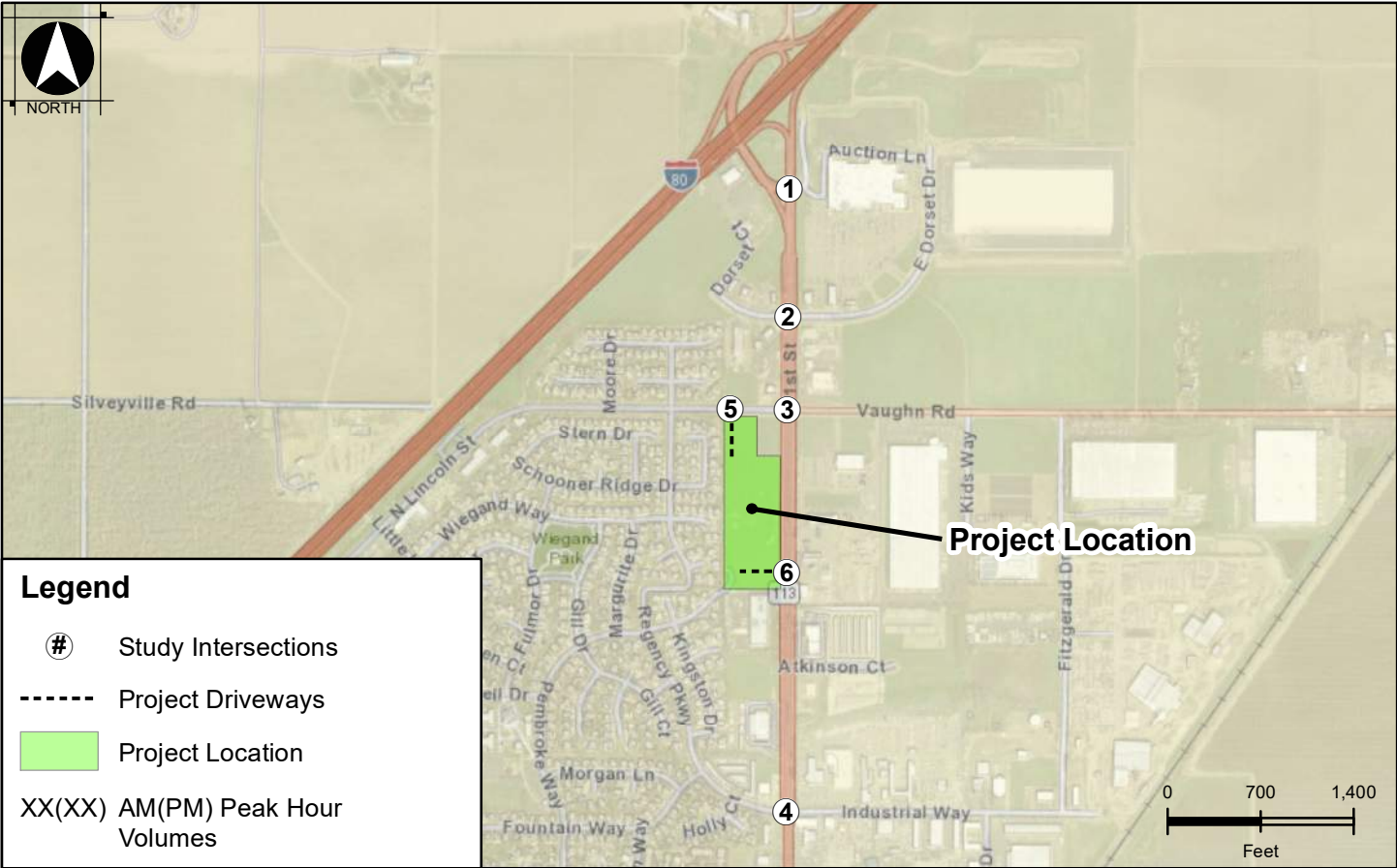
Near-Term intersection operations were quantified under Near-Term traffic volumes (shown in **Figure 5**) and Existing intersection lane geometrics and control (shown in **Figure 3**). **Table 3** illustrates the resulting Near-Term intersection LOS operations. All study intersection traffic operations were calculated using Synchro 11 software.

Table 3. Near-Term Intersection Operations

| # | Intersection | Control Type | LOS Criteria | Peak Hour | Delay (sec) ² | LOS ² | Peak Hour Signal Warrant Met? |
|---|---|-------------------|--------------|-----------|----------------------------------|------------------|-------------------------------|
| 1 | SR 113 & I-80 Ramps/Auction Lane | TWSC ¹ | D | AM | 33.0 (Mvt: WBL/T/R, Vol: 3) | D | No |
| | | | | PM | 59.0 (Mvt: EBL/T, Vol: 6) | F | No |
| 2 | SR 113 & Dorset Drive | Signal | D | AM | 24.5 | C | N/A |
| | | | | PM | 28.8 | C | N/A |
| 3 | SR 113 & North Lincoln Street/Vaughn Road | Signal | D | AM | 30.9 | C | N/A |
| | | | | PM | 33.0 | C | N/A |
| 4 | SR 113 & Regency Parkway | Signal | D | AM | 18.4 | B | N/A |
| | | | | PM | 18.9 | B | N/A |

Notes:
¹ TWSC = Two-Way Stop-Controlled
² For TWSC, the worst approach/movement delay and LOS is reported: Mvt = Worst-Case Movement, Vol = Worst-Case Movement Volume. Average intersections delay is reported for Signalized intersections. HCM 6th Edition reports were generated to determine the delay and LOS at the TWSC intersections. Synchro Intersection reports were generated to determine the delay and LOS at the signalized intersections, as HCM 6th Edition does not support U-turns.
BOLD = Unacceptable LOS

As shown in **Table 3**, the intersection of SR 113 & I-80 Ramps/Auction Lane is anticipated to operate at unacceptable LOS F under Near-Term PM peak hour conditions. The remaining study intersections are projected to operate at acceptable LOS (LOS “D” or better). Synchro intersection LOS output reports are included in **Appendix B**. The SR 113 & I-80 Ramps/Auction Lane intersection is not projected meet peak hour signal warrants for the AM and PM peak hours. The signal warrant worksheets are provided in **Appendix C**.



Near-Term Intersection Turning Movement Volumes
 Independence at Dixon TIA
 Dixon, CA
 July 2023

Figure 5



4. NEAR-TERM PLUS PROJECT CONDITIONS

This chapter provides a description of the proposed Project, a discussion of the trip generation and distribution/assignment methods used to come up with Project trips at study intersections, and an analysis of projected traffic operations and significant adverse effects under Near-Term Plus Project conditions.

4.1 PROJECT SITE

4.1.1 Project Site Description

The proposed Independence at Dixon development site is located on one (1) vacant parcel totaling 10.98 acres within the southwest corner of the intersection of SR 113 & North Lincoln Street/Vaughn Road. There are residential land uses to the west of the Project site, industrial/storage land uses to the south, and commercial/office/mixed-use land uses to the north and east of the Project site. The Project site parcel is zoned as Light Industrial, Professional and Administrative Office, and Planned Development (ML-PAO-PD). The Project would gain access to the existing roadway network via one new right-in/right-out residential driveway connection on North Lincoln Street (Project Driveway 1) and one new full access residential driveway connection on SR 113 (Project Driveway 2). The Project would develop 186 duplex/duet-style residential dwelling units.

4.2 PROJECT GENERATED TRIPS

4.2.1 Trip Generation

The trip generation data contained in the *Institute of Transportation Engineers (ITE) Trip Generation Manual, 11th Edition* was used to approximate the number of trips generated by the Project. The ITE land use category of Single-Family Attached Housing (ITE Code 215) was used to represent the Project.

Table 4. Project Trip Generation

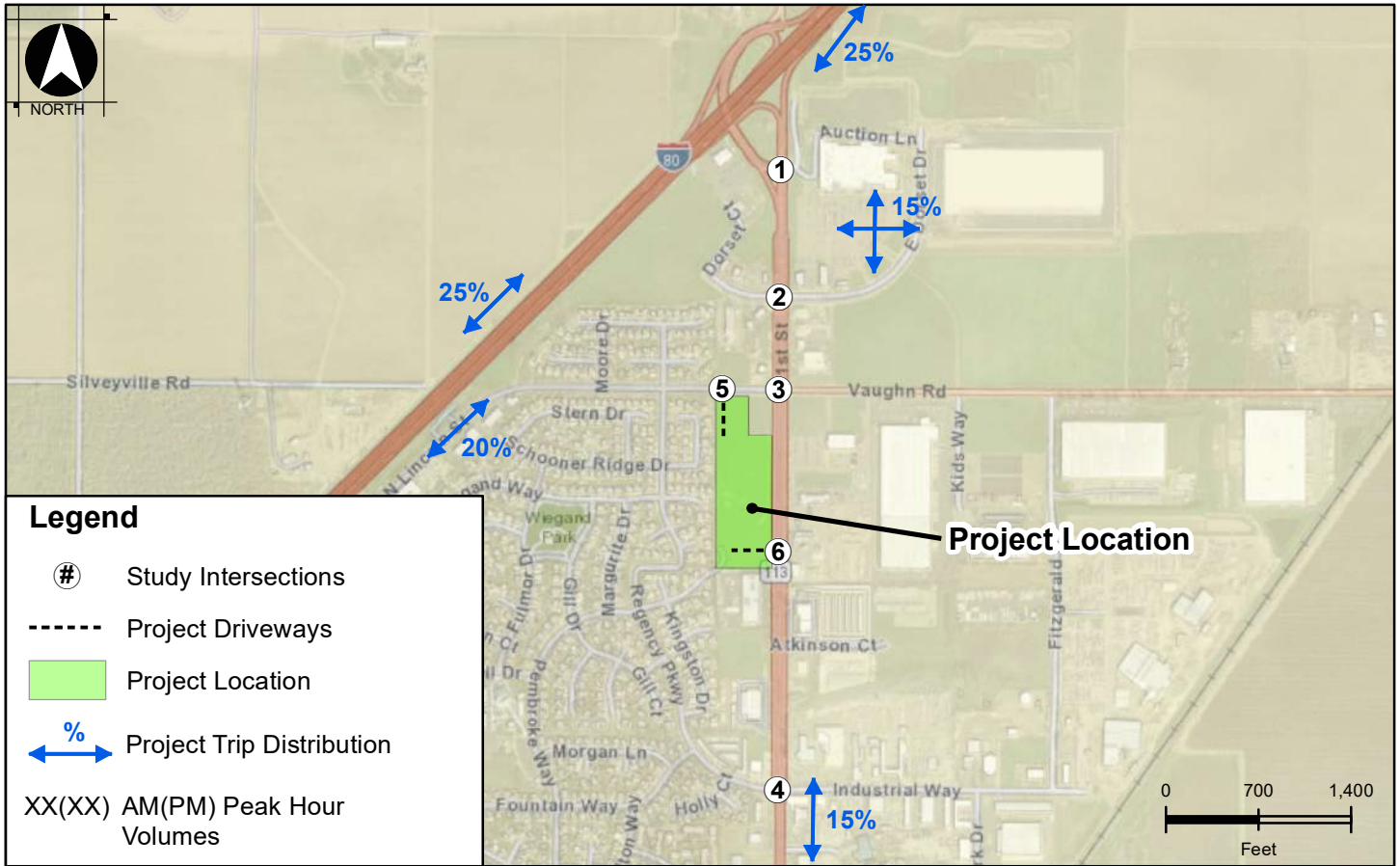
| ITE Code | Land Use Category | Quantity | Units | Daily ¹ | AM Peak Hour ¹ | | | PM Peak Hour ¹ | | |
|----------|--------------------------------|----------|-----------------|--------------------|---------------------------|-----|-------|---------------------------|-----|-------|
| | | | | | In | Out | Total | In | Out | Total |
| 215 | Single-Family Attached Housing | 186 | DU ² | 1,367 | 23 | 68 | 91 | 64 | 44 | 108 |

Notes:
¹ Trip rates are calculated based on ITE Trip Generation (11th Edition) fitted curve equations.
² DU = Dwelling Unit

As shown in **Table 4**, the proposed Project is estimated to generate a total of 1,367 daily trips with 91 AM peak-hour weekday trips and 108 PM peak-hour weekday trips.

4.2.2 Trip Distribution and Assignment

The Project trip distribution was determined based on existing traffic counts and travel patterns, knowledge of the area, Near-Term Plus Project scenario forecasts from the City's TDM (provided by DKS), and engineering judgement. Trip distribution was prepared for the Project trips. Project trip distribution and assignment is shown in **Figure 6**.



| 1 | SR 113 & I-80 Ramps/Auction Ln | 2 | SR 113 & Dorset Dr | 3 | SR 113 & N. Lincoln St/Vaughn Rd | 4 | SR 113 & Regency Pkwy/Industrial Wy | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|--------------------------------|---------------|--------------------|---|----------------------------------|------------|-------------------------------------|-----------|----------|-----------|--|---------------|---------------|-----------|--|-----------|-----------|-----------|----------|--------|-----------|----------|-----------|--|----------|--------|--|--|---------------|-----------|-----------|--|--|----------|--|-----------|--------|--|--|-----------|--|--------------|---------------|----------|--|--|----------|--------|--|---|---------------|---------------|----------|--|--|-----------|--------|--|----------|--|--|---------------|---------------|-----------|--|--|-----------|--|---------|--------|--|----------|--|
| <table border="1"> <tr> <td>I-80 WB Ramps</td> <td>I-80 EB Ramps</td> </tr> <tr> <td>6 (16) ↓</td> <td></td> </tr> <tr> <td></td> <td>Auction Ln</td> </tr> <tr> <td></td> <td>17 (11) →</td> </tr> <tr> <td></td> <td>17 (11) ←</td> </tr> <tr> <td>SR 113</td> <td></td> </tr> <tr> <td>6 (16) →</td> <td></td> </tr> </table> | I-80 WB Ramps | I-80 EB Ramps | 6 (16) ↓ | | | Auction Ln | | 17 (11) → | | 17 (11) ← | SR 113 | | 6 (16) → | | <table border="1"> <tr> <td>Dorset Dr</td> <td>Dorset Dr</td> </tr> <tr> <td>12 (32) ↓</td> <td>3 (10) ←</td> </tr> <tr> <td></td> <td>Dorset Dr</td> </tr> <tr> <td></td> <td>34 (22) ↑</td> </tr> <tr> <td></td> <td>10 (7) →</td> </tr> <tr> <td>SR 113</td> <td></td> </tr> </table> | Dorset Dr | Dorset Dr | 12 (32) ↓ | 3 (10) ← | | Dorset Dr | | 34 (22) ↑ | | 10 (7) → | SR 113 | | <table border="1"> <tr> <td>N. Lincoln St</td> <td>Vaughn Rd</td> </tr> <tr> <td>15 (42) ↓</td> <td></td> </tr> <tr> <td></td> <td>14 (9) ↻</td> </tr> <tr> <td></td> <td>22 (14) ↻</td> </tr> <tr> <td>SR 113</td> <td></td> </tr> <tr> <td></td> <td>22 (14) ↑</td> </tr> </table> | N. Lincoln St | Vaughn Rd | 15 (42) ↓ | | | 14 (9) ↻ | | 22 (14) ↻ | SR 113 | | | 22 (14) ↑ | <table border="1"> <tr> <td>Regency Pkwy</td> <td>Industrial Wy</td> </tr> <tr> <td>10 (7) ↓</td> <td></td> </tr> <tr> <td></td> <td>3 (10) ↑</td> </tr> <tr> <td>SR 113</td> <td></td> </tr> </table> | Regency Pkwy | Industrial Wy | 10 (7) ↓ | | | 3 (10) ↑ | SR 113 | | <table border="1"> <tr> <td>N. Lincoln St</td> <td>N. Lincoln St</td> </tr> <tr> <td>14 (9) ←</td> <td></td> </tr> <tr> <td></td> <td>35 (23) →</td> </tr> <tr> <td>SR 113</td> <td></td> </tr> <tr> <td>5 (13) →</td> <td></td> </tr> </table> | N. Lincoln St | N. Lincoln St | 14 (9) ← | | | 35 (23) → | SR 113 | | 5 (13) → | | <table border="1"> <tr> <td>Project Dwy 2</td> <td>Project Dwy 2</td> </tr> <tr> <td>15 (42) ↓</td> <td></td> </tr> <tr> <td></td> <td>23 (14) →</td> </tr> <tr> <td></td> <td>3 (9) →</td> </tr> <tr> <td>SR 113</td> <td></td> </tr> <tr> <td>10 (7) →</td> <td></td> </tr> </table> | Project Dwy 2 | Project Dwy 2 | 15 (42) ↓ | | | 23 (14) → | | 3 (9) → | SR 113 | | 10 (7) → | |
| I-80 WB Ramps | I-80 EB Ramps | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 (16) ↓ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Auction Ln | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 17 (11) → | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 17 (11) ← | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 (16) → | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Dorset Dr | Dorset Dr | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 12 (32) ↓ | 3 (10) ← | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Dorset Dr | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 34 (22) ↑ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 10 (7) → | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| N. Lincoln St | Vaughn Rd | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 15 (42) ↓ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 14 (9) ↻ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 22 (14) ↻ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 22 (14) ↑ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Regency Pkwy | Industrial Wy | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10 (7) ↓ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 3 (10) ↑ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1"> <tr> <td>N. Lincoln St</td> <td>N. Lincoln St</td> </tr> <tr> <td>14 (9) ←</td> <td></td> </tr> <tr> <td></td> <td>35 (23) →</td> </tr> <tr> <td>SR 113</td> <td></td> </tr> <tr> <td>5 (13) →</td> <td></td> </tr> </table> | N. Lincoln St | N. Lincoln St | 14 (9) ← | | | 35 (23) → | SR 113 | | 5 (13) → | | <table border="1"> <tr> <td>Project Dwy 2</td> <td>Project Dwy 2</td> </tr> <tr> <td>15 (42) ↓</td> <td></td> </tr> <tr> <td></td> <td>23 (14) →</td> </tr> <tr> <td></td> <td>3 (9) →</td> </tr> <tr> <td>SR 113</td> <td></td> </tr> <tr> <td>10 (7) →</td> <td></td> </tr> </table> | Project Dwy 2 | Project Dwy 2 | 15 (42) ↓ | | | 23 (14) → | | 3 (9) → | SR 113 | | 10 (7) → | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| N. Lincoln St | N. Lincoln St | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14 (9) ← | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 35 (23) → | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5 (13) → | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Project Dwy 2 | Project Dwy 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 15 (42) ↓ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 23 (14) → | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 3 (9) → | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10 (7) → | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Project Trips and Distribution
 Independence at Dixon TIA
 Dixon, CA
 July 2023

Figure 6



4.3 NEAR-TERM PLUS PROJECT INTERSECTION OPERATIONS

The Project Trips were added to Near-Term turning movement volumes at the study intersections to develop Near-Term Plus Project turning movement volumes. **Figure 7** shows the Near-Term Plus Project traffic volumes. Near-Term Plus Project intersection operations were evaluated under Near-Term Plus Project traffic volumes and Near-Term Plus Project intersection lane geometrics and traffic control (illustrated in **Figure 3**). **Table 5** indicates the Near-Term Plus Project intersection LOS operations. **Table 5** also contains Near-Term conditions intersection delays and LOS for comparison purposes. All study intersection traffic operations were calculated using Synchro 11 software.

Table 5. Near-Term Plus Project Intersection Operations

| # | Intersection | Control Type ¹ | LOS Criteria | Peak Hour | Near-Term | | Near-Term Plus Project | | |
|---|---|---------------------------|--------------|-----------|--|-----|--|-----|---------------------------|
| | | | | | Delay (sec) ² | LOS | Delay (sec) ² | LOS | Pk Hr Signal Warrant Met? |
| 1 | SR 113 & I-80 Ramps/Auction Lane | TWSC ¹ | D | AM | 33.0 (Mvt: WBL/T/R, Vol: 3) | D | 36.7 (Mvt: WBL/T/R, Vol: 3) | E | No |
| | | | | PM | 59.0 (Mvt: EBL/T, Vol: 6) | F | 65.4 (Mvt: EBL/T, Vol: 6) | F | No |
| 2 | SR 113 & Dorset Drive | Signal | D | AM | 24.5 | C | 25.5 | C | N/A |
| | | | | PM | 28.8 | C | 33.6 | C | N/A |
| 3 | SR 113 & North Lincoln Street/Vaughn Road | Signal | D | AM | 30.9 | C | 31.9 | C | N/A |
| | | | | PM | 33.0 | C | 33.6 | C | N/A |
| 4 | SR 113 & Regency Parkway/Industrial Way | Signal | D | AM | 18.4 | B | 18.3 | B | N/A |
| | | | | PM | 18.9 | B | 19.0 | B | N/A |
| 5 | Project Driveway 1 & North Lincoln Street | OWSC ¹ | D | AM | - | - | 9.4 (Mvt: NB, Vol: 35) | A | No |
| | | | | PM | - | - | 9.5 (Mvt: NB, Vol: 23) | A | No |
| 6 | SR 113 & Project Driveway 2 | OWSC ¹ | D | AM | - | - | 17.0 (Mvt: EB, Vol: 23) | C | No |
| | | | | PM | - | - | 21.8 (Mvt: EB, Vol: 14) | C | No |

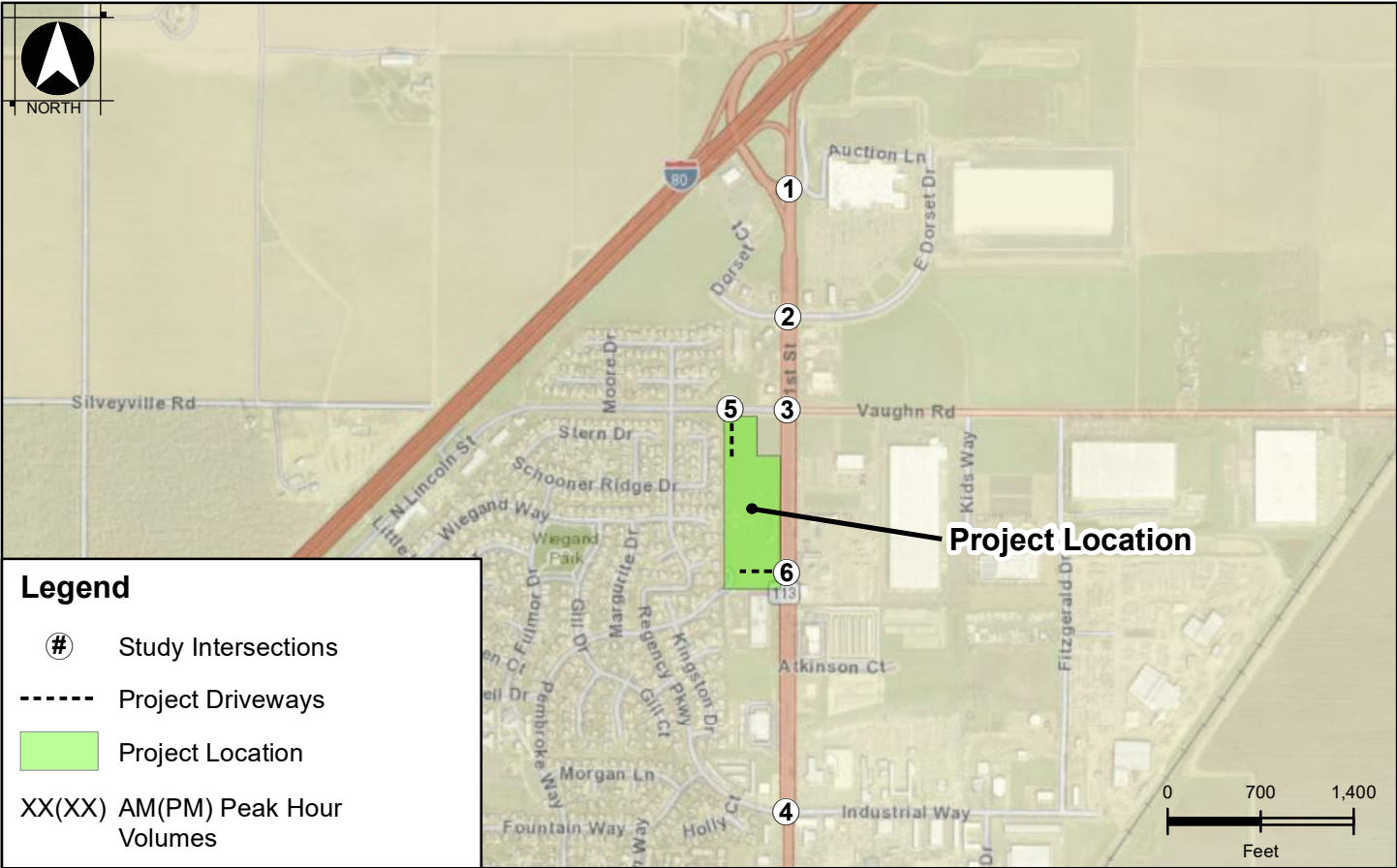
Notes:

¹ TWSC = Two-Way Stop-Controlled, OWSC = One-Way Stop-Controlled

² For TWSC and OWSC, the worst approach/movement delay and LOS is reported: Mvt = Worst-Case Movement, Vol = Worst-Case Movement Volume. Average intersections delay is reported for Signalized intersections. HCM 6th Edition reports were generated to determine the delay and LOS at the TWSC intersections. Synchro Intersection reports were generated to determine the delay and LOS at the signalized intersections, as HCM 6th Edition does not support U-turns.

BOLD = Unacceptable LOS

As shown in **Table 5**, all intersections are projected to operate at acceptable LOS (LOS “D” or better) under Near-Term Plus Project conditions, with the exception of the intersection of SR 113 & I-80 Ramps/Auction Lane, which is projected to operate at LOS E during the AM peak hour and LOS F during the PM peak hour. Synchro output reports are included in **Appendix B**. The SR 113 & I-80 Ramps/Auction Lane intersection is not projected to meet peak hour signal warrants for the AM and PM peak hours. The signal warrant worksheets are provided in **Appendix C**.



| 1 | SR 113 & I-80 Ramps/Auction Ln | 2 | SR 113 & Dorset Dr | 3 | SR 113 & N. Lincoln St/Vaughn Rd | 4 | SR 113 & Regency Pkwy/Industrial Wy | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|--|-----------|--------------------|-----------|----------------------------------|---------------|-------------------------------------|--|---------------|---------------|--------|--|-------|-------|-------|---------|--|--|-----------|-----------|-----------|-----------|-----------|--|--|--------|--------|--|--|----------|----------|----------|----------|--|--|---------------|-----------|---------|---------------|---------------|--------|--|--------|--------|--|---------|---------|---------|----------|-----------|---|---|-----------|-----------|---------|--------------|--------------|--|--|--------|---------|--|--|---------|---------|--|-----------|-------|---|-------|---------------|-----------|-----------|-------|---------------|--|--|--|-----------|--------|---------|--|---|---------|-----------|-----------|---------|---------------|---------|-----------|--|--------|--|--|--------|---------|--------|-------|-----------|---------|----------|-------|---------|---------|---------------|--|--|--|--|--------|--|--|--|--|---------|-------|---------|---------|-----------|---------------|--|--|--|--|--------|--|--|--|--|---------|--|--|--|--|--|-----------|--|--|--|---------------|--|--|--|---------------|--|--|--|-----------|--------|---------|--|---|---------|-----------|--|--|---------------|--|--|--|--------|--|--|--|---------|--------|-------|-----------|
| <table border="1"> <tr> <td> <table border="1"> <tr> <td>13 (16)</td> <td>170 (248)</td> <td>1 (1)</td> <td>1 (0)</td> </tr> <tr> <td colspan="4">I-80 WB Ramps</td> </tr> <tr> <td colspan="4">I-80 EB Ramps</td> </tr> <tr> <td>0 (1)</td> <td>2 (0)</td> <td colspan="2">1 (2)</td> </tr> </table> </td> <td> <table border="1"> <tr> <td>72 (131)</td> <td>416 (435)</td> <td>101 (171)</td> <td>1 (0)</td> </tr> <tr> <td colspan="4">Dorset Dr</td> </tr> <tr> <td colspan="4">SR 113</td> </tr> <tr> <td>35 (139)</td> <td>6 (18)</td> <td>83 (255)</td> <td>0 (1)</td> </tr> </table> </td> <td> <table border="1"> <tr> <td>70 (169)</td> <td>414 (563)</td> <td>75 (65)</td> <td>3 (9)</td> </tr> <tr> <td colspan="4">N. 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| 13 (16) | 170 (248) | 1 (1) | 1 (0) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| I-80 WB Ramps | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| I-80 EB Ramps | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0 (1) | 2 (0) | 1 (2) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 72 (131) | 416 (435) | 101 (171) | 1 (0) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Dorset Dr | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 35 (139) | 6 (18) | 83 (255) | 0 (1) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 70 (169) | 414 (563) | 75 (65) | 3 (9) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| N. Lincoln St | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 52 (74) | 31 (57) | 58 (119) | 1 (0) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 18 (40) | 352 (607) | 45 (18) | 17 (18) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Regency Pkwy | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 19 (57) | 1 (6) | 22 (53) | 1 (1) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| 7 (6) | 437 (550) | 174 (315) | 414 (515) | 1 (2) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Auction Ln | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 29 (25) | 218 (210) | 59 (45) | 47 (74) | 76 (65) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Vaughn Rd | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 31 (57) | 58 (119) | 1 (0) | 76 (65) | 37 (72) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Industrial Wy | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 32 (25) | 7 (3) | 53 (35) | 30 (35) | 542 (570) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Industrial Wy | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 46 (17) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 167 (323) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| N. Lincoln St | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Project Dwy 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 302 (315) | 5 (13) | 35 (23) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 15 (42) | 505 (704) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Project Dwy 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| SR 113 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 23 (14) | 10 (7) | 3 (9) | 634 (680) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Near-Term Plus Project Intersection Turning Movement Volumes
 Independence at Dixon TIA
 Dixon, CA
 July 2023

Figure 7



5. PROJECT ADVERSE EFFECTS AND IMPROVEMENTS

This chapter summarizes adverse effects caused by the Project at study intersections and identifies potential intersection improvements.

5.1 INTERSECTIONS

The intersection of SR 113 & I-80 Ramps/Auction Lane is projected to operate at unacceptable LOS E or F under Existing PM peak hour conditions, Near-Term PM peak hour conditions, and Near-Term Plus Project AM and PM peak hour conditions. However, this intersection is not projected to meet peak hour signal warrants under any study scenarios (see **Appendix C**). Therefore, there would not be a significant adverse effect at the SR 113 & I-80 Ramps/Auction Lane intersection.

The remaining study intersections are projected to operate at acceptable LOS (LOS "D" or better) under all scenarios analyzed.

6. QUEUING ANALYSIS AND IMPROVEMENTS

Vehicle queuing was analyzed for the study intersections. **Table 6** shows the available storage lengths and 95th percentile queues under all analysis scenarios. As shown in **Table 6**, the following queues are projected to exceed storage length:

SR 113 & North Lincoln Street/Vaughn Road:

- SBT – Near-Term Plus Project PM peak hour
- EBL – Near-Term PM peak hour, Near-Term Plus Project AM and PM peak hour

SR 113 & Regency Parkway/Industrial Way:

- NBT – Existing, Near-Term, and Near-Term Plus Project AM and PM peak hour
- SBT – Near-Term Plus Project PM peak hour

It is recommended to adjust the signal timings to provide additional green time at SR 113 & North Lincoln Street/Vaughn Road intersection for the eastbound left-turn and southbound-through movements, and at the SR 113 & Regency Parkway/Industrial Way intersection for the southbound through movement. Synchro output sheets with adjusted signal timings and the resulting improved operations are included in **Appendix B**.

The northbound through 95th percentile queue at the SR 113 & Regency Parkway/Industrial Way intersection blocks the adjacent left-turn pocket under all study conditions, and the Project adds up to five (5) feet of queueing over Near-Term conditions. Signal timing adjustments are not projected to significantly shorten this queue. There is no room to extend the existing northbound left-turn pocket at SR 113 & Regency Parkway/Industrial Way because it is currently back-to-back with another left-turn pocket directly to the south. There is no feasible improvement that can be recommended at this location. Therefore, there would be a significant adverse effect on the northbound queueing of SR 113 & Regency Parkway/Industrial Way that cannot be addressed.

The outbound queues for the proposed Project driveways were analyzed to determine if right turn only lanes should be considered. The queues shown in **Table 6** indicate the outbound queues at the Project driveways are anticipated to be one (1) vehicle or less. Therefore, additional right turn only lanes at the Project driveways are not recommended.

Table 6. Queuing Analysis Results

| Intersection | Movement | Storage (ft) ¹ | Control Type | Peak Hour | 95 th Percentile Queue (ft) | | |
|---|----------|---------------------------|-------------------|-----------|--|----------------------|-----------------------------------|
| | | | | | Existing Conditions | Near-Term Conditions | Near-Term Plus Project Conditions |
| #1, SR 113 & I-80 Ramps/Auction Lane | NBL | 425 | TWSC ² | AM | 8 | 10 | 12 |
| | | | | PM | 18 | 22 | 24 |
| | NBT | 495 | | AM | 0 | 0 | 0 |
| | | | | PM | 0 | 0 | 0 |
| | EBTL | 130 | | AM | 2 | 4 | 4 |
| | | | | PM | 4 | 6 | 6 |
| #2, SR 113 & Dorset Drive | NBL | 200 | Signal | AM | 126 | 150 | 153 |
| | | | | PM | 141 | 161 | 161 |
| | NBT | 270 | | AM | 217 | 218 | 235 |
| | | | | PM | 237 | 252 | 264 |
| | NBR | 320 | | AM | 38 | 43 | 44 |
| | | | | PM | 51 | 54 | 56 |
| | SBL | 235 | | AM | 50 | 63 | 64 |
| | | | | PM | 94 | 100 | 100 |
| | SBT | 305 | | AM | 184 | 201 | 206 |
| | | | | PM | 197 | 191 | 207 |
| | SBR | 135 | | AM | 16 | 36 | 36 |
| | | | | PM | 45 | 49 | 49 |
| | EBL | 150 | | AM | 43 | 45 | 46 |
| | | | | PM | 67 | 80 | 81 |
| | EBT | 220 | | AM | 20 | 21 | 22 |
| | | | | PM | 14 | 19 | 19 |
| | EBR | 160 | | AM | 0 | 0 | 0 |
| | | | | PM | 15 | 36 | 36 |
| | WBL | 275 | | AM | 46 | 52 | 54 |
| | | | | PM | 117 | 135 | 140 |
| | WBT | 265 | | AM | 11 | 13 | 13 |
| | | | | PM | 23 | 26 | 26 |
| | WBR | 195 | | AM | 0 | 0 | 0 |
| | | | | PM | 41 | 44 | 43 |
| #3, SR 113 & North Lincoln Street/Vaughn Road | NBL | 290 | Signal | AM | 58 | 134 | 134 |
| | | | | PM | 101 | 164 | 164 |
| | NBT | 360 | | AM | 217 | 24 | 235 |
| | | | | PM | 243 | 243 | 251 |
| | SBL | 285 | | AM | 101 | 101 | 101 |
| | | | | PM | 91 | 101 | 101 |
| | SBT | 355 | | AM | 173 | 205 | 213 |
| | | | | PM | 283 | 345 | 384 |
| | EBL | 275 | | AM | 130 | 287 | 350 |
| | | | | PM | 141 | 305 | 347 |
| | EBT | 345 | | AM | 33 | 62 | 62 |
| | | | | PM | 38 | 53 | 53 |
| | EBR | 770 | | AM | 0 | 0 | 0 |
| | | | | PM | 16 | 22 | 22 |

| Intersection | Movement | Storage (ft) ¹ | Control Type | Peak Hour | 95 th Percentile Queue (ft) | | |
|---|----------|---------------------------|-------------------|-----------|--|----------------------|-----------------------------------|
| | | | | | Existing Conditions | Near-Term Conditions | Near-Term Plus Project Conditions |
| #3, SR 113 & North Lincoln Street/Vaughn Road (cont.) | WBL | 180 | Signal | AM | 85 | 131 | 133 |
| | | | | PM | 117 | 145 | 145 |
| | WBT | 250 | | AM | 43 | 38 | 38 |
| | | | | PM | 57 | 63 | 63 |
| | WBR | 230 | | AM | 2 | 4 | 4 |
| | | | | PM | 20 | 23 | 23 |
| #4, SR 113 & Regency Parkway/Industrial Way | NBL | 115 | Signal | AM | 46 | 47 | 47 |
| | | | | PM | 57 | 50 | 50 |
| | NBT | 185 | | AM | 203 | 245 | 246 |
| | | | | PM | 212 | 228 | 233 |
| | SBL | 190 | | AM | 67 | 81 | 81 |
| | | | | PM | 38 | 53 | 53 |
| | SBT | 260 | | AM | 141 | 146 | 150 |
| | | | | PM | 252 | 258 | 262 |
| | EBL | 150 | | AM | 47 | 49 | 49 |
| | | | | PM | 39 | 39 | 39 |
| | EBTR | 315 | | AM | 31 | 32 | 32 |
| | | | | PM | 23 | 23 | 23 |
| | WBL | 250 | | AM | 38 | 39 | 39 |
| | | | | PM | 66 | 70 | 70 |
| WBTR | 390 | AM | 17 | 18 | 18 | | |
| | | PM | 32 | 31 | 31 | | |
| #5, Project Driveway 1 & North Lincoln Street | NBR | 75 | OWSC ³ | AM | - | - | 2 |
| | | | | PM | - | - | 2 |
| #6, SR 113 & Project Driveway 2 | EBLR | 145 | OWSC ³ | AM | - | - | 8 |
| | | | | PM | - | - | 6 |
| Notes: | | | | | | | |
| ¹ Storage length for through movements is noted as distance that the queue may extend before blocking the left-turn pocket. This distance is defined as corresponding left-turn pocket length plus approximate taper length (70-feet). | | | | | | | |
| ² TWSC = Two-Way Stop-Controlled | | | | | | | |
| ³ OWSC = One-Way Stop-Controlled | | | | | | | |
| Bold represent queues that exceed existing storage or that may block adjacent turn pockets. | | | | | | | |

7. PROJECT ON-SITE OPERATIONS AND ACCESS EVALUATION

This chapter reviews the proposed Project site plan, including discussion of access driveways and internal circulation.

7.1 PROJECT ACCESS

The Project would gain primary access to the nearby roadway network via one (1) proposed Project driveway on North Lincoln Street and via one (1) proposed Project driveway on SR 113. The two (2) proposed Project driveways are described in detail below:

- Project Driveway 1 on North Lincoln Street: This driveway is proposed to be along North Lincoln Street and would provide access to the residential homes within the Project. The driveway would only allow right-in/right-out movements.
- Project Driveway 2 on SR 113: This driveway is proposed to be along SR 113 and would provide access to the residential homes within the Project. The driveway would allow all movements.

The following discussion on driveway spacing includes measurements taken from the centerlines of the Project Driveways and the proposed gas station driveways (proposed under a separate project) on North Lincoln Street and SR 113. The Project Driveway and the gas station driveway along North Lincoln Street (designated as a minor arterial/major collector) are approximately 220-feet apart. The Project Driveway and gas station driveway along SR 113 (designated as an arterial) are approximately 860-feet apart. All of the driveways except for the Project Driveway on SR 113 would only allow right-in/right-out movements which would limit conflicting movements between the driveways. The proposed driveway spacing is considered adequate.

Based on the site plan shown in **Figure 2**, it appears that emergency vehicles would have sufficient access throughout the Project site. Thus, emergency access to the project is considered adequate.

7.1.1 Project Driveway Sight Distance

Sight distance for egress vehicles at Project Driveway 1 at North Lincoln Street was evaluated based on Figure 3-3A of the City of Dixon 2022 Engineering Design Standards, which indicates a required sight distance of 250 feet for 35 mph roadways.

Corner sight distance for egress vehicles at Project Driveway 2 at SR 113 was evaluated based on Chapter 400 of the Caltrans Highway Design Manual (HDM), which indicates a required corner sight distance of 478 feet for roadways with 50 mph design speeds. Sight distances for the Project Driveways are illustrated in **Appendix E** and are summarized in **Table 7**. Note that only corner sight distance to the left for Project Driveway 2 was checked, as vehicles making a left-turn egress movement would be able to utilize the two-way left-turn lane on SR 113 to make a two-stage left turn out of the driveway.

As shown in **Table 7**, sight distance at both Project Driveways is projected to meet or exceed City and Caltrans requirements.

Table 7. Project Driveways Sight Distance

| Driveway | Speed of Major Road | Required Sight Distance ¹ | Available Sight Distance ² | Sight Distance Met? ² |
|---|---------------------|--------------------------------------|---------------------------------------|----------------------------------|
| Project Driveway 1 at North Lincoln Street | 35 mph | 250' | 250'+ | Yes |
| Project Driveway 2 at SR 113 | 50 mph | 478' | 478'+ | Yes |
| <p><i>Notes:</i> ¹ Required sight distance for Driveway 1 based on Figure 3-3A of the City of Dixon 2022 Engineering Design Standards for a 35 mph posted speed. Required corner sight distance for Driveway 2 based on Chapter 400 of the Caltrans HDM for a design speed of 50 mph ($1.47V_m T_g = 1.47 * 50 * 6.5 = 478'$). ² For Driveway 1, sight distance is measured 15 feet from edge of traveled way and 3 feet to the right of Driveway centerline, per City of Dixon 2022 Engineering Design Standards. For Driveway 2, sight distance is measured 10 feet from edge of traveled way per HDM.</p> | | | | |

7.2 INTERNAL CIRCULATION

Internal circulation within the Project site would occur on bi-directional internal drive aisles, as depicted in **Figure 2**. Pedestrians could use the proposed sidewalks/walkways to be located throughout the Project site to access on-site amenities like the pool, fitness center, dog park, and mail box. Where no direct walkways are proposed, pedestrians could share the low-speed drive aisles with vehicles. Project internal circulation is adequate, and no improvements are recommended.

7.3 EXTERNAL CIRCULATION

There are no proposed pedestrian path connections between the Project and directly adjacent parcels. Bicycles would access the surrounding Class II Bicycle Lane network on SR 113 and North Lincoln Street directly from the Project site. The Project would construct pedestrian sidewalks along Project frontage on SR 113 and North Lincoln Street.

Pedestrians could access Gretchen Higgins Elementary School from the Project site via two main paths:

- Via Project Driveway 1 (approximately 0.76 miles long): turn left on North Lincoln Street, left on Regency Parkway, and right on Pembroke Way. This connection includes sidewalks, curb ramps, and bicycle lanes along the entire route.
- Via Project Driveway 2 (approximately 0.63 miles): turn right on SR 113, right on the pedestrian path (located 350 feet north of Regency Parkway). This connection includes sidewalks, curb ramps, and bicycle lanes/paths along the entire route.

8. SAFETY EVALUATION

The Interim Local Development Intergovernmental Review (LDIGR) Safety Review Practitioners Guidance (Caltrans, December 18, 2020) establishes the safety review expectations for proposed land use projects that would affect Caltrans facilities in the context of the California Environmental Quality Act (CEQA) review process. LDIGR guidelines consist of a traffic safety review, including collision analysis. This section provides an evaluation of LDIGR components at the study intersections with Caltrans facilities (SR 113 & I-80 Ramps/Auction Lane intersection but also SR 113 with Dorset Drive, North Lincoln Street/Vaughn Road, and Regency Parkway/Industrial Way).

Five years of crash data (January 1, 2018 – December 31, 2022) were obtained from the Statewide Integrated Traffic Records System (SWITRS) to identify high collision locations and common collision characteristics. SWITRS collision data is included in **Appendix F**.

Table 8 summarizes the collisions in the study area and describes the collision severity (fatal, serious injury, other visible injury, complaint of pain, and property damage (PDO)) and the collision type (broadside, sideswipe, rear-end, head-on, hit object, and other/not stated). The SWITRS data indicated that a total 28 collisions occurred at the study facilities over the last five years. The severity of most collisions involved PDO, followed by complaint of pain. The most common collision types were rear-end collisions, followed by sideswipe type collisions.

Table 8. Summary of Collision Severity and Type in Study Area (SWITRS, 2018 – 2022)

| Intersection | Total Collisions | Severity | | | | | Type | | | | | |
|---|------------------|----------|----------------|----------------------|-------------------|-----------|----------|-----------|-----------|-----------|------------|------------------|
| | | Fatal | Serious Injury | Other Visible Injury | Complaint of Pain | PDO | Head-On | Sideswipe | Rear-End | Broadside | Hit Object | Other/Not Stated |
| SR 113 & I-80 Ramps/Auction Lane | 5 | 0 | 0 | 0 | 2 | 3 | 2 | 0 | 1 | 1 | 0 | 1 |
| SR 113 & Dorset Drive | 12 | 0 | 0 | 0 | 3 | 9 | 1 | 3 | 4 | 3 | 1 | 0 |
| SR 113 & North Lincoln Street/Vaughn Road | 10 | 0 | 0 | 0 | 1 | 9 | 1 | 3 | 5 | 0 | 0 | 1 |
| SR 113 & Regency Parkway/Industrial Way | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 |
| Totals | 28 | 0 | 0 | 0 | 6 | 22 | 4 | 6 | 11 | 4 | 1 | 2 |

Table 9 shows the primary collision factors (PCFs) at each study intersection. The most common PCFs were unsafe speed, followed by automobile right-of-way and improper turning. It is unlikely that the addition of Project traffic would contribute to an increased collision rate at the study facilities.

Table 9. Summary of Primary Collision Factors in Study Area (SWITRS, 2018 – 2022)

| Intersection | Total Collisions | PCF | | | | | | | | |
|---|------------------|--------------|-----------------------|------------------|------------------|-------------------------|---------------------------|----------------------------|------------------------|----------|
| | | Unsafe Speed | Following Too Closely | Improper Passing | Improper Turning | Automobile Right of Way | Traffic Signals and Signs | Unsafe Starting or Backing | Other Improper Driving | Unknown |
| SR 113 & I-80 Ramps/Auction Lane | 5 | 1 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 |
| SR 113 & Dorset Drive | 12 | 3 | 0 | 1 | 2 | 3 | 2 | 0 | 1 | 0 |
| SR 113 & North Lincoln Street/Vaughn Road | 10 | 3 | 1 | 0 | 2 | 1 | 1 | 1 | 0 | 1 |
| SR 113 & Regency Parkway/Industrial Way | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Totals | 28 | 8 | 1 | 1 | 5 | 7 | 3 | 1 | 1 | 1 |

9. ADVERSE EFFECTS ON BICYCLE AND PEDESTRIAN FACILITIES

This section discusses projected Project effects on study area bicycle and pedestrian facilities. This section also identifies planned bicycle and pedestrian facility improvements in the study area.

9.1 PROJECT EFFECTS ON PEDESTRIAN AND BICYCLE FACILITIES

9.1.1 Effects on Existing Facilities

The Project is not anticipated to cause a significant increase in pedestrian or bicycle demand in the study area that would put existing facilities over capacity. The Project would not adversely affect existing or proposed pedestrian and bicycle facilities in a way that would discourage their use.

9.1.2 Effects on Planned Improvements

The 2020 Solano County Active Transportation Plan (ATP) and City of Dixon Streets Master Plan (2021) identifies proposed improvements to the bicycle network and pedestrian network in the study area. The ATP proposes a project to upgrade the bicycle facilities along SR 113. Specifically, along SR 113, between East C Street and Dorset Drive, the ATP recommends upgrading the existing Class II bicycle lanes to Class IV separated bikeways and constructing Class IV separated bikeways between Dorset Drive and the I-80 Ramps. The ATP also proposes a project to upgrade the existing Class II bicycle lanes to Class II buffered bicycle lanes along North Lincoln Street/Vaughn Drive, between Moore Drive and Pedrick Road. Furthermore, the ATP proposes a project to construct a Class IV separated bikeway between North Lincoln Street and Pedrick Road. The Class IV separated bikeway would run adjacent and parallel to I-80, on the southern side of the freeway. In terms of pedestrian projects, the Plan identifies a sidewalk gap closure project on Vaughn Road, just east of SR 113. The Project would not interfere with the implementation any of the proposed bikeway or pedestrian projects outlined in the Solano County Active Transportation Plan or Dixon General Plan. Note that if a raised cycle track Class IV Bikeway is implemented by the City along SR 113, future modification to the Project Driveways may be required.

9.1.3 Project Access

As discussed in Sections 7.2 and 7.3, there would be adequate pedestrian and bicycle access to and

from the Project along North Lincoln Road and SR 113. At the proposed Project driveways, Project would provide direct connections to existing sidewalks and Class II bicycle lanes.

9.1.4 Project Pedestrian and Bicycle Adverse Effects

The Project would not eliminate or adversely affect an existing bikeway or pedestrian facility in a way that would discourage its use. The Project would not interfere with the implementation of a planned bikeway as shown in the General Plan. Furthermore, the Project would not provide inadequate access for bicyclists and pedestrians, that would result in unsafe conditions, including unsafe bicycle/pedestrian, bicycle/motor vehicle, or pedestrian/motor vehicle conflicts. The Project would provide adequate access for bicyclists and pedestrians, as described above. Therefore, the project is not anticipated to have any significant adverse effects on bicycle or pedestrian facilities.

10. VMT ANALYSIS

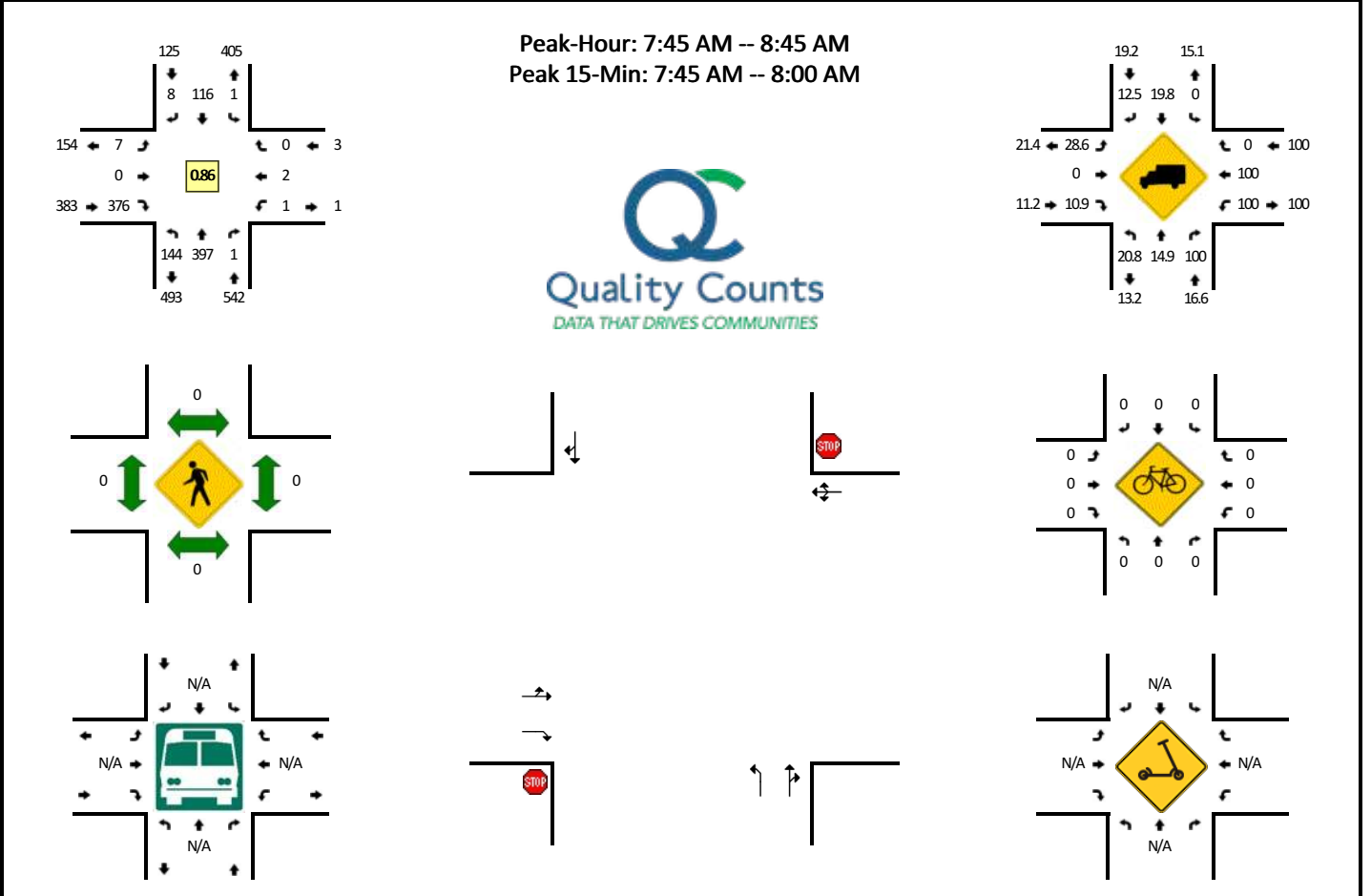
VMT analysis was performed for the Project site by DKS Associates utilizing the City's TDM. Project home-based VMT per capita was found to be 16, which falls below the City threshold of significance of 18.5 VMT per capita, as reported to City staff by DKS via email on May 30, 2023. Therefore, the Project can be assumed to have less than significant VMT impacts.

Appendix A

Traffic Count Data

LOCATION: #1 N 1st St/SR 113 -- I-80 Ramps/Auction Ln
CITY/STATE: Dixon, CA

QC JOB #: 15676001
DATE: Wed, Jan 12 2022

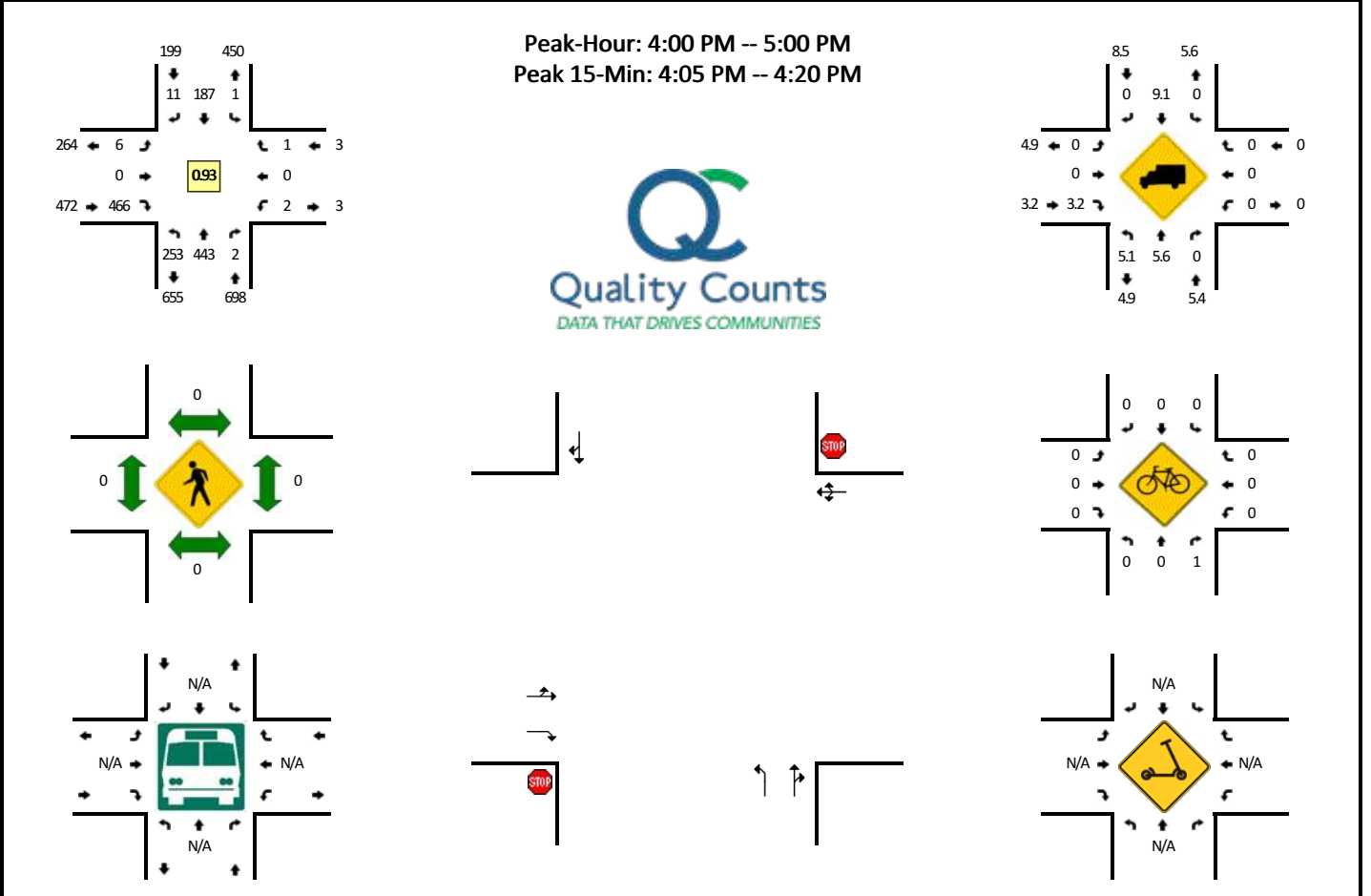


| 5-Min Count Period Beginning At | #1 N 1st St/SR 113 (Northbound) | | | | #1 N 1st St/SR 113 (Southbound) | | | | I-80 Ramps/Auction Ln (Eastbound) | | | | I-80 Ramps/Auction Ln (Westbound) | | | | Total | Hourly Totals |
|---------------------------------|---------------------------------|------|-------|---|---------------------------------|------|-------|---|-----------------------------------|------|-------|----|-----------------------------------|------|-------|---|-------|---------------|
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| 7:00 AM | 8 | 24 | 0 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 37 | 0 | 0 | 0 | 0 | 85 | |
| 7:05 AM | 14 | 27 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 25 | 0 | 0 | 0 | 0 | 76 | |
| 7:10 AM | 13 | 23 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 31 | 0 | 0 | 0 | 0 | 76 | |
| 7:15 AM | 9 | 34 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 87 | |
| 7:20 AM | 5 | 26 | 0 | 0 | 0 | 5 | 2 | 0 | 0 | 1 | 0 | 32 | 0 | 0 | 0 | 0 | 71 | |
| 7:25 AM | 10 | 21 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 1 | 0 | 33 | 0 | 0 | 0 | 0 | 77 | |
| 7:30 AM | 5 | 26 | 0 | 0 | 0 | 18 | 0 | 0 | 0 | 2 | 0 | 26 | 0 | 0 | 0 | 0 | 77 | |
| 7:35 AM | 12 | 28 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 74 | |
| 7:40 AM | 14 | 33 | 0 | 0 | 0 | 14 | 2 | 0 | 0 | 0 | 0 | 38 | 0 | 0 | 0 | 0 | 101 | |
| 7:45 AM | 13 | 44 | 0 | 0 | 0 | 11 | 1 | 1 | 0 | 1 | 0 | 41 | 0 | 0 | 0 | 0 | 112 | |
| 7:50 AM | 15 | 29 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 1 | 0 | 37 | 0 | 0 | 0 | 0 | 90 | |
| 7:55 AM | 14 | 36 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 2 | 0 | 39 | 0 | 1 | 0 | 0 | 103 | 1029 |
| 8:00 AM | 7 | 33 | 0 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 30 | 0 | 0 | 1 | 0 | 83 | 1027 |
| 8:05 AM | 8 | 32 | 1 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 27 | 0 | 0 | 0 | 0 | 77 | 1028 |
| 8:10 AM | 8 | 33 | 0 | 0 | 0 | 13 | 1 | 0 | 0 | 1 | 0 | 20 | 0 | 0 | 1 | 0 | 77 | 1029 |
| 8:15 AM | 12 | 31 | 0 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 72 | 1014 |
| 8:20 AM | 14 | 28 | 0 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 27 | 0 | 0 | 0 | 0 | 80 | 1023 |
| 8:25 AM | 10 | 39 | 0 | 0 | 0 | 7 | 2 | 0 | 0 | 0 | 0 | 32 | 0 | 0 | 0 | 0 | 90 | 1036 |
| 8:30 AM | 10 | 22 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 1 | 0 | 36 | 0 | 0 | 0 | 0 | 78 | 1037 |
| 8:35 AM | 15 | 29 | 0 | 0 | 0 | 10 | 1 | 0 | 0 | 1 | 0 | 32 | 0 | 0 | 0 | 0 | 88 | 1051 |
| 8:40 AM | 18 | 41 | 0 | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 35 | 0 | 0 | 0 | 0 | 103 | 1053 |
| 8:45 AM | 7 | 27 | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 1 | 0 | 34 | 0 | 0 | 0 | 0 | 83 | 1024 |
| 8:50 AM | 19 | 18 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 0 | 0 | 0 | 67 | 1001 |
| 8:55 AM | 8 | 19 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 2 | 0 | 33 | 0 | 0 | 0 | 0 | 72 | 970 |
| Peak 15-Min Flowrates | Northbound | | | | Southbound | | | | Eastbound | | | | Westbound | | | | Total | |
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| All Vehicles | 168 | 436 | 0 | 0 | 0 | 120 | 4 | 4 | 16 | 0 | 468 | 0 | 4 | 0 | 0 | 0 | 1220 | |
| Heavy Trucks | 52 | 48 | 0 | 0 | 0 | 16 | 0 | 0 | 8 | 0 | 36 | 0 | 4 | 0 | 0 | 0 | 164 | |
| Buses | | | | | | | | | | | | | | | | | 0 | |
| Pedestrians | | 0 | | | | 0 | | | | 0 | | | | 0 | | | 0 | |
| Bicycles | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | |
| Scoters | | | | | | | | | | | | | | | | | 0 | |

Comments:

LOCATION: #1 N 1st St/SR 113 -- I-80 Ramps/Auction Ln
CITY/STATE: Dixon, CA

QC JOB #: 15676002
DATE: Wed, Jan 12 2022

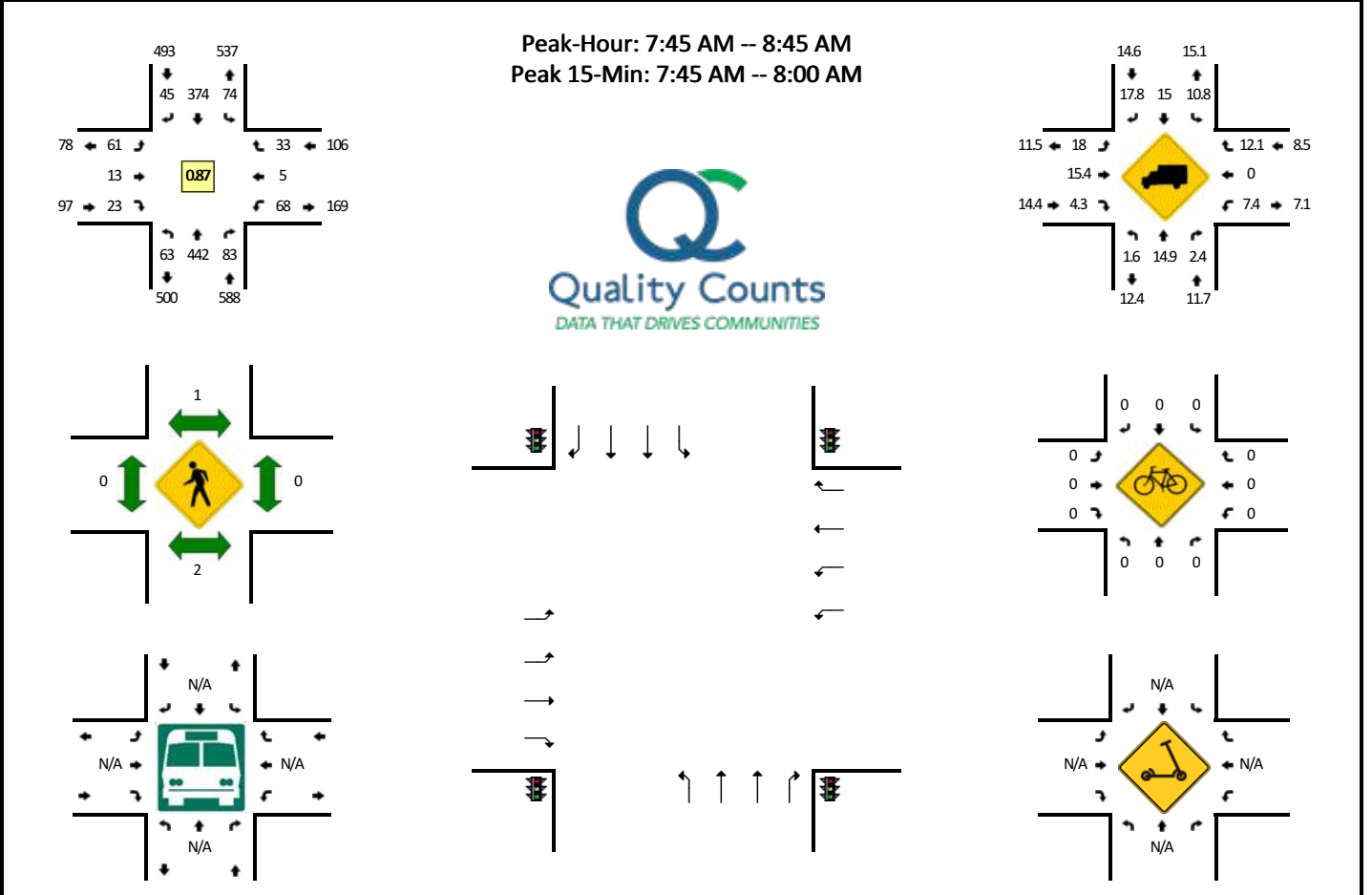


| 5-Min Count Period Beginning At | #1 N 1st St/SR 113 (Northbound) | | | | #1 N 1st St/SR 113 (Southbound) | | | | I-80 Ramps/Auction Ln (Eastbound) | | | | I-80 Ramps/Auction Ln (Westbound) | | | | Total | Hourly Totals |
|---------------------------------|---------------------------------|------|-------|---|---------------------------------|------|-------|---|-----------------------------------|------|-------|---|-----------------------------------|------|-------|---|-------|---------------|
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| 4:00 PM | 24 | 42 | 0 | 0 | 0 | 18 | 0 | 0 | 1 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 128 | |
| 4:05 PM | 26 | 50 | 0 | 0 | 0 | 17 | 1 | 0 | 0 | 0 | 31 | 0 | 0 | 0 | 0 | 0 | 125 | |
| 4:10 PM | 20 | 43 | 1 | 0 | 0 | 11 | 0 | 0 | 1 | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 112 | |
| 4:15 PM | 27 | 38 | 0 | 0 | 0 | 18 | 2 | 0 | 0 | 0 | 44 | 0 | 1 | 0 | 0 | 0 | 130 | |
| 4:20 PM | 19 | 34 | 0 | 0 | 1 | 16 | 0 | 0 | 1 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 108 | |
| 4:25 PM | 16 | 43 | 0 | 0 | 0 | 21 | 1 | 0 | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 114 | |
| 4:30 PM | 21 | 29 | 0 | 0 | 0 | 11 | 1 | 0 | 0 | 0 | 31 | 0 | 0 | 0 | 1 | 0 | 94 | |
| 4:35 PM | 25 | 39 | 0 | 0 | 0 | 11 | 0 | 0 | 1 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 109 | |
| 4:40 PM | 18 | 31 | 0 | 0 | 0 | 15 | 1 | 0 | 1 | 0 | 39 | 0 | 0 | 0 | 0 | 0 | 105 | |
| 4:45 PM | 19 | 19 | 1 | 0 | 0 | 18 | 3 | 0 | 0 | 0 | 44 | 0 | 1 | 0 | 0 | 0 | 105 | |
| 4:50 PM | 11 | 41 | 0 | 0 | 0 | 18 | 1 | 0 | 0 | 0 | 56 | 0 | 0 | 0 | 0 | 0 | 127 | |
| 4:55 PM | 27 | 34 | 0 | 0 | 0 | 13 | 1 | 0 | 1 | 0 | 39 | 0 | 0 | 0 | 0 | 0 | 115 | 1372 |
| 5:00 PM | 25 | 28 | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 34 | 0 | 0 | 0 | 0 | 0 | 101 | 1345 |
| 5:05 PM | 18 | 41 | 0 | 0 | 0 | 14 | 0 | 0 | 3 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 101 | 1321 |
| 5:10 PM | 12 | 42 | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 110 | 1319 |
| 5:15 PM | 20 | 30 | 1 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 37 | 0 | 1 | 0 | 0 | 0 | 101 | 1290 |
| 5:20 PM | 24 | 33 | 1 | 0 | 0 | 20 | 0 | 0 | 3 | 0 | 56 | 0 | 1 | 0 | 0 | 0 | 138 | 1320 |
| 5:25 PM | 21 | 35 | 2 | 0 | 0 | 15 | 1 | 0 | 0 | 0 | 32 | 0 | 0 | 1 | 0 | 0 | 107 | 1313 |
| 5:30 PM | 7 | 30 | 0 | 0 | 0 | 9 | 2 | 0 | 1 | 0 | 40 | 0 | 0 | 0 | 1 | 0 | 90 | 1309 |
| 5:35 PM | 15 | 31 | 2 | 0 | 0 | 19 | 1 | 0 | 1 | 0 | 34 | 0 | 0 | 0 | 0 | 0 | 103 | 1303 |
| 5:40 PM | 18 | 18 | 0 | 0 | 0 | 13 | 2 | 0 | 0 | 0 | 40 | 0 | 0 | 0 | 1 | 0 | 92 | 1290 |
| 5:45 PM | 14 | 23 | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 37 | 0 | 1 | 0 | 0 | 0 | 89 | 1274 |
| 5:50 PM | 17 | 28 | 1 | 0 | 0 | 13 | 1 | 0 | 0 | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 96 | 1243 |
| 5:55 PM | 15 | 24 | 0 | 0 | 0 | 16 | 1 | 0 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 84 | 1212 |
| Peak 15-Min Flowrates | Northbound | | | | Southbound | | | | Eastbound | | | | Westbound | | | | Total | |
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| All Vehicles | 292 | 524 | 4 | 0 | 0 | 184 | 12 | 0 | 4 | 0 | 444 | 0 | 4 | 0 | 0 | 0 | 1468 | |
| Heavy Trucks | 16 | 20 | 0 | | 0 | 20 | 0 | | 0 | 0 | 16 | | 0 | 0 | 0 | | 72 | |
| Buses | | | | | | | | | | | | | | | | | 0 | |
| Pedestrians | | 0 | | | | 0 | | | | 0 | | | | 0 | | | 0 | |
| Bicycles | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | |
| Scoters | | | | | | | | | | | | | | | | | 0 | |

Comments:

LOCATION: #2 N 1st St/SR 113 -- Dorset Drive
CITY/STATE: Dixon, CA

QC JOB #: 15676003
DATE: Wed, Jan 12 2022

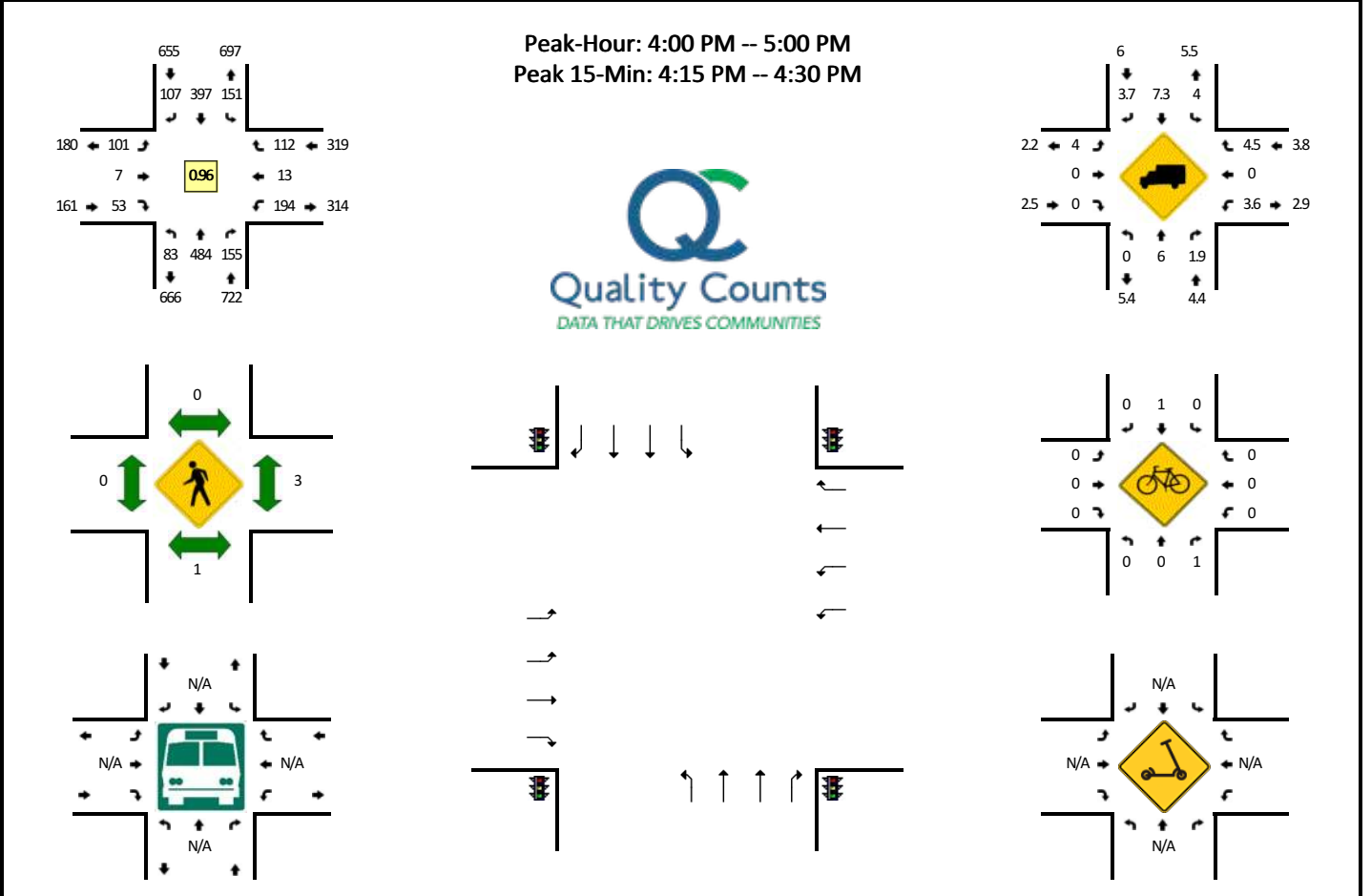


| 5-Min Count Period Beginning At | #2 N 1st St/SR 113 (Northbound) | | | | #2 N 1st St/SR 113 (Southbound) | | | | Dorset Drive (Eastbound) | | | | Dorset Drive (Westbound) | | | | Total | Hourly Totals |
|---------------------------------|---------------------------------|------|-------|----|---------------------------------|------|-------|---|--------------------------|------|-------|---|--------------------------|------|-------|---|-------|---------------|
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| 7:00 AM | 4 | 32 | 4 | 2 | 12 | 35 | 3 | 0 | 1 | 0 | 5 | 0 | 0 | 0 | 3 | 0 | 101 | |
| 7:05 AM | 1 | 27 | 1 | 0 | 6 | 27 | 5 | 0 | 8 | 0 | 1 | 0 | 5 | 0 | 1 | 0 | 82 | |
| 7:10 AM | 0 | 34 | 1 | 4 | 4 | 32 | 3 | 0 | 6 | 3 | 1 | 0 | 2 | 0 | 3 | 0 | 93 | |
| 7:15 AM | 5 | 34 | 2 | 2 | 7 | 36 | 2 | 0 | 1 | 2 | 1 | 0 | 4 | 0 | 2 | 0 | 98 | |
| 7:20 AM | 1 | 28 | 5 | 2 | 5 | 28 | 2 | 0 | 2 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 76 | |
| 7:25 AM | 2 | 25 | 0 | 4 | 7 | 28 | 7 | 0 | 5 | 1 | 1 | 0 | 3 | 0 | 0 | 0 | 83 | |
| 7:30 AM | 4 | 31 | 1 | 8 | 4 | 35 | 5 | 0 | 0 | 3 | 2 | 0 | 3 | 0 | 3 | 0 | 99 | |
| 7:35 AM | 4 | 30 | 3 | 4 | 4 | 31 | 2 | 0 | 11 | 0 | 4 | 0 | 3 | 0 | 3 | 0 | 99 | |
| 7:40 AM | 3 | 33 | 2 | 4 | 8 | 29 | 5 | 0 | 6 | 0 | 3 | 0 | 3 | 0 | 2 | 0 | 98 | |
| 7:45 AM | 3 | 54 | 4 | 2 | 6 | 40 | 6 | 0 | 5 | 1 | 4 | 0 | 8 | 2 | 2 | 0 | 137 | |
| 7:50 AM | 3 | 33 | 3 | 3 | 8 | 41 | 5 | 0 | 7 | 3 | 2 | 0 | 7 | 0 | 3 | 0 | 118 | |
| 7:55 AM | 2 | 37 | 8 | 5 | 4 | 44 | 3 | 0 | 2 | 0 | 2 | 0 | 3 | 1 | 5 | 0 | 116 | 1200 |
| 8:00 AM | 1 | 36 | 0 | 1 | 4 | 32 | 1 | 0 | 4 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 83 | 1182 |
| 8:05 AM | 3 | 36 | 9 | 2 | 5 | 26 | 5 | 1 | 6 | 0 | 2 | 0 | 4 | 1 | 2 | 0 | 102 | 1202 |
| 8:10 AM | 4 | 33 | 10 | 4 | 2 | 25 | 4 | 0 | 3 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 90 | 1199 |
| 8:15 AM | 3 | 33 | 11 | 5 | 3 | 22 | 3 | 0 | 3 | 3 | 0 | 0 | 5 | 0 | 4 | 0 | 95 | 1196 |
| 8:20 AM | 0 | 34 | 7 | 4 | 1 | 30 | 3 | 0 | 4 | 1 | 6 | 0 | 9 | 0 | 4 | 0 | 103 | 1223 |
| 8:25 AM | 1 | 40 | 9 | 2 | 5 | 28 | 5 | 0 | 8 | 0 | 0 | 0 | 5 | 0 | 2 | 0 | 105 | 1245 |
| 8:30 AM | 1 | 28 | 6 | 5 | 13 | 30 | 2 | 0 | 4 | 3 | 3 | 0 | 3 | 1 | 3 | 0 | 102 | 1248 |
| 8:35 AM | 4 | 33 | 4 | 0 | 12 | 31 | 4 | 0 | 6 | 2 | 3 | 0 | 7 | 0 | 3 | 0 | 109 | 1258 |
| 8:40 AM | 3 | 45 | 12 | 2 | 10 | 25 | 4 | 0 | 9 | 0 | 1 | 0 | 9 | 0 | 4 | 0 | 124 | 1284 |
| 8:45 AM | 2 | 26 | 11 | 7 | 12 | 30 | 5 | 0 | 5 | 0 | 0 | 0 | 5 | 2 | 2 | 0 | 107 | 1254 |
| 8:50 AM | 2 | 27 | 5 | 0 | 3 | 28 | 1 | 0 | 8 | 0 | 0 | 0 | 5 | 3 | 2 | 0 | 84 | 1220 |
| 8:55 AM | 4 | 22 | 6 | 4 | 5 | 29 | 4 | 0 | 0 | 2 | 2 | 0 | 9 | 0 | 3 | 0 | 90 | 1194 |
| Peak 15-Min Flowrates | Northbound | | | | Southbound | | | | Eastbound | | | | Westbound | | | | Total | |
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| All Vehicles | 32 | 496 | 60 | 40 | 72 | 500 | 56 | 0 | 56 | 16 | 32 | 0 | 72 | 12 | 40 | 0 | 1484 | |
| Heavy Trucks | 0 | 84 | 8 | | 8 | 44 | 4 | | 8 | 0 | 0 | | 4 | 0 | 0 | | 160 | |
| Buses | | | | | | | | | | | | | | | | | | |
| Pedestrians | | 0 | | | | 4 | | | | 0 | | | | 0 | | | 4 | |
| Bicycles | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | |
| Scoters | | | | | | | | | | | | | | | | | | |

Comments:

LOCATION: #2 N 1st St/SR 113 -- Dorset Drive
CITY/STATE: Dixon, CA

QC JOB #: 15676004
DATE: Wed, Jan 12 2022

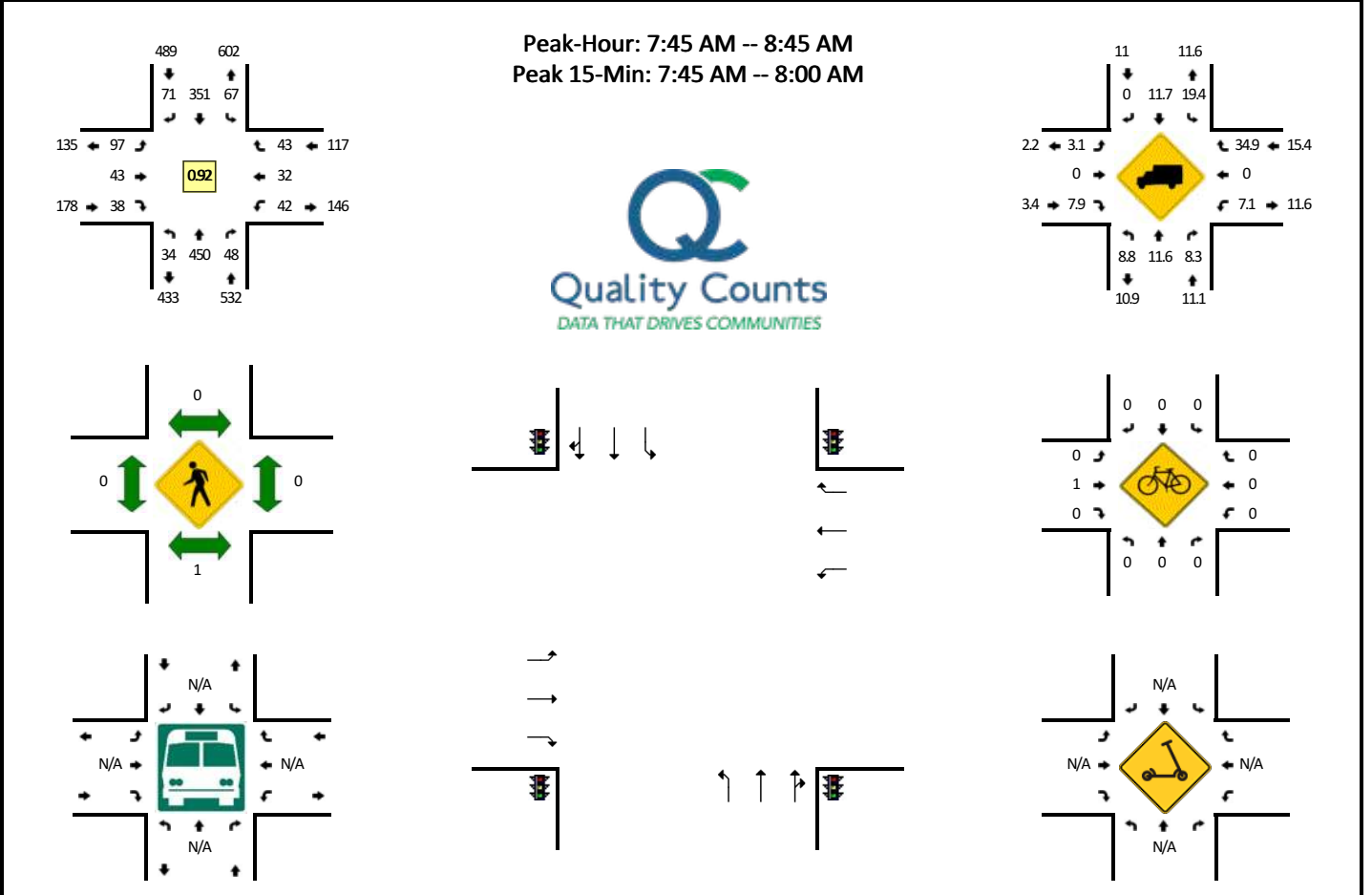


| 5-Min Count Period Beginning At | #2 N 1st St/SR 113 (Northbound) | | | | #2 N 1st St/SR 113 (Southbound) | | | | Dorset Drive (Eastbound) | | | | Dorset Drive (Westbound) | | | | Total | Hourly Totals |
|---------------------------------|---------------------------------|------|-------|----|---------------------------------|------|-------|---|--------------------------|------|-------|---|--------------------------|------|-------|---|-------|---------------|
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| 4:00 PM | 9 | 51 | 10 | 2 | 15 | 41 | 5 | 0 | 8 | 0 | 3 | 0 | 18 | 1 | 11 | 0 | 174 | |
| 4:05 PM | 3 | 53 | 3 | 1 | 14 | 26 | 8 | 0 | 7 | 0 | 6 | 0 | 9 | 0 | 14 | 0 | 144 | |
| 4:10 PM | 5 | 47 | 19 | 5 | 14 | 26 | 7 | 0 | 8 | 0 | 1 | 0 | 17 | 0 | 4 | 1 | 154 | |
| 4:15 PM | 3 | 44 | 16 | 0 | 10 | 33 | 16 | 0 | 11 | 0 | 6 | 0 | 10 | 2 | 9 | 0 | 160 | |
| 4:20 PM | 3 | 36 | 16 | 4 | 10 | 34 | 15 | 0 | 14 | 0 | 5 | 0 | 15 | 0 | 11 | 0 | 163 | |
| 4:25 PM | 10 | 37 | 11 | 1 | 14 | 30 | 10 | 0 | 11 | 3 | 3 | 0 | 19 | 1 | 10 | 0 | 160 | |
| 4:30 PM | 8 | 34 | 12 | 0 | 12 | 27 | 6 | 0 | 9 | 0 | 6 | 0 | 13 | 1 | 9 | 0 | 137 | |
| 4:35 PM | 1 | 45 | 19 | 2 | 11 | 25 | 4 | 0 | 5 | 2 | 2 | 0 | 21 | 4 | 8 | 0 | 149 | |
| 4:40 PM | 2 | 34 | 9 | 2 | 12 | 22 | 11 | 0 | 4 | 0 | 3 | 0 | 28 | 0 | 9 | 0 | 136 | |
| 4:45 PM | 6 | 32 | 13 | 4 | 13 | 47 | 11 | 0 | 9 | 0 | 6 | 0 | 7 | 0 | 6 | 0 | 154 | |
| 4:50 PM | 3 | 34 | 19 | 1 | 18 | 50 | 7 | 0 | 5 | 2 | 4 | 0 | 22 | 3 | 10 | 0 | 178 | |
| 4:55 PM | 7 | 37 | 8 | 1 | 8 | 36 | 7 | 0 | 10 | 0 | 8 | 0 | 14 | 1 | 11 | 0 | 148 | 1857 |
| 5:00 PM | 6 | 35 | 18 | 1 | 8 | 27 | 15 | 1 | 4 | 0 | 7 | 0 | 13 | 1 | 11 | 0 | 147 | 1830 |
| 5:05 PM | 8 | 41 | 15 | 5 | 6 | 17 | 7 | 0 | 15 | 0 | 5 | 0 | 16 | 2 | 7 | 0 | 144 | 1830 |
| 5:10 PM | 2 | 29 | 13 | 5 | 11 | 42 | 11 | 0 | 10 | 1 | 7 | 0 | 19 | 0 | 10 | 1 | 161 | 1837 |
| 5:15 PM | 6 | 38 | 11 | 1 | 4 | 37 | 8 | 0 | 10 | 1 | 4 | 0 | 8 | 1 | 8 | 0 | 137 | 1814 |
| 5:20 PM | 4 | 37 | 19 | 3 | 13 | 40 | 14 | 0 | 8 | 1 | 12 | 0 | 16 | 1 | 9 | 0 | 177 | 1828 |
| 5:25 PM | 13 | 39 | 13 | 0 | 11 | 39 | 10 | 0 | 11 | 2 | 6 | 0 | 10 | 0 | 8 | 0 | 162 | 1830 |
| 5:30 PM | 3 | 25 | 16 | 2 | 6 | 34 | 6 | 0 | 3 | 3 | 6 | 0 | 18 | 3 | 8 | 0 | 133 | 1826 |
| 5:35 PM | 4 | 26 | 11 | 4 | 15 | 31 | 9 | 0 | 10 | 1 | 5 | 0 | 13 | 1 | 9 | 0 | 139 | 1816 |
| 5:40 PM | 4 | 29 | 8 | 1 | 7 | 34 | 10 | 0 | 8 | 2 | 6 | 0 | 14 | 4 | 4 | 1 | 132 | 1812 |
| 5:45 PM | 2 | 15 | 14 | 0 | 10 | 29 | 11 | 0 | 4 | 0 | 6 | 0 | 21 | 1 | 10 | 0 | 123 | 1781 |
| 5:50 PM | 5 | 31 | 16 | 2 | 16 | 23 | 12 | 0 | 11 | 0 | 5 | 0 | 16 | 1 | 7 | 0 | 145 | 1748 |
| 5:55 PM | 7 | 17 | 11 | 5 | 8 | 20 | 17 | 0 | 5 | 1 | 5 | 0 | 13 | 0 | 14 | 0 | 123 | 1723 |
| Peak 15-Min Flowrates | Northbound | | | | Southbound | | | | Eastbound | | | | Westbound | | | | Total | |
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| All Vehicles | 64 | 468 | 172 | 20 | 136 | 388 | 164 | 0 | 144 | 12 | 56 | 0 | 176 | 12 | 120 | 0 | 1932 | |
| Heavy Trucks | 0 | 28 | 4 | | 4 | 32 | 4 | | 8 | 0 | 0 | | 24 | 0 | 8 | | 112 | |
| Buses | | | | | | | | | | | | | | | | | | |
| Pedestrians | | 0 | | | | 0 | | | | 0 | | | | 0 | | | 0 | |
| Bicycles | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | |
| Scoters | | | | | | | | | | | | | | | | | | |

Comments:

LOCATION: #3 N 1st St/SR 113 -- N Lincoln St/Vaughn Rd
CITY/STATE: Dixon, CA

QC JOB #: 15676005
DATE: Wed, Jan 12 2022

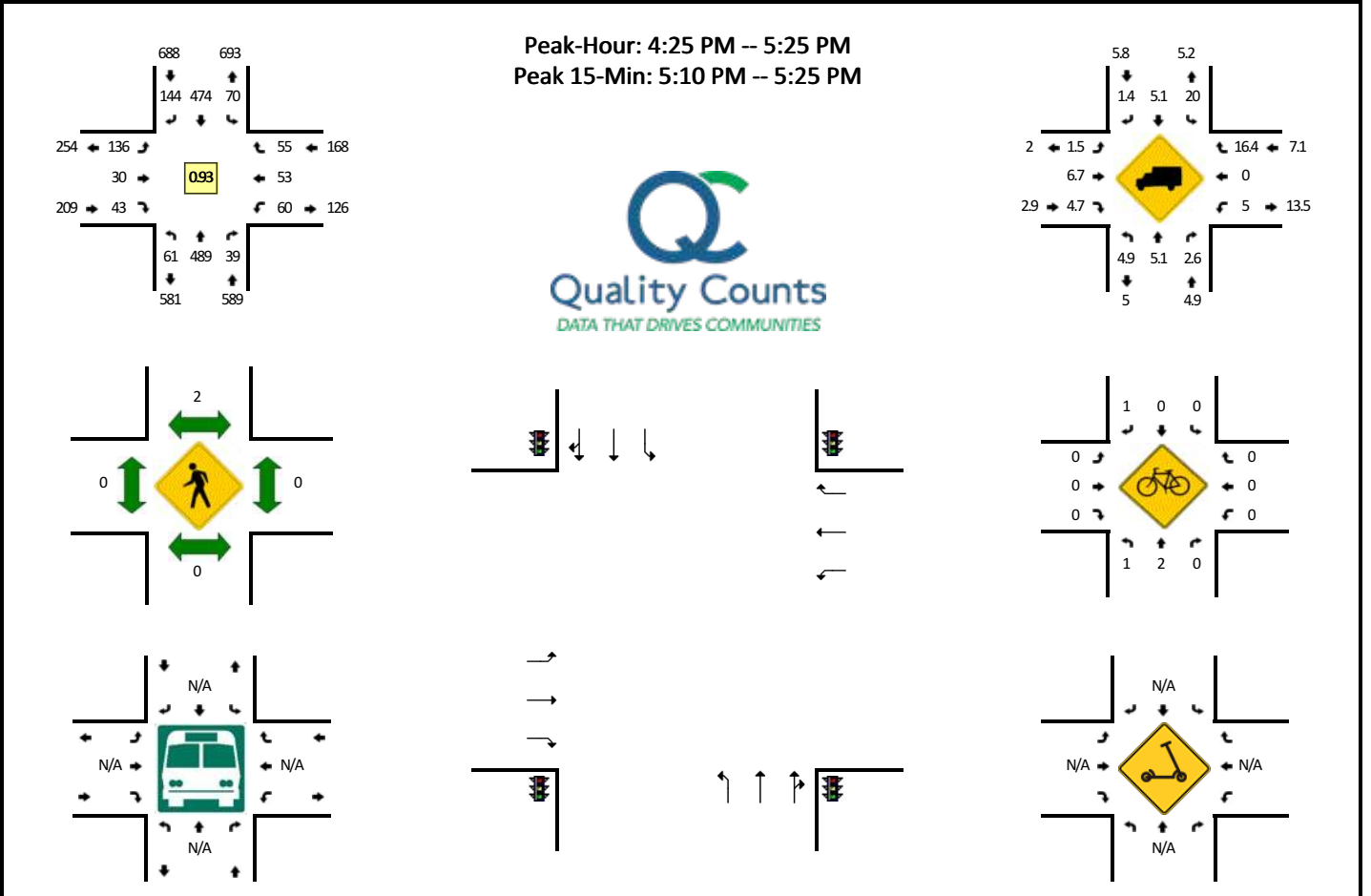


| 5-Min Count Period Beginning At | #3 N 1st St/SR 113 (Northbound) | | | | #3 N 1st St/SR 113 (Southbound) | | | | N Lincoln St/Vaughn Rd (Eastbound) | | | | N Lincoln St/Vaughn Rd (Westbound) | | | | Total | Hourly Totals |
|---------------------------------|---------------------------------|------|-------|---|---------------------------------|------|-------|----|------------------------------------|------|-------|---|------------------------------------|------|-------|---|-------|---------------|
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| 7:00 AM | 1 | 22 | 3 | 0 | 7 | 36 | 4 | 0 | 6 | 6 | 1 | 0 | 3 | 1 | 5 | 0 | 95 | |
| 7:05 AM | 2 | 29 | 2 | 0 | 5 | 20 | 4 | 1 | 5 | 2 | 2 | 0 | 3 | 3 | 3 | 0 | 81 | |
| 7:10 AM | 0 | 27 | 2 | 0 | 3 | 26 | 4 | 1 | 5 | 1 | 1 | 0 | 2 | 0 | 7 | 0 | 79 | |
| 7:15 AM | 0 | 21 | 1 | 0 | 2 | 33 | 6 | 1 | 9 | 2 | 3 | 0 | 2 | 2 | 4 | 0 | 86 | |
| 7:20 AM | 2 | 26 | 3 | 0 | 4 | 19 | 3 | 0 | 4 | 4 | 1 | 0 | 2 | 0 | 1 | 0 | 69 | |
| 7:25 AM | 2 | 21 | 1 | 0 | 7 | 32 | 7 | 0 | 9 | 0 | 1 | 0 | 2 | 3 | 5 | 0 | 90 | |
| 7:30 AM | 1 | 32 | 2 | 0 | 14 | 17 | 6 | 0 | 10 | 0 | 2 | 0 | 4 | 2 | 2 | 0 | 92 | |
| 7:35 AM | 2 | 29 | 0 | 0 | 7 | 28 | 8 | 0 | 10 | 1 | 1 | 0 | 3 | 3 | 1 | 0 | 93 | |
| 7:40 AM | 2 | 27 | 4 | 0 | 3 | 28 | 6 | 1 | 2 | 1 | 4 | 0 | 0 | 2 | 3 | 0 | 83 | |
| 7:45 AM | 1 | 45 | 3 | 1 | 4 | 37 | 12 | 1 | 13 | 5 | 2 | 0 | 2 | 4 | 7 | 0 | 137 | |
| 7:50 AM | 0 | 30 | 4 | 0 | 10 | 35 | 7 | 3 | 7 | 3 | 3 | 0 | 1 | 1 | 8 | 0 | 112 | |
| 7:55 AM | 2 | 26 | 3 | 0 | 5 | 42 | 5 | 1 | 9 | 3 | 4 | 0 | 6 | 2 | 1 | 0 | 109 | 1126 |
| 8:00 AM | 1 | 35 | 0 | 0 | 5 | 27 | 5 | 1 | 7 | 3 | 3 | 0 | 2 | 2 | 0 | 0 | 91 | 1122 |
| 8:05 AM | 3 | 43 | 5 | 0 | 1 | 25 | 5 | 1 | 8 | 7 | 1 | 0 | 2 | 5 | 4 | 0 | 110 | 1151 |
| 8:10 AM | 2 | 31 | 5 | 0 | 3 | 19 | 4 | 0 | 7 | 2 | 5 | 0 | 2 | 2 | 2 | 0 | 84 | 1156 |
| 8:15 AM | 6 | 44 | 6 | 0 | 5 | 24 | 1 | 2 | 8 | 5 | 6 | 0 | 3 | 4 | 1 | 0 | 115 | 1185 |
| 8:20 AM | 4 | 35 | 7 | 0 | 6 | 28 | 9 | 1 | 9 | 9 | 5 | 0 | 5 | 3 | 2 | 0 | 123 | 1239 |
| 8:25 AM | 3 | 42 | 4 | 0 | 5 | 26 | 8 | 1 | 8 | 2 | 2 | 0 | 5 | 3 | 6 | 0 | 115 | 1264 |
| 8:30 AM | 5 | 36 | 6 | 1 | 0 | 27 | 7 | 0 | 4 | 0 | 4 | 0 | 0 | 4 | 5 | 0 | 99 | 1271 |
| 8:35 AM | 3 | 36 | 4 | 0 | 5 | 32 | 6 | 0 | 7 | 3 | 0 | 0 | 8 | 2 | 6 | 0 | 112 | 1290 |
| 8:40 AM | 2 | 47 | 1 | 0 | 6 | 29 | 2 | 1 | 10 | 1 | 3 | 0 | 6 | 0 | 1 | 0 | 109 | 1316 |
| 8:45 AM | 4 | 31 | 1 | 0 | 7 | 34 | 4 | 1 | 10 | 2 | 4 | 0 | 7 | 0 | 2 | 0 | 107 | 1286 |
| 8:50 AM | 1 | 24 | 3 | 0 | 4 | 27 | 2 | 0 | 5 | 4 | 0 | 0 | 3 | 2 | 6 | 0 | 81 | 1255 |
| 8:55 AM | 1 | 17 | 1 | 0 | 4 | 32 | 7 | 0 | 5 | 1 | 0 | 0 | 3 | 2 | 2 | 0 | 75 | 1221 |
| Peak 15-Min Flowrates | Northbound | | | | Southbound | | | | Eastbound | | | | Westbound | | | | Total | |
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| All Vehicles | 12 | 404 | 40 | 4 | 76 | 456 | 96 | 20 | 116 | 44 | 36 | 0 | 36 | 28 | 64 | 0 | 1432 | |
| Heavy Trucks | 0 | 64 | 12 | | 8 | 40 | 0 | | 4 | 0 | 4 | | 4 | 0 | 32 | | 168 | |
| Buses | | | | | | | | | | | | | | | | | | |
| Pedestrians | | 0 | | | | 0 | | | | 0 | | | | 0 | | | 0 | |
| Bicycles | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | |
| Scoters | | | | | | | | | | | | | | | | | | |

Comments:

LOCATION: #3 N 1st St/SR 113 -- N Lincoln St/Vaughn Rd
CITY/STATE: Dixon, CA

QC JOB #: 15676006
DATE: Wed, Jan 12 2022

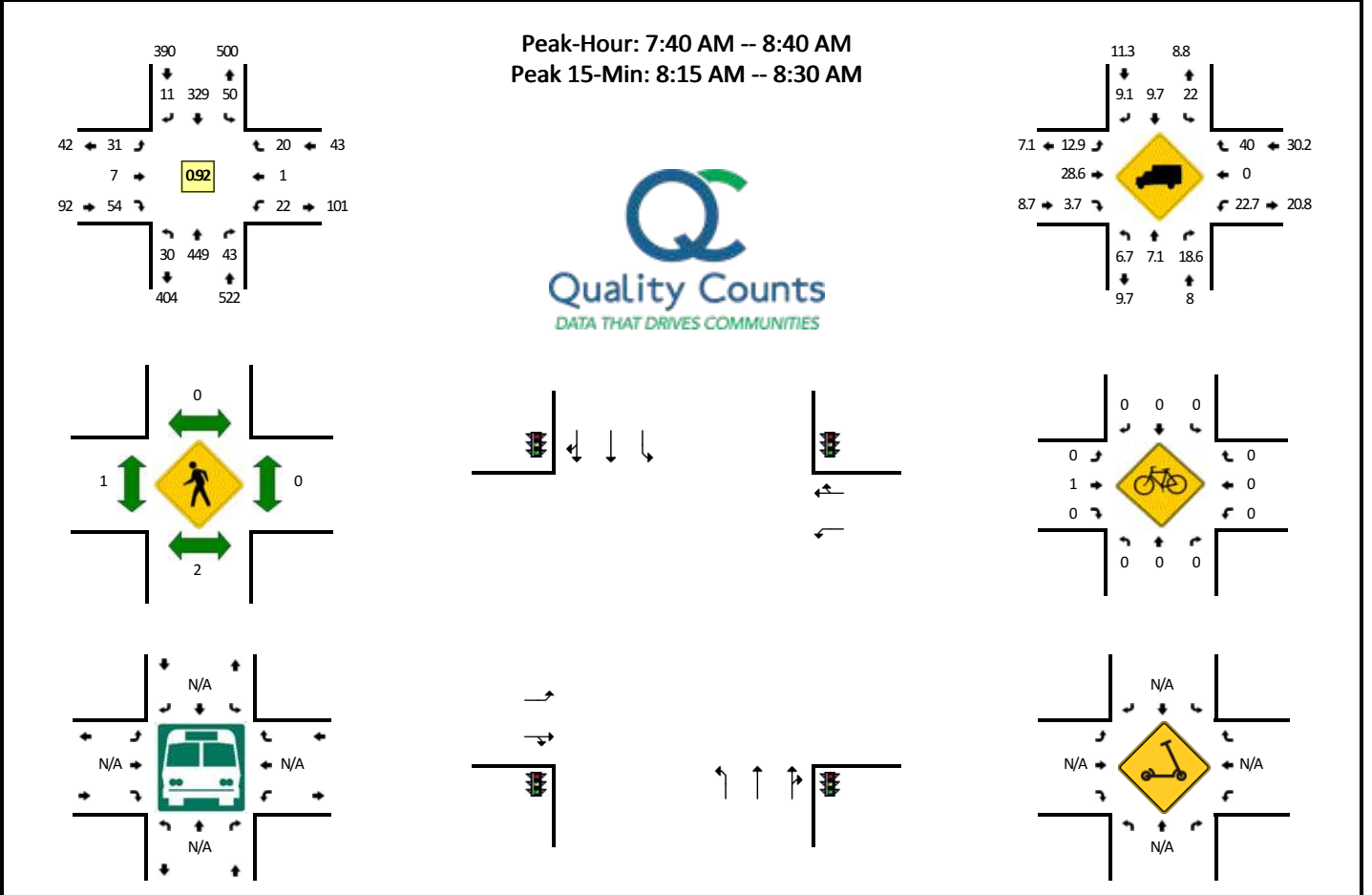


| 5-Min Count Period Beginning At | #3 N 1st St/SR 113 (Northbound) | | | | #3 N 1st St/SR 113 (Southbound) | | | | N Lincoln St/Vaughn Rd (Eastbound) | | | | N Lincoln St/Vaughn Rd (Westbound) | | | | Total | Hourly Totals |
|---------------------------------|---------------------------------|------|-------|---|---------------------------------|------|-------|----|------------------------------------|------|-------|---|------------------------------------|------|-------|---|-------|---------------|
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| 4:00 PM | 4 | 42 | 4 | 0 | 5 | 47 | 14 | 1 | 8 | 1 | 3 | 0 | 7 | 5 | 12 | 0 | 153 | |
| 4:05 PM | 1 | 48 | 6 | 0 | 3 | 30 | 10 | 1 | 12 | 1 | 2 | 0 | 6 | 5 | 16 | 0 | 141 | |
| 4:10 PM | 7 | 36 | 5 | 0 | 4 | 27 | 15 | 2 | 15 | 2 | 1 | 0 | 6 | 3 | 13 | 0 | 136 | |
| 4:15 PM | 5 | 36 | 4 | 0 | 3 | 41 | 8 | 0 | 14 | 2 | 4 | 0 | 5 | 1 | 15 | 0 | 138 | |
| 4:20 PM | 1 | 30 | 2 | 0 | 5 | 36 | 12 | 1 | 15 | 2 | 2 | 0 | 7 | 5 | 4 | 0 | 122 | |
| 4:25 PM | 5 | 45 | 6 | 0 | 8 | 40 | 7 | 0 | 13 | 2 | 4 | 0 | 4 | 3 | 6 | 0 | 143 | |
| 4:30 PM | 2 | 40 | 5 | 0 | 6 | 28 | 6 | 0 | 13 | 4 | 3 | 0 | 6 | 2 | 2 | 0 | 117 | |
| 4:35 PM | 5 | 43 | 2 | 0 | 1 | 45 | 6 | 1 | 12 | 2 | 4 | 0 | 4 | 3 | 4 | 0 | 132 | |
| 4:40 PM | 12 | 40 | 2 | 1 | 7 | 37 | 15 | 0 | 8 | 1 | 3 | 0 | 6 | 4 | 11 | 0 | 147 | |
| 4:45 PM | 5 | 34 | 5 | 1 | 7 | 35 | 11 | 0 | 7 | 0 | 2 | 0 | 4 | 2 | 3 | 0 | 116 | |
| 4:50 PM | 6 | 37 | 0 | 0 | 4 | 53 | 17 | 4 | 14 | 1 | 1 | 0 | 3 | 1 | 2 | 0 | 143 | |
| 4:55 PM | 10 | 35 | 2 | 1 | 4 | 33 | 18 | 2 | 8 | 4 | 6 | 0 | 5 | 7 | 4 | 0 | 139 | |
| 5:00 PM | 1 | 42 | 3 | 0 | 5 | 32 | 14 | 1 | 13 | 1 | 5 | 0 | 3 | 2 | 5 | 0 | 127 | 1627 |
| 5:05 PM | 6 | 51 | 4 | 0 | 1 | 32 | 12 | 2 | 13 | 5 | 2 | 0 | 7 | 7 | 3 | 0 | 145 | 1601 |
| 5:10 PM | 1 | 34 | 3 | 0 | 2 | 40 | 19 | 0 | 12 | 3 | 6 | 0 | 7 | 9 | 4 | 0 | 140 | 1609 |
| 5:15 PM | 3 | 41 | 3 | 1 | 2 | 45 | 8 | 0 | 10 | 4 | 3 | 0 | 3 | 5 | 7 | 0 | 135 | 1606 |
| 5:20 PM | 1 | 47 | 4 | 0 | 10 | 54 | 11 | 3 | 13 | 3 | 4 | 0 | 8 | 8 | 4 | 0 | 170 | 1654 |
| 5:25 PM | 1 | 39 | 3 | 0 | 5 | 36 | 13 | 0 | 15 | 4 | 3 | 0 | 4 | 5 | 6 | 0 | 134 | 1645 |
| 5:30 PM | 3 | 33 | 1 | 0 | 4 | 36 | 13 | 3 | 14 | 1 | 1 | 0 | 3 | 4 | 3 | 0 | 119 | 1647 |
| 5:35 PM | 5 | 35 | 1 | 0 | 6 | 38 | 9 | 0 | 6 | 0 | 2 | 0 | 7 | 2 | 4 | 0 | 115 | 1630 |
| 5:40 PM | 1 | 23 | 0 | 0 | 2 | 28 | 12 | 1 | 7 | 0 | 2 | 0 | 6 | 3 | 3 | 0 | 88 | 1571 |
| 5:45 PM | 1 | 38 | 2 | 0 | 8 | 42 | 17 | 2 | 8 | 1 | 1 | 0 | 5 | 2 | 0 | 0 | 127 | 1582 |
| 5:50 PM | 5 | 29 | 1 | 0 | 4 | 21 | 9 | 2 | 12 | 3 | 0 | 0 | 3 | 3 | 3 | 0 | 95 | 1534 |
| 5:55 PM | 2 | 23 | 3 | 0 | 2 | 40 | 12 | 0 | 13 | 0 | 2 | 0 | 7 | 0 | 2 | 0 | 106 | 1501 |
| Peak 15-Min Flowrates | Northbound | | | | Southbound | | | | Eastbound | | | | Westbound | | | | Total | |
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| All Vehicles | 20 | 488 | 40 | 4 | 56 | 556 | 152 | 12 | 140 | 40 | 52 | 0 | 72 | 88 | 60 | 0 | 1780 | |
| Heavy Trucks | 0 | 36 | 0 | | 12 | 28 | 4 | | 4 | 4 | 0 | | 0 | 0 | 12 | | 100 | |
| Buses | | | | | | | | | | | | | | | | | | |
| Pedestrians | | 0 | | | | 0 | | | | 0 | | | | 0 | | | 0 | |
| Bicycles | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | |
| Scoters | | | | | | | | | | | | | | | | | | |

Comments:

LOCATION: #4 N 1st St/SR 113 -- Regency Pkwy/Industrial Wy
CITY/STATE: Dixon, CA

QC JOB #: 15676007
DATE: Wed, Jan 12 2022

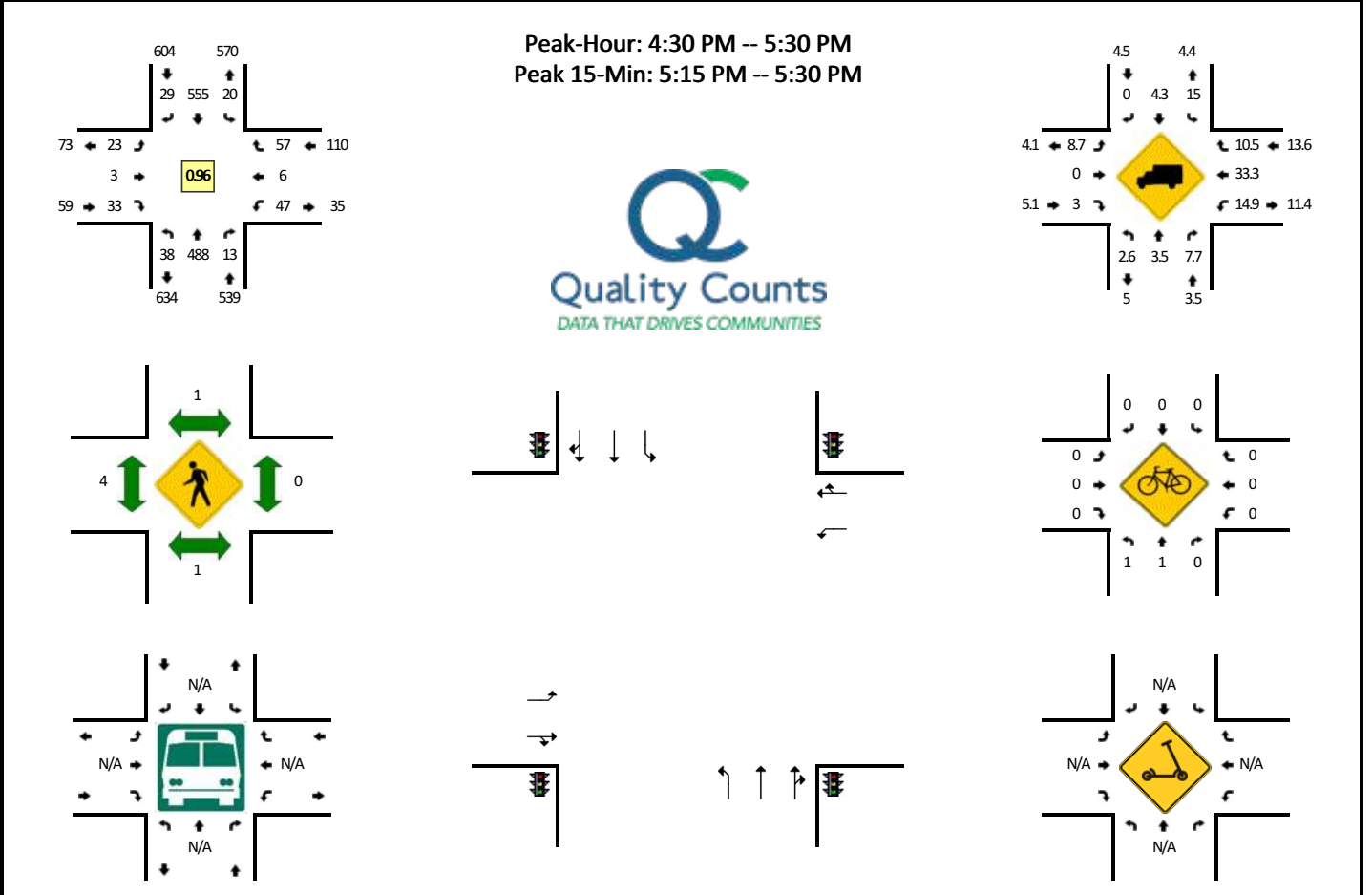


| 5-Min Count Period Beginning At | #4 N 1st St/SR 113 (Northbound) | | | | #4 N 1st St/SR 113 (Southbound) | | | | Regency Pkwy/Industrial Wy (Eastbound) | | | | Regency Pkwy/Industrial Wy (Westbound) | | | | Total | Hourly Totals |
|---------------------------------|---------------------------------|------|-------|---|---------------------------------|------|-------|---|--|------|-------|---|--|------|-------|---|-------|---------------|
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| 7:00 AM | 0 | 26 | 2 | 0 | 1 | 16 | 0 | 0 | 1 | 1 | 3 | 0 | 1 | 0 | 1 | 0 | 52 | |
| 7:05 AM | 0 | 25 | 2 | 0 | 2 | 26 | 1 | 0 | 1 | 1 | 5 | 0 | 0 | 0 | 1 | 0 | 64 | |
| 7:10 AM | 0 | 22 | 3 | 0 | 3 | 19 | 1 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 51 | |
| 7:15 AM | 1 | 24 | 3 | 0 | 5 | 26 | 0 | 0 | 0 | 1 | 0 | 0 | 5 | 0 | 1 | 0 | 66 | |
| 7:20 AM | 1 | 27 | 1 | 0 | 4 | 20 | 2 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 1 | 1 | 61 | |
| 7:25 AM | 1 | 22 | 3 | 0 | 3 | 20 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 51 | |
| 7:30 AM | 3 | 36 | 1 | 0 | 5 | 20 | 1 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 72 | |
| 7:35 AM | 1 | 22 | 4 | 0 | 4 | 15 | 2 | 0 | 2 | 2 | 1 | 0 | 3 | 1 | 1 | 0 | 58 | |
| 7:40 AM | 1 | 39 | 4 | 0 | 8 | 29 | 0 | 0 | 3 | 0 | 3 | 0 | 1 | 0 | 1 | 0 | 89 | |
| 7:45 AM | 1 | 32 | 4 | 0 | 3 | 25 | 0 | 0 | 4 | 2 | 2 | 0 | 2 | 0 | 2 | 0 | 77 | |
| 7:50 AM | 0 | 32 | 0 | 0 | 1 | 24 | 2 | 0 | 1 | 0 | 4 | 0 | 1 | 0 | 2 | 1 | 68 | |
| 7:55 AM | 1 | 32 | 6 | 0 | 6 | 34 | 0 | 0 | 2 | 0 | 5 | 0 | 1 | 0 | 1 | 0 | 88 | 797 |
| 8:00 AM | 5 | 28 | 7 | 0 | 5 | 35 | 0 | 0 | 1 | 1 | 8 | 0 | 3 | 1 | 2 | 0 | 96 | 841 |
| 8:05 AM | 4 | 49 | 0 | 0 | 3 | 28 | 1 | 0 | 5 | 0 | 6 | 0 | 1 | 0 | 0 | 0 | 97 | 874 |
| 8:10 AM | 3 | 29 | 2 | 0 | 3 | 14 | 0 | 0 | 4 | 2 | 12 | 0 | 1 | 0 | 0 | 0 | 70 | 893 |
| 8:15 AM | 3 | 46 | 9 | 0 | 5 | 21 | 2 | 0 | 3 | 0 | 5 | 0 | 1 | 0 | 1 | 0 | 96 | 923 |
| 8:20 AM | 5 | 49 | 3 | 0 | 2 | 32 | 0 | 0 | 0 | 1 | 1 | 0 | 4 | 0 | 2 | 0 | 99 | 961 |
| 8:25 AM | 3 | 37 | 3 | 0 | 4 | 28 | 2 | 0 | 4 | 1 | 2 | 0 | 2 | 0 | 5 | 0 | 91 | 1001 |
| 8:30 AM | 4 | 44 | 4 | 0 | 6 | 23 | 3 | 0 | 1 | 0 | 6 | 0 | 3 | 0 | 2 | 0 | 96 | 1025 |
| 8:35 AM | 0 | 32 | 1 | 0 | 4 | 36 | 1 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 80 | 1047 |
| 8:40 AM | 3 | 34 | 2 | 0 | 2 | 23 | 2 | 0 | 3 | 2 | 2 | 0 | 0 | 0 | 9 | 0 | 82 | 1040 |
| 8:45 AM | 2 | 38 | 0 | 0 | 4 | 28 | 2 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 79 | 1042 |
| 8:50 AM | 2 | 21 | 1 | 0 | 3 | 31 | 2 | 0 | 4 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 67 | 1041 |
| 8:55 AM | 0 | 23 | 1 | 0 | 3 | 28 | 0 | 1 | 0 | 1 | 2 | 0 | 2 | 2 | 3 | 0 | 66 | 1019 |
| Peak 15-Min Flowrates | Northbound | | | | Southbound | | | | Eastbound | | | | Westbound | | | | Total | |
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| All Vehicles | 44 | 528 | 60 | 0 | 44 | 324 | 16 | 0 | 28 | 8 | 32 | 0 | 28 | 0 | 32 | 0 | 1144 | |
| Heavy Trucks | 8 | 24 | 20 | | 12 | 44 | 4 | | 4 | 4 | 0 | | 8 | 0 | 12 | | 140 | |
| Buses | | | | | | | | | | | | | | | | | | |
| Pedestrians | | 0 | | | | 0 | | | | 4 | | | | 0 | | | 4 | |
| Bicycles | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | |
| Scoters | | | | | | | | | | | | | | | | | | |

Comments:

LOCATION: #4 N 1st St/SR 113 -- Regency Pkwy/Industrial Wy
CITY/STATE: Dixon, CA

QC JOB #: 15676008
DATE: Wed, Jan 12 2022



| 5-Min Count Period Beginning At | #4 N 1st St/SR 113 (Northbound) | | | | #4 N 1st St/SR 113 (Southbound) | | | | Regency Pkwy/Industrial Wy (Eastbound) | | | | Regency Pkwy/Industrial Wy (Westbound) | | | | Total | Hourly Totals |
|---------------------------------|---------------------------------|------|-------|---|---------------------------------|------|-------|---|--|------|-------|---|--|------|-------|---|-------|---------------|
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| 4:00 PM | 2 | 39 | 2 | 0 | 1 | 43 | 3 | 0 | 2 | 0 | 3 | 0 | 5 | 0 | 6 | 0 | 106 | |
| 4:05 PM | 4 | 40 | 1 | 1 | 1 | 43 | 1 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 6 | 1 | 102 | |
| 4:10 PM | 5 | 51 | 1 | 0 | 3 | 34 | 0 | 0 | 0 | 0 | 1 | 0 | 6 | 0 | 4 | 0 | 105 | |
| 4:15 PM | 1 | 29 | 0 | 0 | 2 | 50 | 1 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 4 | 0 | 92 | |
| 4:20 PM | 1 | 38 | 1 | 0 | 0 | 49 | 1 | 0 | 2 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 98 | |
| 4:25 PM | 3 | 33 | 1 | 0 | 2 | 36 | 3 | 0 | 2 | 0 | 4 | 0 | 4 | 0 | 4 | 0 | 92 | |
| 4:30 PM | 5 | 38 | 0 | 0 | 5 | 45 | 4 | 0 | 3 | 0 | 3 | 0 | 2 | 1 | 7 | 0 | 113 | |
| 4:35 PM | 2 | 44 | 1 | 0 | 0 | 37 | 4 | 0 | 1 | 0 | 3 | 0 | 10 | 0 | 9 | 0 | 111 | |
| 4:40 PM | 2 | 43 | 1 | 0 | 0 | 46 | 5 | 0 | 2 | 0 | 3 | 0 | 5 | 0 | 4 | 1 | 112 | |
| 4:45 PM | 5 | 36 | 1 | 0 | 2 | 44 | 2 | 0 | 0 | 1 | 3 | 0 | 5 | 0 | 6 | 0 | 105 | |
| 4:50 PM | 6 | 38 | 3 | 0 | 1 | 47 | 3 | 1 | 3 | 0 | 2 | 0 | 3 | 1 | 3 | 0 | 111 | |
| 4:55 PM | 4 | 34 | 0 | 0 | 0 | 51 | 2 | 0 | 2 | 0 | 2 | 0 | 5 | 1 | 4 | 0 | 105 | 1252 |
| 5:00 PM | 2 | 47 | 3 | 0 | 2 | 54 | 0 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 4 | 0 | 118 | 1264 |
| 5:05 PM | 3 | 47 | 0 | 0 | 1 | 27 | 1 | 0 | 1 | 0 | 3 | 0 | 7 | 0 | 5 | 0 | 95 | 1257 |
| 5:10 PM | 3 | 34 | 2 | 0 | 1 | 49 | 1 | 0 | 1 | 0 | 2 | 0 | 1 | 1 | 4 | 0 | 99 | 1251 |
| 5:15 PM | 0 | 38 | 1 | 0 | 2 | 56 | 3 | 0 | 6 | 1 | 3 | 0 | 3 | 0 | 7 | 0 | 120 | 1279 |
| 5:20 PM | 2 | 50 | 0 | 0 | 1 | 56 | 2 | 0 | 1 | 0 | 5 | 0 | 2 | 1 | 3 | 0 | 123 | 1304 |
| 5:25 PM | 4 | 39 | 1 | 0 | 3 | 43 | 2 | 0 | 2 | 0 | 3 | 0 | 2 | 0 | 1 | 0 | 100 | 1312 |
| 5:30 PM | 2 | 37 | 3 | 0 | 3 | 46 | 5 | 0 | 1 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 100 | 1299 |
| 5:35 PM | 3 | 29 | 2 | 0 | 1 | 45 | 3 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 5 | 0 | 91 | 1279 |
| 5:40 PM | 0 | 23 | 4 | 0 | 2 | 38 | 2 | 0 | 2 | 0 | 4 | 0 | 0 | 0 | 3 | 0 | 78 | 1245 |
| 5:45 PM | 0 | 39 | 0 | 0 | 0 | 28 | 1 | 0 | 0 | 0 | 4 | 0 | 3 | 0 | 3 | 0 | 78 | 1218 |
| 5:50 PM | 4 | 27 | 2 | 0 | 1 | 38 | 2 | 0 | 3 | 0 | 4 | 0 | 0 | 1 | 4 | 0 | 86 | 1193 |
| 5:55 PM | 0 | 28 | 0 | 0 | 1 | 35 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 73 | 1161 |
| Peak 15-Min Flowrates | Northbound | | | | Southbound | | | | Eastbound | | | | Westbound | | | | Total | |
| | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | Left | Thru | Right | U | | |
| All Vehicles | 24 | 508 | 8 | 0 | 24 | 620 | 28 | 0 | 36 | 4 | 44 | 0 | 28 | 4 | 44 | 0 | 1372 | |
| Heavy Trucks | 0 | 40 | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 4 | 0 | 8 | 4 | 8 | 0 | 84 | |
| Buses | | | | | | | | | | | | | | | | | | |
| Pedestrians | | 0 | | | | 0 | | | | 0 | | | | 0 | | | 0 | |
| Bicycles | 4 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 4 | |
| Scoters | | | | | | | | | | | | | | | | | | |

Comments:

Appendix B

Synchro Output Reports

Independence at Dixon TIA

2: SR 113 & Dorset Dr/E. Dorset Dr

Existing AM Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 62 | 13 | 23 | 69 | 5 | 33 | 35 | 64 | 446 | 84 | 1 | 75 |
| Future Volume (vph) | 62 | 13 | 23 | 69 | 5 | 33 | 35 | 64 | 446 | 84 | 1 | 75 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 160 | 195 | | 195 | | 200 | | 320 | | 235 |
| Storage Lanes | 2 | | 1 | 2 | | 1 | | 1 | | 1 | | 2 |
| Taper Length (ft) | 25 | | | 25 | | | | 25 | | | | 25 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.95 | 0.97 |
| Ped Bike Factor | | | 0.99 | | | 0.99 | | | | | | |
| Frt | | | 0.850 | | | 0.850 | | | | 0.850 | | |
| Flt Protected | 0.950 | | | 0.950 | | | | 0.950 | | | | 0.950 |
| Satd. Flow (prot) | 2968 | 1652 | 1553 | 3273 | 1900 | 1442 | 0 | 1782 | 3139 | 1583 | 0 | 3158 |
| Flt Permitted | 0.950 | | | 0.950 | | | | 0.950 | | | | 0.950 |
| Satd. Flow (perm) | 2968 | 1652 | 1531 | 3273 | 1900 | 1423 | 0 | 1782 | 3139 | 1583 | 0 | 3158 |
| Right Turn on Red | | | Yes | | | Yes | | | | Yes | | |
| Satd. Flow (RTOR) | | | 87 | | | 87 | | | | 97 | | |
| Link Speed (mph) | | 35 | | | 35 | | | | 45 | | | |
| Link Distance (ft) | | 600 | | | 696 | | | | 687 | | | |
| Travel Time (s) | | 11.7 | | | 13.6 | | | | 10.4 | | | |
| Confl. Peds. (#/hr) | | | 2 | | | 1 | | | | | | |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Heavy Vehicles (%) | 18% | 15% | 4% | 7% | 0% | 12% | 0% | 2% | 15% | 2% | 0% | 11% |
| Adj. Flow (vph) | 71 | 15 | 26 | 79 | 6 | 38 | 40 | 74 | 513 | 97 | 1 | 86 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 71 | 15 | 26 | 79 | 6 | 38 | 0 | 114 | 513 | 97 | 0 | 87 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | R NA | Left | Left | Right | R NA | Left |
| Median Width(ft) | | 24 | | | 24 | | | | 24 | | | |
| Link Offset(ft) | | 0 | | | 0 | | | | 0 | | | |
| Crosswalk Width(ft) | | 16 | | | 16 | | | | 16 | | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 15 | | 9 | 9 | 15 | | 9 | 9 | 15 |
| Turn Type | Prot | NA | Perm | Prot | NA | Perm | Prot | Prot | NA | Perm | Prot | Prot |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 5 | 2 | | 1 | 1 |
| Permitted Phases | | | 4 | | | 8 | | | | 2 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 5 | 2 | 2 | 1 | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 13.0 | 12.0 | 12.0 | 13.0 | 12.0 | 12.0 | 12.0 | 12.0 | 10.0 | 10.0 | 13.0 | 13.0 |
| Minimum Split (s) | 16.7 | 41.6 | 41.6 | 16.0 | 41.6 | 41.6 | 15.7 | 15.7 | 36.8 | 36.8 | 16.7 | 16.7 |
| Total Split (s) | 20.7 | 41.6 | 41.6 | 18.7 | 41.6 | 41.6 | 18.7 | 18.7 | 36.8 | 36.8 | 18.7 | 18.7 |
| Total Split (%) | 17.3% | 34.7% | 34.7% | 15.6% | 34.7% | 34.7% | 15.6% | 15.6% | 30.7% | 30.7% | 15.6% | 15.6% |
| Maximum Green (s) | 17.0 | 37.0 | 37.0 | 15.7 | 37.0 | 37.0 | 15.0 | 15.0 | 31.0 | 31.0 | 15.0 | 15.0 |
| Yellow Time (s) | 3.7 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 3.7 | 3.7 | 4.8 | 4.8 | 3.7 | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | 0.5 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | 1.0 | 0.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 |
| Total Lost Time (s) | 3.7 | 4.6 | 4.6 | 3.0 | 4.6 | 4.6 | | 3.7 | 5.8 | 5.8 | | 3.7 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Existing AM Peak Hour



| Lane Group | SBT | SBR |
|----------------------------|-------|-------|
| Lane Configurations | ↑↑ | ↑ |
| Traffic Volume (vph) | 377 | 45 |
| Future Volume (vph) | 377 | 45 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Storage Length (ft) | | 135 |
| Storage Lanes | | 1 |
| Taper Length (ft) | | |
| Lane Util. Factor | 0.95 | 1.00 |
| Ped Bike Factor | | |
| Frt | | 0.850 |
| Flt Protected | | |
| Satd. Flow (prot) | 3139 | 1369 |
| Flt Permitted | | |
| Satd. Flow (perm) | 3139 | 1369 |
| Right Turn on Red | | Yes |
| Satd. Flow (RTOR) | | 76 |
| Link Speed (mph) | 45 | |
| Link Distance (ft) | 967 | |
| Travel Time (s) | 14.7 | |
| Confl. Peds. (#/hr) | | |
| Peak Hour Factor | 0.87 | 0.87 |
| Heavy Vehicles (%) | 15% | 18% |
| Adj. Flow (vph) | 433 | 52 |
| Shared Lane Traffic (%) | | |
| Lane Group Flow (vph) | 433 | 52 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Right |
| Median Width(ft) | 24 | |
| Link Offset(ft) | 0 | |
| Crosswalk Width(ft) | 16 | |
| Two way Left Turn Lane | | |
| Headway Factor | 1.00 | 1.00 |
| Turning Speed (mph) | | 9 |
| Turn Type | NA | Perm |
| Protected Phases | 6 | |
| Permitted Phases | | 6 |
| Detector Phase | 6 | 6 |
| Switch Phase | | |
| Minimum Initial (s) | 10.0 | 10.0 |
| Minimum Split (s) | 38.8 | 38.8 |
| Total Split (s) | 38.8 | 38.8 |
| Total Split (%) | 32.4% | 32.4% |
| Maximum Green (s) | 33.0 | 33.0 |
| Yellow Time (s) | 4.8 | 4.8 |
| All-Red Time (s) | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |
| Total Lost Time (s) | 5.8 | 5.8 |
| Lead/Lag | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Existing AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 | 3.0 | 1.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.2 | 1.2 | 1.0 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | Min | Min | None | None |
| Walk Time (s) | | 7.0 | 7.0 | | 7.0 | 7.0 | | | 7.0 | 7.0 | | |
| Flash Dont Walk (s) | | 30.0 | 30.0 | | 30.0 | 30.0 | | | 24.0 | 24.0 | | |
| Pedestrian Calls (#/hr) | | 2 | 2 | | 1 | 1 | | | 0 | 0 | | |
| Act Effct Green (s) | 16.3 | 18.3 | 18.3 | 16.3 | 18.0 | 18.0 | | 15.3 | 24.5 | 24.5 | | 16.3 |
| Actuated g/C Ratio | 0.26 | 0.29 | 0.29 | 0.26 | 0.29 | 0.29 | | 0.25 | 0.39 | 0.39 | | 0.26 |
| v/c Ratio | 0.09 | 0.03 | 0.05 | 0.09 | 0.01 | 0.08 | | 0.26 | 0.42 | 0.14 | | 0.11 |
| Control Delay | 30.3 | 23.5 | 0.2 | 30.0 | 23.8 | 0.3 | | 32.4 | 25.7 | 7.6 | | 30.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 |
| Total Delay | 30.3 | 23.5 | 0.2 | 30.0 | 23.8 | 0.3 | | 32.4 | 25.7 | 7.6 | | 30.0 |
| LOS | C | C | A | C | C | A | | C | C | A | | C |
| Approach Delay | | 22.4 | | | 20.5 | | | | 24.4 | | | |
| Approach LOS | | C | | | C | | | | C | | | |

Intersection Summary

| | |
|------------------------------------|------------------------|
| Area Type: | Other |
| Cycle Length: | 119.8 |
| Actuated Cycle Length: | 62.2 |
| Natural Cycle: | 115 |
| Control Type: | Actuated-Uncoordinated |
| Maximum v/c Ratio: | 0.42 |
| Intersection Signal Delay: | 23.7 |
| Intersection LOS: | C |
| Intersection Capacity Utilization: | 60.0% |
| ICU Level of Service: | B |
| Analysis Period (min): | 15 |

Splits and Phases: 2: SR 113 & Dorset Dr/E. Dorset Dr



Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr






















Existing AM Peak Hour



| Lane Group | SBT | SBR |
|-------------------------|------|------|
| Vehicle Extension (s) | 0.2 | 0.2 |
| Minimum Gap (s) | 3.0 | 3.0 |
| Time Before Reduce (s) | 1.2 | 1.2 |
| Time To Reduce (s) | 0.1 | 0.1 |
| Recall Mode | Min | Min |
| Walk Time (s) | 7.0 | 7.0 |
| Flash Dont Walk (s) | 26.0 | 26.0 |
| Pedestrian Calls (#/hr) | 0 | 0 |
| Act Effct Green (s) | 25.1 | 25.1 |
| Actuated g/C Ratio | 0.40 | 0.40 |
| v/c Ratio | 0.34 | 0.09 |
| Control Delay | 24.7 | 4.4 |
| Queue Delay | 0.0 | 0.0 |
| Total Delay | 24.7 | 4.4 |
| LOS | C | A |
| Approach Delay | 23.7 | |
| Approach LOS | C | |
| Intersection Summary | | |

Independence at Dixon TIA
3: SR 113 & N. Lincoln St/Vaughn Rd

Existing AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|----------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
| Lane Configurations |  |  |  | |  |  |  | |  |  |  | |
| Traffic Volume (vph) | 109 | 26 | 39 | 1 | 43 | 37 | 48 | 1 | 36 | 461 | 37 | 3 |
| Future Volume (vph) | 109 | 26 | 39 | 1 | 43 | 37 | 48 | 1 | 36 | 461 | 37 | 3 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 275 | | 0 | | 180 | | 230 | | 290 | | 0 | |
| Storage Lanes | 1 | | 1 | | 1 | | 1 | | 1 | | 0 | |
| Taper Length (ft) | 25 | | | | 25 | | | | 25 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 | 0.95 |
| Ped Bike Factor | | | 0.99 | | | | | | | 1.00 | | |
| Frt | | | 0.850 | | | | 0.850 | | | 0.989 | | |
| Flt Protected | 0.950 | | | | 0.950 | | | | 0.950 | | | |
| Satd. Flow (prot) | 1752 | 1900 | 1495 | 0 | 1689 | 1900 | 1196 | 0 | 1659 | 3193 | 0 | 0 |
| Flt Permitted | 0.950 | | | | 0.312 | | | | 0.950 | | | |
| Satd. Flow (perm) | 1752 | 1900 | 1476 | 0 | 555 | 1900 | 1196 | 0 | 1659 | 3193 | 0 | 0 |
| Right Turn on Red | | | Yes | | | | Yes | | | | Yes | |
| Satd. Flow (RTOR) | | | 104 | | | | 104 | | | 7 | | |
| Link Speed (mph) | | 35 | | | | 45 | | | 45 | | | |
| Link Distance (ft) | | 437 | | | | 359 | | | 1163 | | | |
| Travel Time (s) | | 8.5 | | | | 5.4 | | | 17.6 | | | |
| Confl. Peds. (#/hr) | | | 1 | | | | | | | | 3 | |
| Confl. Bikes (#/hr) | | 1 | | | | | | | | | | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.92 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (%) | 3% | 0% | 8% | 0% | 7% | 0% | 35% | 0% | 9% | 12% | 8% | 0% |
| Adj. Flow (vph) | 115 | 27 | 41 | 1 | 45 | 39 | 51 | 1 | 38 | 485 | 39 | 3 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 115 | 27 | 41 | 0 | 46 | 39 | 51 | 0 | 39 | 524 | 0 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | R NA | Left | Left | Right | R NA | Left | Left | Right | R NA |
| Median Width(ft) | | 12 | | | | 12 | | | 12 | | | |
| Link Offset(ft) | | 0 | | | | 0 | | | 0 | | | |
| Crosswalk Width(ft) | | 16 | | | | 16 | | | 16 | | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 9 | 15 | | 9 | 9 | 15 | | 9 | 9 |
| Turn Type | Prot | NA | Perm | custom | Prot | NA | Perm | Prot | Prot | NA | | Prot |
| Protected Phases | 7 | 4 | | | 3 | 8 | | 5 | 5 | 2 | | 1 |
| Permitted Phases | | | 4 | 3 | | | 8 | | | | | |
| Detector Phase | 7 | 4 | 4 | 3 | 3 | 8 | 8 | 5 | 5 | 2 | | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 10.0 | 10.0 | 10.0 | | 11.0 |
| Minimum Split (s) | 14.7 | 36.2 | 36.2 | 14.7 | 14.7 | 36.2 | 36.2 | 13.7 | 13.7 | 33.8 | | 14.7 |
| Total Split (s) | 18.7 | 36.2 | 36.2 | 18.7 | 18.7 | 36.2 | 36.2 | 18.7 | 18.7 | 33.8 | | 18.7 |
| Total Split (%) | 17.4% | 33.7% | 33.7% | 17.4% | 17.4% | 33.7% | 33.7% | 17.4% | 17.4% | 31.5% | | 17.4% |
| Maximum Green (s) | 15.0 | 32.0 | 32.0 | 15.0 | 15.0 | 32.0 | 32.0 | 15.0 | 15.0 | 28.0 | | 15.0 |
| Yellow Time (s) | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 4.8 | | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Lost Time (s) | 3.7 | 4.2 | 4.2 | | 3.7 | 4.2 | 4.2 | | 3.7 | 5.8 | | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead | Lead | Lag | | Lead |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Existing AM Peak Hour



| Lane Group | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|
| Lane Configurations | | | |
| Traffic Volume (vph) | 74 | 356 | 70 |
| Future Volume (vph) | 74 | 356 | 70 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 |
| Storage Length (ft) | 285 | | 0 |
| Storage Lanes | 1 | | 0 |
| Taper Length (ft) | 25 | | |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | | | |
| Frt | | 0.975 | |
| Flt Protected | 0.950 | | |
| Satd. Flow (prot) | 1526 | 3199 | 0 |
| Flt Permitted | 0.950 | | |
| Satd. Flow (perm) | 1526 | 3199 | 0 |
| Right Turn on Red | | | Yes |
| Satd. Flow (RTOR) | | 21 | |
| Link Speed (mph) | | 45 | |
| Link Distance (ft) | | 687 | |
| Travel Time (s) | | 10.4 | |
| Confl. Peds. (#/hr) | | | |
| Confl. Bikes (#/hr) | | | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (%) | 19% | 12% | 0% |
| Adj. Flow (vph) | 78 | 375 | 74 |
| Shared Lane Traffic (%) | | | |
| Lane Group Flow (vph) | 81 | 449 | 0 |
| Enter Blocked Intersection | No | No | No |
| Lane Alignment | Left | Left | Right |
| Median Width(ft) | | 12 | |
| Link Offset(ft) | | 0 | |
| Crosswalk Width(ft) | | 16 | |
| Two way Left Turn Lane | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 |
| Turn Type | Prot | NA | |
| Protected Phases | 1 | 6 | |
| Permitted Phases | | | |
| Detector Phase | 1 | 6 | |
| Switch Phase | | | |
| Minimum Initial (s) | 11.0 | 10.0 | |
| Minimum Split (s) | 14.7 | 33.8 | |
| Total Split (s) | 18.7 | 33.8 | |
| Total Split (%) | 17.4% | 31.5% | |
| Maximum Green (s) | 15.0 | 28.0 | |
| Yellow Time (s) | 3.7 | 4.8 | |
| All-Red Time (s) | 0.0 | 1.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | |
| Total Lost Time (s) | 3.7 | 5.8 | |
| Lead/Lag | Lead | Lag | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Existing AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
|-------------------------|------|------|------|------|------|------|------|------|------|------|-----|------|
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 | | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | None | Min | | None |
| Walk Time (s) | | 7.0 | 7.0 | | | 7.0 | 7.0 | | | 7.0 | | |
| Flash Dont Walk (s) | | 25.0 | 25.0 | | | 25.0 | 25.0 | | | 21.0 | | |
| Pedestrian Calls (#/hr) | | 1 | 1 | | | 0 | 0 | | | 3 | | |
| Act Effect Green (s) | 13.3 | 15.5 | 15.5 | | 17.5 | 16.5 | 16.5 | | 11.7 | 25.0 | | |
| Actuated g/C Ratio | 0.20 | 0.23 | 0.23 | | 0.26 | 0.25 | 0.25 | | 0.18 | 0.38 | | |
| v/c Ratio | 0.33 | 0.06 | 0.10 | | 0.32 | 0.08 | 0.14 | | 0.13 | 0.43 | | |
| Control Delay | 34.4 | 25.4 | 0.5 | | 38.5 | 24.2 | 0.9 | | 34.7 | 26.3 | | |
| Queue Delay | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Delay | 34.4 | 25.4 | 0.5 | | 38.5 | 24.2 | 0.9 | | 34.7 | 26.3 | | |
| LOS | C | C | A | | D | C | A | | C | C | | |
| Approach Delay | | 25.5 | | | | 20.3 | | | | 26.9 | | |
| Approach LOS | | C | | | | C | | | | C | | |

Intersection Summary

Area Type: Other
 Cycle Length: 107.4
 Actuated Cycle Length: 66.5
 Natural Cycle: 100
 Control Type: Actuated-Uncoordinated
 Maximum v/c Ratio: 0.43
 Intersection Signal Delay: 24.1
 Intersection LOS: C
 Intersection Capacity Utilization 57.3%
 ICU Level of Service B
 Analysis Period (min) 15

Splits and Phases: 3: SR 113 & N. Lincoln St/Vaughn Rd

| | | | |
|--------------|--------------|--------------|--------------|
| Ø1 18.7 s | Ø2 33.8 s | Ø3 18.7 s | Ø4 36.2 s |
| Ø5 18.7 s | Ø6 33.8 s | Ø7 18.7 s | Ø8 36.2 s |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Existing AM Peak Hour



| Lane Group | SBL | SBT | SBR |
|-----------------------------|------|------|-----|
| Lead-Lag Optimize? | Yes | Yes | |
| Vehicle Extension (s) | 0.2 | 0.2 | |
| Minimum Gap (s) | 1.0 | 3.0 | |
| Time Before Reduce (s) | 1.0 | 1.0 | |
| Time To Reduce (s) | 0.1 | 0.1 | |
| Recall Mode | None | Min | |
| Walk Time (s) | | 7.0 | |
| Flash Dont Walk (s) | | 21.0 | |
| Pedestrian Calls (#/hr) | | 0 | |
| Act Effct Green (s) | 13.1 | 31.8 | |
| Actuated g/C Ratio | 0.20 | 0.48 | |
| v/c Ratio | 0.27 | 0.29 | |
| Control Delay | 34.6 | 19.3 | |
| Queue Delay | 0.0 | 0.0 | |
| Total Delay | 34.6 | 19.3 | |
| LOS | C | B | |
| Approach Delay | | 21.6 | |
| Approach LOS | | C | |
| Intersection Summary | | | |

Independence at Dixon TIA
4: SR 113 & Regency Pkwy/Industrial Wy

Existing AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 31 | 7 | 54 | 1 | 22 | 1 | 20 | 30 | 453 | 43 | 50 | 332 |
| Future Volume (vph) | 31 | 7 | 54 | 1 | 22 | 1 | 20 | 30 | 453 | 43 | 50 | 332 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 0 | | 250 | | 0 | 115 | | 0 | 190 | |
| Storage Lanes | 1 | | 0 | | 1 | | 0 | 1 | | 0 | 1 | |
| Taper Length (ft) | 25 | | | | 25 | | | 25 | | | 25 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 |
| Ped Bike Factor | | 0.99 | | | | | | | | | | 1.00 |
| Frt | | 0.868 | | | | | 0.857 | | 0.987 | | | 0.995 |
| Flt Protected | 0.950 | | | | 0.950 | | | 0.950 | | | 0.950 | |
| Satd. Flow (prot) | 1597 | 1523 | 0 | 0 | 1479 | 1178 | 0 | 1687 | 3298 | 0 | 1480 | 3264 |
| Flt Permitted | 0.950 | | | | 0.950 | | | 0.950 | | | 0.950 | |
| Satd. Flow (perm) | 1597 | 1523 | 0 | 0 | 1479 | 1178 | 0 | 1687 | 3298 | 0 | 1480 | 3264 |
| Right Turn on Red | | | Yes | | | | Yes | | | Yes | | |
| Satd. Flow (RTOR) | | 59 | | | | 22 | | 9 | | | | 3 |
| Link Speed (mph) | | 30 | | | | 30 | | 30 | | | | 45 |
| Link Distance (ft) | | 736 | | | | 904 | | 473 | | | | 1866 |
| Travel Time (s) | | 16.7 | | | | 20.5 | | 10.8 | | | | 28.3 |
| Confl. Bikes (#/hr) | | 1 | 2 | | | | | | | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 13% | 29% | 4% | 0% | 23% | 0% | 40% | 7% | 7% | 19% | 22% | 10% |
| Adj. Flow (vph) | 34 | 8 | 59 | 1 | 24 | 1 | 22 | 33 | 492 | 47 | 54 | 361 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 34 | 67 | 0 | 0 | 25 | 23 | 0 | 33 | 539 | 0 | 54 | 373 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | R NA | Left | Left | Right | Left | Left | Right | Left | Left |
| Median Width(ft) | | 12 | | | | 12 | | 12 | | | 12 | |
| Link Offset(ft) | | 0 | | | | 0 | | 0 | | | 0 | |
| Crosswalk Width(ft) | | 16 | | | | 16 | | 16 | | | 16 | |
| Two way Left Turn Lane | | | | | | | | | | | | Yes |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 9 | 15 | | 9 | 15 | | 9 | 15 | |
| Turn Type | Prot | NA | | Prot | Prot | NA | | Prot | NA | | Prot | NA |
| Protected Phases | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 6 |
| Permitted Phases | | | | | | | | | | | | |
| Detector Phase | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | | 11.0 | 11.0 | 11.0 | | 10.0 | 10.0 | | 10.0 | 10.0 |
| Minimum Split (s) | 14.7 | 35.2 | | 14.7 | 14.7 | 35.2 | | 13.7 | 27.8 | | 13.7 | 27.8 |
| Total Split (s) | 18.7 | 35.2 | | 18.7 | 18.7 | 35.2 | | 18.7 | 30.8 | | 18.7 | 30.8 |
| Total Split (%) | 18.1% | 34.0% | | 18.1% | 18.1% | 34.0% | | 18.1% | 29.8% | | 18.1% | 29.8% |
| Maximum Green (s) | 15.0 | 31.0 | | 15.0 | 15.0 | 31.0 | | 15.0 | 25.0 | | 15.0 | 25.0 |
| Yellow Time (s) | 3.7 | 3.7 | | 3.7 | 3.7 | 3.7 | | 3.7 | 4.8 | | 3.7 | 4.8 |
| All-Red Time (s) | 0.0 | 0.5 | | 0.0 | 0.0 | 0.5 | | 0.0 | 1.0 | | 0.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 |
| Total Lost Time (s) | 3.7 | 4.2 | | 3.7 | 4.2 | 3.7 | | 3.7 | 5.8 | | 3.7 | 5.8 |
| Lead/Lag | Lead | Lag | | Lead | Lead | Lag | | Lead | Lag | | Lead | Lag |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | | Yes | Yes | | Yes | Yes |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Existing AM Peak Hour

| Lane Group | SBR |
|----------------------------|-------|
| Lane Configurations | |
| Traffic Volume (vph) | 11 |
| Future Volume (vph) | 11 |
| Ideal Flow (vphpl) | 1900 |
| Storage Length (ft) | 0 |
| Storage Lanes | 0 |
| Taper Length (ft) | |
| Lane Util. Factor | 0.95 |
| Ped Bike Factor | |
| Flt | |
| Flt Protected | |
| Satd. Flow (prot) | 0 |
| Flt Permitted | |
| Satd. Flow (perm) | 0 |
| Right Turn on Red | Yes |
| Satd. Flow (RTOR) | |
| Link Speed (mph) | |
| Link Distance (ft) | |
| Travel Time (s) | |
| Confl. Bikes (#/hr) | 1 |
| Peak Hour Factor | 0.92 |
| Heavy Vehicles (%) | 9% |
| Adj. Flow (vph) | 12 |
| Shared Lane Traffic (%) | |
| Lane Group Flow (vph) | 0 |
| Enter Blocked Intersection | No |
| Lane Alignment | Right |
| Median Width(ft) | |
| Link Offset(ft) | |
| Crosswalk Width(ft) | |
| Two way Left Turn Lane | |
| Headway Factor | 1.00 |
| Turning Speed (mph) | 9 |
| Turn Type | |
| Protected Phases | |
| Permitted Phases | |
| Detector Phase | |
| Switch Phase | |
| Minimum Initial (s) | |
| Minimum Split (s) | |
| Total Split (s) | |
| Total Split (%) | |
| Maximum Green (s) | |
| Yellow Time (s) | |
| All-Red Time (s) | |
| Lost Time Adjust (s) | |
| Total Lost Time (s) | |
| Lead/Lag | |
| Lead-Lag Optimize? | |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Existing AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|-------------------------|------|------|-----|------|------|------|-----|------|------|-----|------|------|
| Vehicle Extension (s) | 0.2 | 0.2 | | 0.2 | 0.2 | 0.2 | | 0.2 | 0.2 | | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | | 0.1 | 0.1 | 0.1 | | 0.1 | 0.1 | | 0.1 | 0.1 |
| Recall Mode | None | None | | None | None | None | | None | Min | | None | Min |
| Walk Time (s) | | 7.0 | | | | 7.0 | | | 7.0 | | | 7.0 |
| Flash Dont Walk (s) | | 24.0 | | | | 24.0 | | | 15.0 | | | 15.0 |
| Pedestrian Calls (#/hr) | | 2 | | | | 0 | | | 0 | | | 1 |
| Act Effct Green (s) | 13.7 | 15.6 | | | 13.6 | 15.6 | | 12.4 | 26.0 | | 12.4 | 26.0 |
| Actuated g/C Ratio | 0.30 | 0.34 | | | 0.30 | 0.34 | | 0.27 | 0.57 | | 0.27 | 0.57 |
| v/c Ratio | 0.07 | 0.12 | | | 0.06 | 0.06 | | 0.07 | 0.29 | | 0.13 | 0.20 |
| Control Delay | 23.4 | 7.4 | | | 24.3 | 9.3 | | 24.4 | 15.1 | | 24.1 | 14.8 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 |
| Total Delay | 23.4 | 7.4 | | | 24.3 | 9.3 | | 24.4 | 15.1 | | 24.1 | 14.8 |
| LOS | C | A | | | C | A | | C | B | | C | B |
| Approach Delay | | 12.8 | | | | 17.1 | | | 15.7 | | | 16.0 |
| Approach LOS | | B | | | | B | | | B | | | B |

Intersection Summary

| | |
|-----------------------------------|------------------------|
| Area Type: | Other |
| Cycle Length: | 103.4 |
| Actuated Cycle Length: | 45.5 |
| Natural Cycle: | 95 |
| Control Type: | Actuated-Uncoordinated |
| Maximum v/c Ratio: | 0.29 |
| Intersection Signal Delay: | 15.6 |
| Intersection LOS: | B |
| Intersection Capacity Utilization | 43.1% |
| ICU Level of Service | A |
| Analysis Period (min) | 15 |

Splits and Phases: 4: SR 113 & Regency Pkwy/Industrial Wy

| | | | |
|--------|--------|--------|--------|
| | | | |
| 18.7 s | 30.8 s | 18.7 s | 35.2 s |
| | | | |
| 18.7 s | 30.8 s | 18.7 s | 35.2 s |



| | |
|-------------------------|-----|
| Lane Group | SBR |
| Vehicle Extension (s) | |
| Minimum Gap (s) | |
| Time Before Reduce (s) | |
| Time To Reduce (s) | |
| Recall Mode | |
| Walk Time (s) | |
| Flash Dont Walk (s) | |
| Pedestrian Calls (#/hr) | |
| Act Effct Green (s) | |
| Actuated g/C Ratio | |
| v/c Ratio | |
| Control Delay | |
| Queue Delay | |
| Total Delay | |
| LOS | |
| Approach Delay | |
| Approach LOS | |
| Intersection Summary | |

Independence at Dixon TIA

1: SR 113/I-80 EB Ramps & I-80 WB Ramps/Auction Ln

Existing AM Peak Hour

| Intersection | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 2.1 | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL | SBT | SBR |
| Lane Configurations | | ↖ | ↗ | | ↕ | | ↖ | ↗ | | | | ↕ | |
| Traffic Vol, veh/h | 7 | 0 | 379 | 1 | 2 | 0 | 145 | 400 | 1 | 1 | 1 | 117 | 8 |
| Future Vol, veh/h | 7 | 0 | 379 | 1 | 2 | 0 | 145 | 400 | 1 | 1 | 1 | 117 | 8 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | Free | - | - | None | - | - | None | - | - | - | None |
| Storage Length | - | - | 0 | - | - | - | 0 | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | - | 0 | - |
| Peak Hour Factor | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| Heavy Vehicles, % | 29 | 0 | 11 | 100 | 100 | 0 | 21 | 15 | 100 | 0 | 0 | 20 | 13 |
| Mvmt Flow | 8 | 0 | 441 | 1 | 2 | 0 | 169 | 465 | 1 | 1 | 1 | 136 | 9 |

| Major/Minor | Minor2 | | Minor1 | | Major1 | | Major2 | | | | | | |
|----------------------|--------|-----|--------|-----|--------|-----|--------|---|---|---|------|---|---|
| Conflicting Flow All | 948 | 949 | - | 947 | 953 | 466 | 145 | 0 | 0 | - | 466 | 0 | 0 |
| Stage 1 | 143 | 145 | - | 804 | 804 | - | - | - | - | - | - | - | - |
| Stage 2 | 805 | 804 | - | 143 | 149 | - | - | - | - | - | - | - | - |
| Critical Hdwy | 7.39 | 6.5 | - | 8.1 | 7.5 | 6.2 | 4.31 | - | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.761 | 4 | - | 4.4 | 4.9 | 3.3 | 2.389 | - | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 215 | 262 | 0 | 164 | 180 | 601 | 1329 | - | - | - | 1106 | - | - |
| Stage 1 | 799 | 781 | 0 | 263 | 283 | - | - | - | - | - | - | - | - |
| Stage 2 | 339 | 398 | 0 | 673 | 620 | - | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | | | - | - |
| Mov Cap-1 Maneuver | 192 | 229 | - | 148 | 157 | 601 | 1329 | - | - | ~ | ~ | - | - |
| Mov Cap-2 Maneuver | 192 | 229 | - | 148 | 157 | - | - | - | - | - | - | - | - |
| Stage 1 | 698 | 781 | - | 230 | 247 | - | - | - | - | - | - | - | - |
| Stage 2 | 293 | 347 | - | 673 | 620 | - | - | - | - | - | - | - | - |

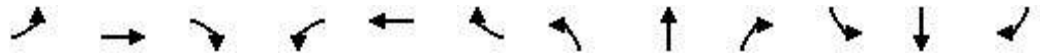
| Approach | EB | | WB | | NB | | SB | | | |
|----------------------|------|--|------|--|-----|--|----|--|--|--|
| HCM Control Delay, s | 24.6 | | 28.9 | | 2.2 | | | | | |
| HCM LOS | C | | D | | | | | | | |

| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | EBLn2 | WBLn1 | SBL | SBT | SBR |
|-----------------------|-------|-----|-----|-------|-------|-------|-----|-----|-----|
| Capacity (veh/h) | 1329 | - | - | 192 | - | 154 | ~ | - | - |
| HCM Lane V/C Ratio | 0.127 | - | - | 0.042 | - | 0.023 | ~ | - | - |
| HCM Control Delay (s) | 8.1 | - | - | 24.6 | 0 | 28.9 | - | - | - |
| HCM Lane LOS | A | - | - | C | A | D | - | - | - |
| HCM 95th %tile Q(veh) | 0.4 | - | - | 0.1 | - | 0.1 | ~ | - | - |

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Existing AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 71 | 15 | 26 | 79 | 6 | 38 | 114 | 513 | 97 | 87 | 433 | 52 |
| v/c Ratio | 0.09 | 0.03 | 0.05 | 0.09 | 0.01 | 0.08 | 0.26 | 0.42 | 0.14 | 0.11 | 0.34 | 0.09 |
| Control Delay | 30.3 | 23.5 | 0.2 | 30.0 | 23.8 | 0.3 | 32.4 | 25.7 | 7.6 | 30.0 | 24.7 | 4.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 30.3 | 23.5 | 0.2 | 30.0 | 23.8 | 0.3 | 32.4 | 25.7 | 7.6 | 30.0 | 24.7 | 4.4 |
| Queue Length 50th (ft) | 13 | 5 | 0 | 14 | 2 | 0 | 44 | 111 | 0 | 16 | 89 | 0 |
| Queue Length 95th (ft) | 43 | 20 | 0 | 46 | 11 | 0 | 126 | 217 | 38 | 50 | 184 | 16 |
| Internal Link Dist (ft) | | 520 | | | 616 | | | 607 | | | 887 | |
| Turn Bay Length (ft) | 150 | | 160 | 195 | | 195 | 200 | | 320 | 235 | | 135 |
| Base Capacity (vph) | 1018 | 1147 | 1089 | 1037 | 1290 | 994 | 539 | 2037 | 1061 | 956 | 2037 | 915 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.07 | 0.01 | 0.02 | 0.08 | 0.00 | 0.04 | 0.21 | 0.25 | 0.09 | 0.09 | 0.21 | 0.06 |

Intersection Summary

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Existing AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|-------------------------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 115 | 27 | 41 | 46 | 39 | 51 | 39 | 524 | 81 | 449 |
| v/c Ratio | 0.33 | 0.06 | 0.10 | 0.32 | 0.08 | 0.14 | 0.13 | 0.43 | 0.27 | 0.29 |
| Control Delay | 34.4 | 25.4 | 0.5 | 38.5 | 24.2 | 0.9 | 34.7 | 26.3 | 34.6 | 19.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.4 | 25.4 | 0.5 | 38.5 | 24.2 | 0.9 | 34.7 | 26.3 | 34.6 | 19.3 |
| Queue Length 50th (ft) | 41 | 9 | 0 | 16 | 13 | 0 | 14 | 101 | 28 | 55 |
| Queue Length 95th (ft) | 130 | 33 | 0 | #85 | 43 | 2 | 58 | 217 | 101 | 173 |
| Internal Link Dist (ft) | | 357 | | | 279 | | | 1083 | | 607 |
| Turn Bay Length (ft) | 275 | | | 180 | | 230 | 290 | | 285 | |
| Base Capacity (vph) | 461 | 1054 | 865 | 166 | 1056 | 711 | 437 | 1575 | 402 | 1606 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.25 | 0.03 | 0.05 | 0.28 | 0.04 | 0.07 | 0.09 | 0.33 | 0.20 | 0.28 |

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy























Existing AM Peak Hour



| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
|-----------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 34 | 67 | 25 | 23 | 33 | 539 | 54 | 373 |
| v/c Ratio | 0.07 | 0.12 | 0.06 | 0.06 | 0.07 | 0.29 | 0.13 | 0.20 |
| Control Delay | 23.4 | 7.4 | 24.3 | 9.3 | 24.4 | 15.1 | 24.1 | 14.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 23.4 | 7.4 | 24.3 | 9.3 | 24.4 | 15.1 | 24.1 | 14.8 |
| Queue Length 50th (ft) | 3 | 1 | 2 | 0 | 4 | 34 | 6 | 23 |
| Queue Length 95th (ft) | 47 | 31 | 38 | 17 | 46 | 203 | 67 | 141 |
| Internal Link Dist (ft) | | 656 | | 824 | | 393 | | 1786 |
| Turn Bay Length (ft) | 150 | | 250 | | 115 | | 190 | |
| Base Capacity (vph) | 652 | 1221 | 604 | 940 | 689 | 2370 | 604 | 2344 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.05 | 0.05 | 0.04 | 0.02 | 0.05 | 0.23 | 0.09 | 0.16 |
| Intersection Summary | | | | | | | | |

Independence at Dixon TIA
2: SR 113 & Dorset Dr/E. Dorset Dr

Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|----------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL |
| Lane Configurations |  |  |  | |  |  |  | |  |  |  |  |
| Traffic Volume (vph) | 108 | 7 | 57 | 1 | 208 | 14 | 120 | 25 | 89 | 518 | 166 | 162 |
| Future Volume (vph) | 108 | 7 | 57 | 1 | 208 | 14 | 120 | 25 | 89 | 518 | 166 | 162 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 160 | | 195 | | 195 | | 200 | | 320 | 235 |
| Storage Lanes | 2 | | 1 | | 2 | | 1 | | 1 | | 1 | 2 |
| Taper Length (ft) | 25 | | | | 25 | | | | 25 | | | 25 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.97 |
| Ped Bike Factor | | | 0.99 | | | | | | | | 0.98 | |
| Frt | | | 0.850 | | | | 0.850 | | | | 0.850 | |
| Flt Protected | 0.950 | | | | 0.950 | | | | 0.950 | | | 0.950 |
| Satd. Flow (prot) | 2968 | 1652 | 1553 | 0 | 3274 | 1900 | 1442 | 0 | 1777 | 3139 | 1583 | 3155 |
| Flt Permitted | 0.950 | | | | 0.950 | | | | 0.950 | | | 0.950 |
| Satd. Flow (perm) | 2968 | 1652 | 1532 | 0 | 3274 | 1900 | 1442 | 0 | 1777 | 3139 | 1558 | 3155 |
| Right Turn on Red | | | Yes | | | | Yes | | | | Yes | |
| Satd. Flow (RTOR) | | | 87 | | | | 125 | | | | 173 | |
| Link Speed (mph) | | 35 | | | | 35 | | | | 45 | | |
| Link Distance (ft) | | 600 | | | | 696 | | | | 687 | | |
| Travel Time (s) | | 11.7 | | | | 13.6 | | | | 10.4 | | |
| Confl. Peds. (#/hr) | | | 1 | | | | | | | | | 3 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | 1 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (%) | 18% | 15% | 4% | 0% | 7% | 0% | 12% | 0% | 2% | 15% | 2% | 11% |
| Adj. Flow (vph) | 113 | 7 | 59 | 1 | 217 | 15 | 125 | 26 | 93 | 540 | 173 | 169 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 113 | 7 | 59 | 0 | 218 | 15 | 125 | 0 | 119 | 540 | 173 | 169 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | R NA | Left | Left | Right | R NA | Left | Left | Right | Left |
| Median Width(ft) | | 24 | | | | 24 | | | | 24 | | |
| Link Offset(ft) | | 0 | | | | 0 | | | | 0 | | |
| Crosswalk Width(ft) | | 16 | | | | 16 | | | | 16 | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 9 | 15 | | 9 | 9 | 15 | | 9 | 15 |
| Turn Type | Prot | NA | Perm | Prot | Prot | NA | Perm | Prot | Prot | NA | Perm | Prot |
| Protected Phases | 7 | 4 | | 3 | 3 | 8 | | 5 | 5 | 2 | | 1 |
| Permitted Phases | | | 4 | | | | 8 | | | | 2 | |
| Detector Phase | 7 | 4 | 4 | 3 | 3 | 8 | 8 | 5 | 5 | 2 | 2 | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 13.0 | 12.0 | 12.0 | 13.0 | 13.0 | 12.0 | 12.0 | 12.0 | 12.0 | 10.0 | 10.0 | 13.0 |
| Minimum Split (s) | 16.7 | 41.6 | 41.6 | 16.0 | 16.0 | 41.6 | 41.6 | 15.7 | 15.7 | 36.8 | 36.8 | 16.7 |
| Total Split (s) | 20.7 | 41.6 | 41.6 | 18.7 | 18.7 | 41.6 | 41.6 | 18.7 | 18.7 | 36.8 | 36.8 | 18.7 |
| Total Split (%) | 17.3% | 34.7% | 34.7% | 15.6% | 15.6% | 34.7% | 34.7% | 15.6% | 15.6% | 30.7% | 30.7% | 15.6% |
| Maximum Green (s) | 17.0 | 37.0 | 37.0 | 15.7 | 15.7 | 37.0 | 37.0 | 15.0 | 15.0 | 31.0 | 31.0 | 15.0 |
| Yellow Time (s) | 3.7 | 4.1 | 4.1 | 3.0 | 3.0 | 4.1 | 4.1 | 3.7 | 3.7 | 4.8 | 4.8 | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | 1.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 3.7 | 4.6 | 4.6 | | 3.0 | 4.6 | 4.6 | | 3.7 | 5.8 | 5.8 | 3.7 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Existing PM Peak Hour



| Lane Group | SBT | SBR |
|----------------------------|-------|-------|
| Lane Configurations | ↑↑ | ↑ |
| Traffic Volume (vph) | 425 | 115 |
| Future Volume (vph) | 425 | 115 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Storage Length (ft) | | 135 |
| Storage Lanes | | 1 |
| Taper Length (ft) | | |
| Lane Util. Factor | 0.95 | 1.00 |
| Ped Bike Factor | | |
| Frt | | 0.850 |
| Flt Protected | | |
| Satd. Flow (prot) | 3139 | 1369 |
| Flt Permitted | | |
| Satd. Flow (perm) | 3139 | 1369 |
| Right Turn on Red | | Yes |
| Satd. Flow (RTOR) | | 120 |
| Link Speed (mph) | 45 | |
| Link Distance (ft) | 967 | |
| Travel Time (s) | 14.7 | |
| Confl. Peds. (#/hr) | | |
| Confl. Bikes (#/hr) | | |
| Peak Hour Factor | 0.96 | 0.96 |
| Heavy Vehicles (%) | 15% | 18% |
| Adj. Flow (vph) | 443 | 120 |
| Shared Lane Traffic (%) | | |
| Lane Group Flow (vph) | 443 | 120 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Right |
| Median Width(ft) | 24 | |
| Link Offset(ft) | 0 | |
| Crosswalk Width(ft) | 16 | |
| Two way Left Turn Lane | | |
| Headway Factor | 1.00 | 1.00 |
| Turning Speed (mph) | | 9 |
| Turn Type | NA | Perm |
| Protected Phases | 6 | |
| Permitted Phases | | 6 |
| Detector Phase | 6 | 6 |
| Switch Phase | | |
| Minimum Initial (s) | 10.0 | 10.0 |
| Minimum Split (s) | 38.8 | 38.8 |
| Total Split (s) | 38.8 | 38.8 |
| Total Split (%) | 32.4% | 32.4% |
| Maximum Green (s) | 33.0 | 33.0 |
| Yellow Time (s) | 4.8 | 4.8 |
| All-Red Time (s) | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |
| Total Lost Time (s) | 5.8 | 5.8 |
| Lead/Lag | Lag | Lag |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Existing PM Peak Hour

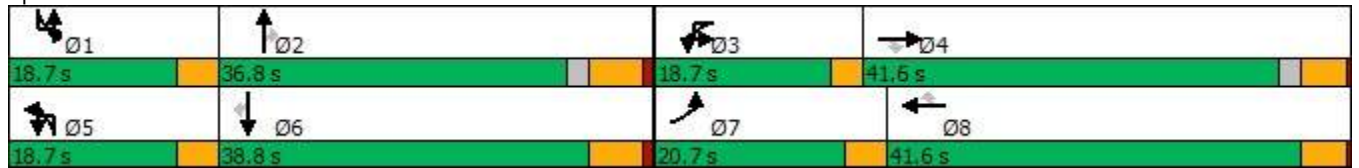


| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 2.0 | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 | 3.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.2 | 1.2 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | None | Min | Min | None |
| Walk Time (s) | | 7.0 | 7.0 | | | 7.0 | 7.0 | | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | | 30.0 | 30.0 | | | 30.0 | 30.0 | | | 24.0 | 24.0 | |
| Pedestrian Calls (#/hr) | | 1 | 1 | | | 0 | 0 | | | 3 | 3 | |
| Act Effect Green (s) | 13.9 | 16.4 | 16.4 | | 17.9 | 16.1 | 16.1 | | 13.2 | 16.7 | 16.7 | 13.9 |
| Actuated g/C Ratio | 0.19 | 0.22 | 0.22 | | 0.24 | 0.22 | 0.22 | | 0.18 | 0.22 | 0.22 | 0.19 |
| v/c Ratio | 0.20 | 0.02 | 0.15 | | 0.28 | 0.04 | 0.31 | | 0.38 | 0.77 | 0.36 | 0.29 |
| Control Delay | 33.4 | 25.1 | 3.2 | | 30.7 | 25.6 | 7.5 | | 37.3 | 36.5 | 7.1 | 33.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 33.4 | 25.1 | 3.2 | | 30.7 | 25.6 | 7.5 | | 37.3 | 36.5 | 7.1 | 33.4 |
| LOS | C | C | A | | C | C | A | | D | D | A | C |
| Approach Delay | | 23.1 | | | | 22.4 | | | | 30.5 | | |
| Approach LOS | | C | | | | C | | | | C | | |

Intersection Summary

| | |
|------------------------------------|------------------------|
| Area Type: | Other |
| Cycle Length: | 119.8 |
| Actuated Cycle Length: | 74.6 |
| Natural Cycle: | 115 |
| Control Type: | Actuated-Uncoordinated |
| Maximum v/c Ratio: | 0.77 |
| Intersection Signal Delay: | 27.6 |
| Intersection LOS: | C |
| Intersection Capacity Utilization: | 62.4% |
| ICU Level of Service: | B |
| Analysis Period (min): | 15 |

Splits and Phases: 2: SR 113 & Dorset Dr/E. Dorset Dr



Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Existing PM Peak Hour



| Lane Group | SBT | SBR |
|-------------------------|------|------|
| Lead-Lag Optimize? | Yes | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 |
| Minimum Gap (s) | 3.0 | 3.0 |
| Time Before Reduce (s) | 1.2 | 1.2 |
| Time To Reduce (s) | 0.1 | 0.1 |
| Recall Mode | Min | Min |
| Walk Time (s) | 7.0 | 7.0 |
| Flash Dont Walk (s) | 26.0 | 26.0 |
| Pedestrian Calls (#/hr) | 0 | 0 |
| Act Effct Green (s) | 17.4 | 17.4 |
| Actuated g/C Ratio | 0.23 | 0.23 |
| v/c Ratio | 0.61 | 0.29 |
| Control Delay | 31.2 | 8.1 |
| Queue Delay | 0.0 | 0.0 |
| Total Delay | 31.2 | 8.1 |
| LOS | C | A |
| Approach Delay | 27.9 | |
| Approach LOS | C | |
| Intersection Summary | | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Existing PM Peak Hour



| Lane Group | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 3 | 118 | 31 | 66 | 95 | 52 | 71 | 6 | 72 | 509 | 48 | 9 |
| Future Volume (vph) | 3 | 118 | 31 | 66 | 95 | 52 | 71 | 6 | 72 | 509 | 48 | 9 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | | 275 | | 0 | 180 | | 230 | | 290 | | 0 | |
| Storage Lanes | | 1 | | 1 | 1 | | 1 | | 1 | | 0 | |
| Taper Length (ft) | | 25 | | | 25 | | | | 25 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 | 0.95 |
| Ped Bike Factor | | | | 0.99 | | | | | | 1.00 | | |
| Frt | | | | 0.850 | | | 0.850 | | | 0.987 | | |
| Flt Protected | | 0.950 | | | 0.950 | | | | 0.950 | | | |
| Satd. Flow (prot) | 0 | 1754 | 1900 | 1495 | 1687 | 1900 | 1196 | 0 | 1666 | 3187 | 0 | 0 |
| Flt Permitted | | 0.950 | | | 0.950 | | | | 0.950 | | | |
| Satd. Flow (perm) | 0 | 1754 | 1900 | 1476 | 1687 | 1900 | 1196 | 0 | 1666 | 3187 | 0 | 0 |
| Right Turn on Red | | | | Yes | | | Yes | | | | Yes | |
| Satd. Flow (RTOR) | | | | 104 | | | 104 | | | 9 | | |
| Link Speed (mph) | | | 35 | | | 45 | | | | 45 | | |
| Link Distance (ft) | | | 437 | | | 359 | | | | 1163 | | |
| Travel Time (s) | | | 8.5 | | | 5.4 | | | | 17.6 | | |
| Confl. Peds. (#/hr) | | | | 1 | | | | | | | 3 | |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (%) | 0% | 3% | 0% | 8% | 7% | 0% | 35% | 0% | 9% | 12% | 8% | 0% |
| Adj. Flow (vph) | 3 | 127 | 33 | 71 | 102 | 56 | 76 | 6 | 77 | 547 | 52 | 10 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 130 | 33 | 71 | 102 | 56 | 76 | 0 | 83 | 599 | 0 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | R NA | Left | Left | Right | Left | Left | Right | R NA | Left | Left | Right | R NA |
| Median Width(ft) | | | 12 | | | 12 | | | | 12 | | |
| Link Offset(ft) | | | 0 | | | 0 | | | | 0 | | |
| Crosswalk Width(ft) | | | 16 | | | 16 | | | | 16 | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 9 | 15 | | 9 | 15 | | 9 | 9 | 15 | | 9 | 9 |
| Turn Type | Prot | Prot | NA | Perm | Prot | NA | Perm | Prot | Prot | NA | | Prot |
| Protected Phases | 7 | 7 | 4 | | 3 | 8 | | 5 | 5 | 2 | | 1 |
| Permitted Phases | | | | 4 | | | 8 | | | | | |
| Detector Phase | 7 | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 5 | 2 | | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 10.0 | 10.0 | 10.0 | | 11.0 |
| Minimum Split (s) | 14.7 | 14.7 | 36.2 | 36.2 | 14.7 | 36.2 | 36.2 | 13.7 | 13.7 | 33.8 | | 14.7 |
| Total Split (s) | 18.7 | 18.7 | 36.2 | 36.2 | 18.7 | 36.2 | 36.2 | 18.7 | 18.7 | 33.8 | | 18.7 |
| Total Split (%) | 17.4% | 17.4% | 33.7% | 33.7% | 17.4% | 33.7% | 33.7% | 17.4% | 17.4% | 31.5% | | 17.4% |
| Maximum Green (s) | 15.0 | 15.0 | 32.0 | 32.0 | 15.0 | 32.0 | 32.0 | 15.0 | 15.0 | 28.0 | | 15.0 |
| Yellow Time (s) | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 4.8 | | 3.7 |
| All-Red Time (s) | 0.0 | 0.0 | 0.5 | 0.5 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | | 0.0 |
| Lost Time Adjust (s) | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Lost Time (s) | | 3.7 | 4.2 | 4.2 | 3.7 | 4.2 | 4.2 | | 3.7 | 5.8 | | |
| Lead/Lag | Lead | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lead | Lag | | Lead |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Existing PM Peak Hour



| Lane Group | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|
| Lane Configurations | | | |
| Traffic Volume (vph) | 58 | 495 | 157 |
| Future Volume (vph) | 58 | 495 | 157 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 |
| Storage Length (ft) | 285 | | 0 |
| Storage Lanes | 1 | | 0 |
| Taper Length (ft) | 25 | | |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | | | |
| Frt | | 0.964 | |
| Flt Protected | 0.950 | | |
| Satd. Flow (prot) | 1551 | 3190 | 0 |
| Flt Permitted | 0.950 | | |
| Satd. Flow (perm) | 1551 | 3190 | 0 |
| Right Turn on Red | | | Yes |
| Satd. Flow (RTOR) | | 38 | |
| Link Speed (mph) | | 45 | |
| Link Distance (ft) | | 687 | |
| Travel Time (s) | | 10.4 | |
| Confl. Peds. (#/hr) | | | |
| Confl. Bikes (#/hr) | | | |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (%) | 19% | 12% | 0% |
| Adj. Flow (vph) | 62 | 532 | 169 |
| Shared Lane Traffic (%) | | | |
| Lane Group Flow (vph) | 72 | 701 | 0 |
| Enter Blocked Intersection | No | No | No |
| Lane Alignment | Left | Left | Right |
| Median Width(ft) | | 12 | |
| Link Offset(ft) | | 0 | |
| Crosswalk Width(ft) | | 16 | |
| Two way Left Turn Lane | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 |
| Turn Type | Prot | NA | |
| Protected Phases | 1 | 6 | |
| Permitted Phases | | | |
| Detector Phase | 1 | 6 | |
| Switch Phase | | | |
| Minimum Initial (s) | 11.0 | 10.0 | |
| Minimum Split (s) | 14.7 | 33.8 | |
| Total Split (s) | 18.7 | 33.8 | |
| Total Split (%) | 17.4% | 31.5% | |
| Maximum Green (s) | 15.0 | 28.0 | |
| Yellow Time (s) | 3.7 | 4.8 | |
| All-Red Time (s) | 0.0 | 1.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | |
| Total Lost Time (s) | 3.7 | 5.8 | |
| Lead/Lag | Lead | Lag | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Existing PM Peak Hour



| Lane Group | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
|-------------------------|------|------|------|------|------|------|------|------|------|------|-----|------|
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 | | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | None | Min | | None |
| Walk Time (s) | | | 7.0 | 7.0 | | 7.0 | 7.0 | | | 7.0 | | |
| Flash Dont Walk (s) | | | 25.0 | 25.0 | | 25.0 | 25.0 | | | 21.0 | | |
| Pedestrian Calls (#/hr) | | | 1 | 1 | | 0 | 0 | | | 3 | | |
| Act Effct Green (s) | | 13.8 | 16.0 | 16.0 | 13.6 | 15.8 | 15.8 | | 12.4 | 26.4 | | |
| Actuated g/C Ratio | | 0.21 | 0.24 | 0.24 | 0.21 | 0.24 | 0.24 | | 0.19 | 0.40 | | |
| v/c Ratio | | 0.35 | 0.07 | 0.16 | 0.29 | 0.12 | 0.21 | | 0.27 | 0.47 | | |
| Control Delay | | 34.3 | 25.0 | 3.0 | 34.1 | 26.0 | 4.3 | | 34.8 | 25.2 | | |
| Queue Delay | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Delay | | 34.3 | 25.0 | 3.0 | 34.1 | 26.0 | 4.3 | | 34.8 | 25.2 | | |
| LOS | | C | C | A | C | C | A | | C | C | | |
| Approach Delay | | | 23.5 | | | 22.5 | | | | 26.4 | | |
| Approach LOS | | | C | | | C | | | | C | | |

Intersection Summary

| | |
|------------------------------------|------------------------|
| Area Type: | Other |
| Cycle Length: | 107.4 |
| Actuated Cycle Length: | 65.9 |
| Natural Cycle: | 100 |
| Control Type: | Actuated-Uncoordinated |
| Maximum v/c Ratio: | 0.53 |
| Intersection Signal Delay: | 25.2 |
| Intersection LOS: | C |
| Intersection Capacity Utilization: | 60.9% |
| ICU Level of Service: | B |
| Analysis Period (min): | 15 |

Splits and Phases: 3: SR 113 & N. Lincoln St/Vaughn Rd

| | | | |
|--------|--------|--------|--------|
| Ø1 | Ø2 | Ø3 | Ø4 |
| 18.7 s | 33.8 s | 18.7 s | 36.2 s |
| Ø5 | Ø6 | Ø7 | Ø8 |
| 18.7 s | 33.8 s | 18.7 s | 36.2 s |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd





















Existing PM Peak Hour



| Lane Group | SBL | SBT | SBR |
|-----------------------------|------|------|-----|
| Lead-Lag Optimize? | Yes | Yes | |
| Vehicle Extension (s) | 0.2 | 0.2 | |
| Minimum Gap (s) | 1.0 | 3.0 | |
| Time Before Reduce (s) | 1.0 | 1.0 | |
| Time To Reduce (s) | 0.1 | 0.1 | |
| Recall Mode | None | Min | |
| Walk Time (s) | | 7.0 | |
| Flash Dont Walk (s) | | 21.0 | |
| Pedestrian Calls (#/hr) | | 0 | |
| Act Effct Green (s) | 13.4 | 26.9 | |
| Actuated g/C Ratio | 0.20 | 0.41 | |
| v/c Ratio | 0.23 | 0.53 | |
| Control Delay | 34.1 | 24.8 | |
| Queue Delay | 0.0 | 0.0 | |
| Total Delay | 34.1 | 24.8 | |
| LOS | C | C | |
| Approach Delay | | 25.6 | |
| Approach LOS | | C | |
| Intersection Summary | | | |

Independence at Dixon TIA
4: SR 113 & Regency Pkwy/Industrial Wy

Existing PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|----------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL |
| Lane Configurations |  |  | | |  |  | |  |  |  | |  |
| Traffic Volume (vph) | 25 | 3 | 35 | 1 | 50 | 6 | 61 | 41 | 523 | 14 | 2 | 21 |
| Future Volume (vph) | 25 | 3 | 35 | 1 | 50 | 6 | 61 | 41 | 523 | 14 | 2 | 21 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 0 | | 250 | | 0 | 115 | | 0 | | 190 |
| Storage Lanes | 1 | | 0 | | 1 | | 0 | 1 | | 0 | | 1 |
| Taper Length (ft) | 25 | | | | 25 | | | 25 | | | | 25 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 |
| Ped Bike Factor | | 0.99 | | | | 0.99 | | | | | | |
| Frt | | 0.862 | | | | 0.863 | | | 0.996 | | | |
| Flt Protected | 0.950 | | | | 0.950 | | | 0.950 | | | | 0.950 |
| Satd. Flow (prot) | 1597 | 1528 | 0 | 0 | 1473 | 1186 | 0 | 1687 | 3350 | 0 | 0 | 1502 |
| Flt Permitted | 0.950 | | | | 0.950 | | | 0.950 | | | | 0.950 |
| Satd. Flow (perm) | 1597 | 1528 | 0 | 0 | 1473 | 1186 | 0 | 1687 | 3350 | 0 | 0 | 1502 |
| Right Turn on Red | | | Yes | | | | Yes | | | Yes | | |
| Satd. Flow (RTOR) | | 36 | | | | 64 | | | 2 | | | |
| Link Speed (mph) | | 30 | | | | 30 | | | 30 | | | |
| Link Distance (ft) | | 736 | | | | 904 | | | 473 | | | |
| Travel Time (s) | | 16.7 | | | | 20.5 | | | 10.8 | | | |
| Confl. Peds. (#/hr) | | | 1 | | | | 1 | | | | | |
| Confl. Bikes (#/hr) | | 1 | | | | | | | | | | |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (%) | 13% | 29% | 4% | 0% | 23% | 0% | 40% | 7% | 7% | 19% | 0% | 22% |
| Adj. Flow (vph) | 26 | 3 | 36 | 1 | 52 | 6 | 64 | 43 | 545 | 15 | 2 | 22 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 26 | 39 | 0 | 0 | 53 | 70 | 0 | 43 | 560 | 0 | 0 | 24 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | R NA | Left | Left | Right | Left | Left | Right | R NA | Left |
| Median Width(ft) | | 12 | | | | 12 | | | 12 | | | |
| Link Offset(ft) | | 0 | | | | 0 | | | 0 | | | |
| Crosswalk Width(ft) | | 16 | | | | 16 | | | 16 | | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 9 | 15 | | 9 | 15 | | 9 | 9 | 15 |
| Turn Type | Prot | NA | | Prot | Prot | NA | | Prot | NA | | Prot | Prot |
| Protected Phases | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 1 |
| Permitted Phases | | | | | | | | | | | | |
| Detector Phase | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | | 11.0 | 11.0 | 11.0 | | 10.0 | 10.0 | | 10.0 | 10.0 |
| Minimum Split (s) | 14.7 | 35.2 | | 14.7 | 14.7 | 35.2 | | 13.7 | 27.8 | | 13.7 | 13.7 |
| Total Split (s) | 18.7 | 35.2 | | 18.7 | 18.7 | 35.2 | | 18.7 | 30.8 | | 18.7 | 18.7 |
| Total Split (%) | 18.1% | 34.0% | | 18.1% | 18.1% | 34.0% | | 18.1% | 29.8% | | 18.1% | 18.1% |
| Maximum Green (s) | 15.0 | 31.0 | | 15.0 | 15.0 | 31.0 | | 15.0 | 25.0 | | 15.0 | 15.0 |
| Yellow Time (s) | 3.7 | 3.7 | | 3.7 | 3.7 | 3.7 | | 3.7 | 4.8 | | 3.7 | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | | 0.0 | 0.0 | 0.5 | | 0.0 | 1.0 | | 0.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 |
| Total Lost Time (s) | 3.7 | 4.2 | | 3.7 | 4.2 | 3.7 | | 3.7 | 5.8 | | 3.7 | 3.7 |
| Lead/Lag | Lead | Lag | | Lead | Lead | Lag | | Lead | Lag | | Lead | Lead |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Existing PM Peak Hour



| Lane Group | SBT | SBR |
|----------------------------|-------|-------|
| Lane Configurations | ↑↑ | |
| Traffic Volume (vph) | 595 | 31 |
| Future Volume (vph) | 595 | 31 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Storage Length (ft) | | 0 |
| Storage Lanes | | 0 |
| Taper Length (ft) | | |
| Lane Util. Factor | 0.95 | 0.95 |
| Ped Bike Factor | 1.00 | |
| Frt | 0.993 | |
| Flt Protected | | |
| Satd. Flow (prot) | 3256 | 0 |
| Flt Permitted | | |
| Satd. Flow (perm) | 3256 | 0 |
| Right Turn on Red | | Yes |
| Satd. Flow (RTOR) | 5 | |
| Link Speed (mph) | 45 | |
| Link Distance (ft) | 1866 | |
| Travel Time (s) | 28.3 | |
| Confl. Peds. (#/hr) | | 4 |
| Confl. Bikes (#/hr) | | |
| Peak Hour Factor | 0.96 | 0.96 |
| Heavy Vehicles (%) | 10% | 9% |
| Adj. Flow (vph) | 620 | 32 |
| Shared Lane Traffic (%) | | |
| Lane Group Flow (vph) | 652 | 0 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Right |
| Median Width(ft) | 12 | |
| Link Offset(ft) | 0 | |
| Crosswalk Width(ft) | 16 | |
| Two way Left Turn Lane | Yes | |
| Headway Factor | 1.00 | 1.00 |
| Turning Speed (mph) | | 9 |
| Turn Type | NA | |
| Protected Phases | 6 | |
| Permitted Phases | | |
| Detector Phase | 6 | |
| Switch Phase | | |
| Minimum Initial (s) | 10.0 | |
| Minimum Split (s) | 27.8 | |
| Total Split (s) | 30.8 | |
| Total Split (%) | 29.8% | |
| Maximum Green (s) | 25.0 | |
| Yellow Time (s) | 4.8 | |
| All-Red Time (s) | 1.0 | |
| Lost Time Adjust (s) | 0.0 | |
| Total Lost Time (s) | 5.8 | |
| Lead/Lag | Lag | |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Existing PM Peak Hour



| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL |
|-------------------------|------|------|-----|------|------|------|-----|------|------|-----|------|------|
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | | Yes | Yes | | Yes | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | | 0.2 | 0.2 | 0.2 | | 0.2 | 0.2 | | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | | 0.1 | 0.1 | 0.1 | | 0.1 | 0.1 | | 0.1 | 0.1 |
| Recall Mode | None | None | | None | None | None | | None | Min | | None | None |
| Walk Time (s) | | 7.0 | | | | 7.0 | | | 7.0 | | | |
| Flash Dont Walk (s) | | 24.0 | | | | 24.0 | | | 15.0 | | | |
| Pedestrian Calls (#/hr) | | 1 | | | | 1 | | | 0 | | | |
| Act Effct Green (s) | 14.5 | 16.9 | | 14.5 | 19.4 | | | 13.2 | 33.6 | | | 13.2 |
| Actuated g/C Ratio | 0.26 | 0.30 | | 0.26 | 0.35 | | | 0.23 | 0.60 | | | 0.23 |
| v/c Ratio | 0.06 | 0.08 | | 0.14 | 0.16 | | | 0.11 | 0.28 | | | 0.07 |
| Control Delay | 30.9 | 9.7 | | 30.3 | 8.6 | | | 31.1 | 17.4 | | | 32.2 |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | | 0.0 | 0.0 | | | 0.0 |
| Total Delay | 30.9 | 9.7 | | 30.3 | 8.6 | | | 31.1 | 17.4 | | | 32.2 |
| LOS | C | A | | C | A | | | C | B | | | C |
| Approach Delay | | 18.2 | | | 17.9 | | | | 18.3 | | | |
| Approach LOS | | B | | | B | | | | B | | | |

Intersection Summary

Area Type: Other
 Cycle Length: 103.4
 Actuated Cycle Length: 56.2
 Natural Cycle: 95
 Control Type: Actuated-Uncoordinated
 Maximum v/c Ratio: 0.36
 Intersection Signal Delay: 19.4 Intersection LOS: B
 Intersection Capacity Utilization 47.6% ICU Level of Service A
 Analysis Period (min) 15

Splits and Phases: 4: SR 113 & Regency Pkwy/Industrial Wy

| | | | |
|--------|--------|--------|--------|
| | | | |
| 18.7 s | 30.8 s | 18.7 s | 35.2 s |
| | | | |
| 18.7 s | 30.8 s | 18.7 s | 35.2 s |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Existing PM Peak Hour



| Lane Group | SBT | SBR |
|-------------------------|------|-----|
| Lead-Lag Optimize? | Yes | |
| Vehicle Extension (s) | 0.2 | |
| Minimum Gap (s) | 1.0 | |
| Time Before Reduce (s) | 1.0 | |
| Time To Reduce (s) | 0.1 | |
| Recall Mode | Min | |
| Walk Time (s) | 7.0 | |
| Flash Dont Walk (s) | 15.0 | |
| Pedestrian Calls (#/hr) | 4 | |
| Act Effct Green (s) | 31.2 | |
| Actuated g/C Ratio | 0.56 | |
| v/c Ratio | 0.36 | |
| Control Delay | 20.3 | |
| Queue Delay | 0.0 | |
| Total Delay | 20.3 | |
| LOS | C | |
| Approach Delay | 20.8 | |
| Approach LOS | C | |
| Intersection Summary | | |

Independence at Dixon TIA

1: SR 113/I-80 EB Ramps & I-80 WB Ramps/Auction Ln

Existing PM Peak Hour

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 2.9 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↕ | ↗ | | ↕ | | ↗ | ↖ | | | ↕ | |
| Traffic Vol, veh/h | 6 | 0 | 499 | 2 | 0 | 1 | 271 | 475 | 2 | 1 | 200 | 12 |
| Future Vol, veh/h | 6 | 0 | 499 | 2 | 0 | 1 | 271 | 475 | 2 | 1 | 200 | 12 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | Free | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 0 | - | - | - | 0 | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, % | 29 | 0 | 11 | 100 | 100 | 0 | 21 | 15 | 100 | 0 | 20 | 13 |
| Mvmt Flow | 6 | 0 | 537 | 2 | 0 | 1 | 291 | 511 | 2 | 1 | 215 | 13 |

| Major/Minor | Minor2 | | Minor1 | | Major1 | | Major2 | | | | | |
|----------------------|--------|------|--------|------|--------|-----|--------|---|---|------|---|---|
| Conflicting Flow All | 1319 | 1319 | - | 1318 | 1324 | 512 | 228 | 0 | 0 | 513 | 0 | 0 |
| Stage 1 | 224 | 224 | - | 1094 | 1094 | - | - | - | - | - | - | - |
| Stage 2 | 1095 | 1095 | - | 224 | 230 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.39 | 6.5 | - | 8.1 | 7.5 | 6.2 | 4.31 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.761 | 4 | - | 4.4 | 4.9 | 3.3 | 2.389 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 118 | 158 | 0 | 85 | 101 | 566 | 1236 | - | - | 1063 | - | - |
| Stage 1 | 721 | 722 | 0 | 172 | 196 | - | - | - | - | - | - | - |
| Stage 2 | 230 | 292 | 0 | 601 | 565 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | - | - | - |
| Mov Cap-1 Maneuver | 96 | 121 | - | 70 | 77 | 566 | 1236 | - | - | 1063 | - | - |
| Mov Cap-2 Maneuver | 96 | 121 | - | 70 | 77 | - | - | - | - | - | - | - |
| Stage 1 | 552 | 721 | - | 132 | 150 | - | - | - | - | - | - | - |
| Stage 2 | 176 | 223 | - | 600 | 564 | - | - | - | - | - | - | - |

| Approach | EB | | WB | | NB | | SB | |
|----------------------|------|--|------|--|-----|--|----|--|
| HCM Control Delay, s | 45.2 | | 42.6 | | 3.2 | | 0 | |
| HCM LOS | E | | E | | | | | |

| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | EBLn2 | WBLn1 | SBL | SBT | SBR |
|-----------------------|-------|-----|-----|-------|-------|-------|-------|-----|-----|
| Capacity (veh/h) | 1236 | - | - | 96 | - | 99 | 1063 | - | - |
| HCM Lane V/C Ratio | 0.236 | - | - | 0.067 | - | 0.033 | 0.001 | - | - |
| HCM Control Delay (s) | 8.8 | - | - | 45.2 | 0 | 42.6 | 8.4 | 0 | - |
| HCM Lane LOS | A | - | - | E | A | E | A | A | - |
| HCM 95th %tile Q(veh) | 0.9 | - | - | 0.2 | - | 0.1 | 0 | - | - |

Independence at Dixon TIA

2: SR 113 & Dorset Dr/E. Dorset Dr

Existing PM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 113 | 7 | 59 | 218 | 15 | 125 | 119 | 540 | 173 | 169 | 443 | 120 |
| v/c Ratio | 0.20 | 0.02 | 0.15 | 0.28 | 0.04 | 0.31 | 0.38 | 0.77 | 0.36 | 0.29 | 0.61 | 0.29 |
| Control Delay | 33.4 | 25.1 | 3.2 | 30.7 | 25.6 | 7.5 | 37.3 | 36.5 | 7.1 | 33.4 | 31.2 | 8.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 33.4 | 25.1 | 3.2 | 30.7 | 25.6 | 7.5 | 37.3 | 36.5 | 7.1 | 33.4 | 31.2 | 8.1 |
| Queue Length 50th (ft) | 21 | 3 | 0 | 43 | 6 | 0 | 47 | 118 | 0 | 32 | 92 | 0 |
| Queue Length 95th (ft) | 67 | 14 | 15 | 117 | 23 | 41 | 141 | 237 | 51 | 94 | 197 | 45 |
| Internal Link Dist (ft) | | 520 | | | 616 | | | 607 | | | 887 | |
| Turn Bay Length (ft) | 150 | | 160 | 195 | | 195 | 200 | | 320 | 235 | | 135 |
| Base Capacity (vph) | 722 | 922 | 893 | 874 | 1006 | 822 | 381 | 1483 | 827 | 677 | 1483 | 710 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.16 | 0.01 | 0.07 | 0.25 | 0.01 | 0.15 | 0.31 | 0.36 | 0.21 | 0.25 | 0.30 | 0.17 |

Intersection Summary

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Existing PM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|-------------------------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 130 | 33 | 71 | 102 | 56 | 76 | 83 | 599 | 72 | 701 |
| v/c Ratio | 0.35 | 0.07 | 0.16 | 0.29 | 0.12 | 0.21 | 0.27 | 0.47 | 0.23 | 0.53 |
| Control Delay | 34.3 | 25.0 | 3.0 | 34.1 | 26.0 | 4.3 | 34.8 | 25.2 | 34.1 | 24.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.3 | 25.0 | 3.0 | 34.1 | 26.0 | 4.3 | 34.8 | 25.2 | 34.1 | 24.8 |
| Queue Length 50th (ft) | 48 | 12 | 0 | 37 | 20 | 0 | 31 | 117 | 26 | 133 |
| Queue Length 95th (ft) | 141 | 38 | 16 | 117 | 57 | 20 | 101 | 243 | 91 | 283 |
| Internal Link Dist (ft) | | 357 | | | 279 | | | 1083 | | 607 |
| Turn Bay Length (ft) | 275 | | | 180 | | 230 | 290 | | 285 | |
| Base Capacity (vph) | 483 | 1047 | 860 | 465 | 1047 | 706 | 459 | 1623 | 427 | 1637 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.27 | 0.03 | 0.08 | 0.22 | 0.05 | 0.11 | 0.18 | 0.37 | 0.17 | 0.43 |

Intersection Summary

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy



























Existing PM Peak Hour



| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
|-----------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 26 | 39 | 53 | 70 | 43 | 560 | 24 | 652 |
| v/c Ratio | 0.06 | 0.08 | 0.14 | 0.16 | 0.11 | 0.28 | 0.07 | 0.36 |
| Control Delay | 30.9 | 9.7 | 30.3 | 8.6 | 31.1 | 17.4 | 32.2 | 20.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 30.9 | 9.7 | 30.3 | 8.6 | 31.1 | 17.4 | 32.2 | 20.3 |
| Queue Length 50th (ft) | 9 | 1 | 19 | 1 | 15 | 72 | 8 | 128 |
| Queue Length 95th (ft) | 39 | 23 | 66 | 32 | 57 | 212 | 38 | 252 |
| Internal Link Dist (ft) | | 656 | | 824 | | 393 | | 1786 |
| Turn Bay Length (ft) | 150 | | 250 | | 115 | | 190 | |
| Base Capacity (vph) | 561 | 1009 | 518 | 796 | 593 | 2071 | 527 | 1966 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.05 | 0.04 | 0.10 | 0.09 | 0.07 | 0.27 | 0.05 | 0.33 |
| Intersection Summary | | | | | | | | |

Independence at Dixon TIA
2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term AM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|----------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL |
| Lane Configurations |   |  |  |   |  |  | | |  |   |  |   |
| Traffic Volume (vph) | 67 | 14 | 28 | 80 | 6 | 35 | 35 | 88 | 447 | 116 | 1 | 101 |
| Future Volume (vph) | 67 | 14 | 28 | 80 | 6 | 35 | 35 | 88 | 447 | 116 | 1 | 101 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 160 | 195 | | 195 | | 200 | | 320 | | 235 |
| Storage Lanes | 2 | | 1 | 2 | | 1 | | 1 | | 1 | | 2 |
| Taper Length (ft) | 25 | | | 25 | | | | 25 | | | | 25 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.95 | 0.97 |
| Ped Bike Factor | | | 0.99 | | | 0.99 | | | | | | |
| Frt | | | 0.850 | | | 0.850 | | | | 0.850 | | |
| Flt Protected | 0.950 | | | 0.950 | | | | 0.950 | | | | 0.950 |
| Satd. Flow (prot) | 2968 | 1652 | 1553 | 3273 | 1900 | 1442 | 0 | 1780 | 3139 | 1583 | 0 | 3157 |
| Flt Permitted | 0.950 | | | 0.950 | | | | 0.950 | | | | 0.950 |
| Satd. Flow (perm) | 2968 | 1652 | 1531 | 3273 | 1900 | 1423 | 0 | 1780 | 3139 | 1583 | 0 | 3157 |
| Right Turn on Red | | | Yes | | | Yes | | | | Yes | | |
| Satd. Flow (RTOR) | | | 87 | | | 87 | | | | 133 | | |
| Link Speed (mph) | | 35 | | | 35 | | | | 45 | | | |
| Link Distance (ft) | | 600 | | | 696 | | | | 687 | | | |
| Travel Time (s) | | 11.7 | | | 13.6 | | | | 10.4 | | | |
| Confl. Peds. (#/hr) | | | 2 | | | 1 | | | | | | |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Heavy Vehicles (%) | 18% | 15% | 4% | 7% | 0% | 12% | 0% | 2% | 15% | 2% | 0% | 11% |
| Adj. Flow (vph) | 77 | 16 | 32 | 92 | 7 | 40 | 40 | 101 | 514 | 133 | 1 | 116 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 77 | 16 | 32 | 92 | 7 | 40 | 0 | 141 | 514 | 133 | 0 | 117 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | R NA | Left | Left | Right | R NA | Left |
| Median Width(ft) | | 24 | | | 24 | | | | 24 | | | |
| Link Offset(ft) | | 0 | | | 0 | | | | 0 | | | |
| Crosswalk Width(ft) | | 16 | | | 16 | | | | 16 | | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 15 | | 9 | 9 | 15 | | 9 | 9 | 15 |
| Turn Type | Prot | NA | Perm | Prot | NA | Perm | Prot | Prot | NA | Perm | Prot | Prot |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 5 | 2 | | 1 | 1 |
| Permitted Phases | | | 4 | | | 8 | | | | 2 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 5 | 2 | 2 | 1 | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 13.0 | 12.0 | 12.0 | 13.0 | 12.0 | 12.0 | 12.0 | 12.0 | 10.0 | 10.0 | 13.0 | 13.0 |
| Minimum Split (s) | 16.7 | 41.6 | 41.6 | 16.0 | 41.6 | 41.6 | 15.7 | 15.7 | 36.8 | 36.8 | 16.7 | 16.7 |
| Total Split (s) | 20.7 | 41.6 | 41.6 | 18.7 | 41.6 | 41.6 | 18.7 | 18.7 | 36.8 | 36.8 | 18.7 | 18.7 |
| Total Split (%) | 17.3% | 34.7% | 34.7% | 15.6% | 34.7% | 34.7% | 15.6% | 15.6% | 30.7% | 30.7% | 15.6% | 15.6% |
| Maximum Green (s) | 17.0 | 37.0 | 37.0 | 15.7 | 37.0 | 37.0 | 15.0 | 15.0 | 31.0 | 31.0 | 15.0 | 15.0 |
| Yellow Time (s) | 3.7 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 3.7 | 3.7 | 4.8 | 4.8 | 3.7 | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | 0.5 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | 1.0 | 0.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 |
| Total Lost Time (s) | 3.7 | 4.6 | 4.6 | 3.0 | 4.6 | 4.6 | | 3.7 | 5.8 | 5.8 | | 3.7 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term AM Peak Hour



| Lane Group | SBT | SBR |
|----------------------------|-------|-------|
| Lane Configurations | ↑↑ | ↑ |
| Traffic Volume (vph) | 404 | 72 |
| Future Volume (vph) | 404 | 72 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Storage Length (ft) | | 135 |
| Storage Lanes | | 1 |
| Taper Length (ft) | | |
| Lane Util. Factor | 0.95 | 1.00 |
| Ped Bike Factor | | |
| Frt | | 0.850 |
| Flt Protected | | |
| Satd. Flow (prot) | 3139 | 1369 |
| Flt Permitted | | |
| Satd. Flow (perm) | 3139 | 1369 |
| Right Turn on Red | | Yes |
| Satd. Flow (RTOR) | | 83 |
| Link Speed (mph) | 45 | |
| Link Distance (ft) | 967 | |
| Travel Time (s) | 14.7 | |
| Confl. Peds. (#/hr) | | |
| Peak Hour Factor | 0.87 | 0.87 |
| Heavy Vehicles (%) | 15% | 18% |
| Adj. Flow (vph) | 464 | 83 |
| Shared Lane Traffic (%) | | |
| Lane Group Flow (vph) | 464 | 83 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Right |
| Median Width(ft) | 24 | |
| Link Offset(ft) | 0 | |
| Crosswalk Width(ft) | 16 | |
| Two way Left Turn Lane | | |
| Headway Factor | 1.00 | 1.00 |
| Turning Speed (mph) | | 9 |
| Turn Type | NA | Perm |
| Protected Phases | 6 | |
| Permitted Phases | | 6 |
| Detector Phase | 6 | 6 |
| Switch Phase | | |
| Minimum Initial (s) | 10.0 | 10.0 |
| Minimum Split (s) | 38.8 | 38.8 |
| Total Split (s) | 38.8 | 38.8 |
| Total Split (%) | 32.4% | 32.4% |
| Maximum Green (s) | 33.0 | 33.0 |
| Yellow Time (s) | 4.8 | 4.8 |
| All-Red Time (s) | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |
| Total Lost Time (s) | 5.8 | 5.8 |
| Lead/Lag | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term AM Peak Hour

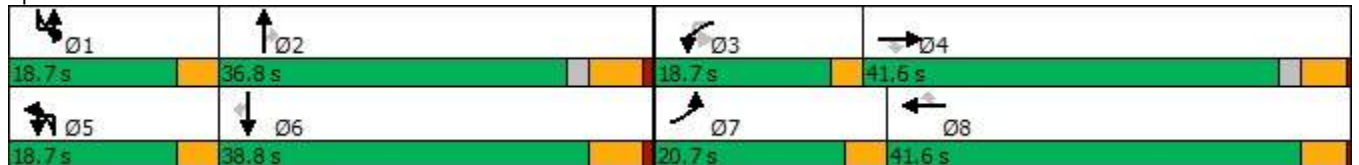


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 | 3.0 | 1.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.2 | 1.2 | 1.0 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | Min | Min | None | None |
| Walk Time (s) | | 7.0 | 7.0 | | 7.0 | 7.0 | | | 7.0 | 7.0 | | |
| Flash Dont Walk (s) | | 30.0 | 30.0 | | 30.0 | 30.0 | | | 24.0 | 24.0 | | |
| Pedestrian Calls (#/hr) | | 2 | 2 | | 1 | 1 | | | 0 | 0 | | |
| Act Effct Green (s) | 16.8 | 18.9 | 18.9 | 17.0 | 18.5 | 18.5 | | 15.9 | 23.9 | 23.9 | | 16.8 |
| Actuated g/C Ratio | 0.26 | 0.30 | 0.30 | 0.27 | 0.29 | 0.29 | | 0.25 | 0.37 | 0.37 | | 0.26 |
| v/c Ratio | 0.10 | 0.03 | 0.06 | 0.11 | 0.01 | 0.08 | | 0.32 | 0.44 | 0.20 | | 0.14 |
| Control Delay | 30.7 | 23.6 | 0.2 | 30.4 | 23.8 | 0.3 | | 33.6 | 27.3 | 6.8 | | 30.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 |
| Total Delay | 30.7 | 23.6 | 0.2 | 30.4 | 23.8 | 0.3 | | 33.6 | 27.3 | 6.8 | | 30.6 |
| LOS | C | C | A | C | C | A | | C | C | A | | C |
| Approach Delay | | 22.0 | | | 21.5 | | | | 25.0 | | | |
| Approach LOS | | C | | | C | | | | C | | | |

Intersection Summary

| | |
|------------------------------------|------------------------|
| Area Type: | Other |
| Cycle Length: | 119.8 |
| Actuated Cycle Length: | 64 |
| Natural Cycle: | 115 |
| Control Type: | Actuated-Uncoordinated |
| Maximum v/c Ratio: | 0.44 |
| Intersection Signal Delay: | 24.5 |
| Intersection LOS: | C |
| Intersection Capacity Utilization: | 60.0% |
| ICU Level of Service: | B |
| Analysis Period (min): | 15 |

Splits and Phases: 2: SR 113 & Dorset Dr/E. Dorset Dr



Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term AM Peak Hour



| Lane Group | SBT | SBR |
|-------------------------|------|------|
| Vehicle Extension (s) | 0.2 | 0.2 |
| Minimum Gap (s) | 3.0 | 3.0 |
| Time Before Reduce (s) | 1.2 | 1.2 |
| Time To Reduce (s) | 0.1 | 0.1 |
| Recall Mode | Min | Min |
| Walk Time (s) | 7.0 | 7.0 |
| Flash Dont Walk (s) | 26.0 | 26.0 |
| Pedestrian Calls (#/hr) | 0 | 0 |
| Act Effct Green (s) | 24.3 | 24.3 |
| Actuated g/C Ratio | 0.38 | 0.38 |
| v/c Ratio | 0.39 | 0.15 |
| Control Delay | 26.8 | 8.3 |
| Queue Delay | 0.0 | 0.0 |
| Total Delay | 26.8 | 8.3 |
| LOS | C | A |
| Approach Delay | 25.1 | |
| Approach LOS | C | |
| Intersection Summary | | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term AM Peak Hour



| Lane Group | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
|----------------------------|-------|-------|-------|-------|--------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | ↔ | ↑ | ↗ | | ↖ | ↑ | ↗ | | ↔ | ↑↔ | |
| Traffic Volume (vph) | 15 | 196 | 59 | 47 | 1 | 58 | 31 | 52 | 76 | 37 | 429 | 92 |
| Future Volume (vph) | 15 | 196 | 59 | 47 | 1 | 58 | 31 | 52 | 76 | 37 | 429 | 92 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | | 275 | | 0 | | 180 | | 230 | | 290 | | 0 |
| Storage Lanes | | 1 | | 1 | | 1 | | 1 | | 1 | | 0 |
| Taper Length (ft) | | 25 | | | | 25 | | | | 25 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | | | | 0.99 | | | | | | | 1.00 | |
| Frt | | | | 0.850 | | | | 0.850 | | | 0.973 | |
| Flt Protected | | 0.950 | | | | 0.950 | | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1756 | 1900 | 1495 | 0 | 1689 | 1900 | 1196 | 0 | 1753 | 3148 | 0 |
| Flt Permitted | | 0.950 | | | | 0.247 | | | | 0.950 | | |
| Satd. Flow (perm) | 0 | 1756 | 1900 | 1476 | 0 | 439 | 1900 | 1196 | 0 | 1753 | 3148 | 0 |
| Right Turn on Red | | | | Yes | | | | Yes | | | | Yes |
| Satd. Flow (RTOR) | | | | 104 | | | | 104 | | | | 23 |
| Link Speed (mph) | | | 35 | | | | 45 | | | | 45 | |
| Link Distance (ft) | | | 437 | | | | 359 | | | | 1163 | |
| Travel Time (s) | | | 8.5 | | | | 5.4 | | | | 17.6 | |
| Confl. Peds. (#/hr) | | | | 1 | | | | | | | | 3 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.92 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (%) | 0% | 3% | 0% | 8% | 0% | 7% | 0% | 35% | 0% | 9% | 12% | 8% |
| Adj. Flow (vph) | 16 | 206 | 62 | 49 | 1 | 61 | 33 | 55 | 80 | 39 | 452 | 97 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 222 | 62 | 49 | 0 | 62 | 33 | 55 | 0 | 119 | 549 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | R NA | Left | Left | Right | R NA | Left | Left | Right | R NA | Left | Left | Right |
| Median Width(ft) | | | 12 | | | | 12 | | | | 12 | |
| Link Offset(ft) | | | 0 | | | | 0 | | | | 0 | |
| Crosswalk Width(ft) | | | 16 | | | | 16 | | | | 16 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 9 | 15 | | 9 | 9 | 15 | | 9 | 9 | 15 | | 9 |
| Turn Type | Prot | Prot | NA | Perm | custom | Prot | NA | Perm | Prot | Prot | NA | |
| Protected Phases | 7 | 7 | 4 | | | 3 | 8 | | 5 | 5 | 2 | |
| Permitted Phases | | | | 4 | 3 | | | 8 | | | | |
| Detector Phase | 7 | 7 | 4 | 4 | 3 | 3 | 8 | 8 | 5 | 5 | 2 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 10.0 | 10.0 | 10.0 | |
| Minimum Split (s) | 14.7 | 14.7 | 36.2 | 36.2 | 14.7 | 14.7 | 36.2 | 36.2 | 13.7 | 13.7 | 33.8 | |
| Total Split (s) | 18.7 | 18.7 | 36.2 | 36.2 | 18.7 | 18.7 | 36.2 | 36.2 | 18.7 | 18.7 | 33.8 | |
| Total Split (%) | 17.4% | 17.4% | 33.7% | 33.7% | 17.4% | 17.4% | 33.7% | 33.7% | 17.4% | 17.4% | 31.5% | |
| Maximum Green (s) | 15.0 | 15.0 | 32.0 | 32.0 | 15.0 | 15.0 | 32.0 | 32.0 | 15.0 | 15.0 | 28.0 | |
| Yellow Time (s) | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 4.8 | |
| All-Red Time (s) | 0.0 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 3.7 | 4.2 | 4.2 | | | 3.7 | 4.2 | | 3.7 | 5.8 | |
| Lead/Lag | Lead | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead | Lead | Lag | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term AM Peak Hour



| Lane Group | SBU | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|
| Lane Configurations | | | | |
| Traffic Volume (vph) | 3 | 75 | 399 | 70 |
| Future Volume (vph) | 3 | 75 | 399 | 70 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | | 285 | | 0 |
| Storage Lanes | | 1 | | 0 |
| Taper Length (ft) | | 25 | | |
| Lane Util. Factor | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | | | | |
| Frt | | | 0.978 | |
| Flt Protected | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1526 | 3204 | 0 |
| Flt Permitted | | 0.950 | | |
| Satd. Flow (perm) | 0 | 1526 | 3204 | 0 |
| Right Turn on Red | | | | Yes |
| Satd. Flow (RTOR) | | | 18 | |
| Link Speed (mph) | | | 45 | |
| Link Distance (ft) | | | 687 | |
| Travel Time (s) | | | 10.4 | |
| Confl. Peds. (#/hr) | | | | |
| Confl. Bikes (#/hr) | | | | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (%) | 0% | 19% | 12% | 0% |
| Adj. Flow (vph) | 3 | 79 | 420 | 74 |
| Shared Lane Traffic (%) | | | | |
| Lane Group Flow (vph) | 0 | 82 | 494 | 0 |
| Enter Blocked Intersection | No | No | No | No |
| Lane Alignment | R NA | Left | Left | Right |
| Median Width(ft) | | | 12 | |
| Link Offset(ft) | | | 0 | |
| Crosswalk Width(ft) | | | 16 | |
| Two way Left Turn Lane | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 9 | 15 | | 9 |
| Turn Type | Prot | Prot | NA | |
| Protected Phases | 1 | 1 | 6 | |
| Permitted Phases | | | | |
| Detector Phase | 1 | 1 | 6 | |
| Switch Phase | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | 10.0 | |
| Minimum Split (s) | 14.7 | 14.7 | 33.8 | |
| Total Split (s) | 18.7 | 18.7 | 33.8 | |
| Total Split (%) | 17.4% | 17.4% | 31.5% | |
| Maximum Green (s) | 15.0 | 15.0 | 28.0 | |
| Yellow Time (s) | 3.7 | 3.7 | 4.8 | |
| All-Red Time (s) | 0.0 | 0.0 | 1.0 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 3.7 | 5.8 | |
| Lead/Lag | Lead | Lead | Lag | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term AM Peak Hour



| Lane Group | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | None | None | None | Min |
| Walk Time (s) | | | 7.0 | 7.0 | | | 7.0 | 7.0 | | | | 7.0 |
| Flash Dont Walk (s) | | | 25.0 | 25.0 | | | 25.0 | 25.0 | | | | 21.0 |
| Pedestrian Calls (#/hr) | | | 1 | 1 | | | 0 | 0 | | | | 3 |
| Act Effct Green (s) | | 15.4 | 15.3 | 15.3 | | 16.1 | 16.1 | 16.1 | | 12.1 | 16.9 | |
| Actuated g/C Ratio | | 0.22 | 0.22 | 0.22 | | 0.23 | 0.23 | 0.23 | | 0.18 | 0.25 | |
| v/c Ratio | | 0.57 | 0.15 | 0.12 | | 0.61 | 0.07 | 0.15 | | 0.39 | 0.69 | |
| Control Delay | | 37.9 | 26.9 | 0.6 | | 60.0 | 25.8 | 1.6 | | 37.0 | 31.0 | |
| Queue Delay | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | | 37.9 | 26.9 | 0.6 | | 60.0 | 25.8 | 1.6 | | 37.0 | 31.0 | |
| LOS | | D | C | A | | E | C | A | | D | C | |
| Approach Delay | | | 30.4 | | | | 31.1 | | | | | 32.1 |
| Approach LOS | | | C | | | | C | | | | | C |

Intersection Summary

Area Type: Other
 Cycle Length: 107.4
 Actuated Cycle Length: 68.9
 Natural Cycle: 100
 Control Type: Actuated-Uncoordinated
 Maximum v/c Ratio: 0.69
 Intersection Signal Delay: 30.9
 Intersection LOS: C
 Intersection Capacity Utilization 60.7%
 ICU Level of Service B
 Analysis Period (min) 15

Splits and Phases: 3: SR 113 & N. Lincoln St/Vaughn Rd

| | | | |
|--------|--------|--------|--------|
| Ø1 | Ø2 | Ø3 | Ø4 |
| 18.7 s | 33.8 s | 18.7 s | 36.2 s |
| Ø5 | Ø6 | Ø7 | Ø8 |
| 18.7 s | 33.8 s | 18.7 s | 36.2 s |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term AM Peak Hour



| Lane Group | SBU | SBL | SBT | SBR |
|-------------------------|------|------|------|-----|
| Lead-Lag Optimize? | Yes | Yes | Yes | |
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | |
| Minimum Gap (s) | 1.0 | 1.0 | 3.0 | |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | |
| Recall Mode | None | None | Min | |
| Walk Time (s) | | | 7.0 | |
| Flash Dont Walk (s) | | | 21.0 | |
| Pedestrian Calls (#/hr) | | | 0 | |
| Act Effct Green (s) | | 12.8 | 17.3 | |
| Actuated g/C Ratio | | 0.19 | 0.25 | |
| v/c Ratio | | 0.29 | 0.60 | |
| Control Delay | | 35.7 | 28.8 | |
| Queue Delay | | 0.0 | 0.0 | |
| Total Delay | | 35.7 | 28.8 | |
| LOS | | D | C | |
| Approach Delay | | | 29.8 | |
| Approach LOS | | | C | |
| Intersection Summary | | | | |

Independence at Dixon TIA
4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 32 | 7 | 53 | 1 | 22 | 1 | 19 | 30 | 539 | 46 | 17 | 45 |
| Future Volume (vph) | 32 | 7 | 53 | 1 | 22 | 1 | 19 | 30 | 539 | 46 | 17 | 45 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 0 | | 250 | | 0 | 115 | | 0 | | 190 |
| Storage Lanes | 1 | | 0 | | 1 | | 0 | 1 | | 0 | | 1 |
| Taper Length (ft) | 25 | | | | 25 | | | 25 | | | | 25 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 |
| Ped Bike Factor | | 0.99 | | | | | | | | | | |
| Frt | | 0.868 | | | | 0.857 | | | 0.988 | | | |
| Flt Protected | 0.950 | | | | 0.950 | | | 0.950 | | | | 0.950 |
| Satd. Flow (prot) | 1597 | 1523 | 0 | 0 | 1479 | 1178 | 0 | 1687 | 3304 | 0 | 0 | 1555 |
| Flt Permitted | 0.950 | | | | 0.950 | | | 0.950 | | | | 0.950 |
| Satd. Flow (perm) | 1597 | 1523 | 0 | 0 | 1479 | 1178 | 0 | 1687 | 3304 | 0 | 0 | 1555 |
| Right Turn on Red | | | Yes | | | | Yes | | | Yes | | |
| Satd. Flow (RTOR) | | 58 | | | | 21 | | 8 | | | | |
| Link Speed (mph) | | 30 | | | | 30 | | 30 | | | | |
| Link Distance (ft) | | 736 | | | | 904 | | 473 | | | | |
| Travel Time (s) | | 16.7 | | | | 20.5 | | 10.8 | | | | |
| Confl. Bikes (#/hr) | | 1 | 2 | | | | | | | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 13% | 29% | 4% | 0% | 23% | 0% | 40% | 7% | 7% | 19% | 0% | 22% |
| Adj. Flow (vph) | 35 | 8 | 58 | 1 | 24 | 1 | 21 | 33 | 586 | 50 | 18 | 49 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 35 | 66 | 0 | 0 | 25 | 22 | 0 | 33 | 636 | 0 | 0 | 67 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | R NA | Left | Left | Right | Left | Left | Right | R NA | Left |
| Median Width(ft) | | 12 | | | | 12 | | 12 | | | | |
| Link Offset(ft) | | 0 | | | | 0 | | 0 | | | | |
| Crosswalk Width(ft) | | 16 | | | | 16 | | 16 | | | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 9 | 15 | | 9 | 15 | | 9 | 9 | 15 |
| Turn Type | Prot | NA | | Prot | Prot | NA | | Prot | NA | | Prot | Prot |
| Protected Phases | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 1 |
| Permitted Phases | | | | | | | | | | | | |
| Detector Phase | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | | 11.0 | 11.0 | 11.0 | | 10.0 | 10.0 | | 10.0 | 10.0 |
| Minimum Split (s) | 14.7 | 35.2 | | 14.7 | 14.7 | 35.2 | | 13.7 | 27.8 | | 13.7 | 13.7 |
| Total Split (s) | 18.7 | 35.2 | | 18.7 | 18.7 | 35.2 | | 18.7 | 30.8 | | 18.7 | 18.7 |
| Total Split (%) | 18.1% | 34.0% | | 18.1% | 18.1% | 34.0% | | 18.1% | 29.8% | | 18.1% | 18.1% |
| Maximum Green (s) | 15.0 | 31.0 | | 15.0 | 15.0 | 31.0 | | 15.0 | 25.0 | | 15.0 | 15.0 |
| Yellow Time (s) | 3.7 | 3.7 | | 3.7 | 3.7 | 3.7 | | 3.7 | 4.8 | | 3.7 | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | | 0.0 | 0.0 | 0.5 | | 0.0 | 1.0 | | 0.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 |
| Total Lost Time (s) | 3.7 | 4.2 | | 3.7 | 4.2 | 3.7 | | 3.7 | 5.8 | | 3.7 | 3.7 |
| Lead/Lag | Lead | Lag | | Lead | Lead | Lag | | Lead | Lag | | Lead | Lead |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | | Yes | Yes | | Yes | Yes |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term AM Peak Hour



| Lane Group | SBT | SBR |
|----------------------------|-------|-------|
| Lane Configurations | ↑↑ | |
| Traffic Volume (vph) | 342 | 18 |
| Future Volume (vph) | 342 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Storage Length (ft) | | 0 |
| Storage Lanes | | 0 |
| Taper Length (ft) | | |
| Lane Util. Factor | 0.95 | 0.95 |
| Ped Bike Factor | 1.00 | |
| Frt | 0.992 | |
| Flt Protected | | |
| Satd. Flow (prot) | 3253 | 0 |
| Flt Permitted | | |
| Satd. Flow (perm) | 3253 | 0 |
| Right Turn on Red | | Yes |
| Satd. Flow (RTOR) | 5 | |
| Link Speed (mph) | 45 | |
| Link Distance (ft) | 1866 | |
| Travel Time (s) | 28.3 | |
| Confl. Bikes (#/hr) | | 1 |
| Peak Hour Factor | 0.92 | 0.92 |
| Heavy Vehicles (%) | 10% | 9% |
| Adj. Flow (vph) | 372 | 20 |
| Shared Lane Traffic (%) | | |
| Lane Group Flow (vph) | 392 | 0 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Right |
| Median Width(ft) | 12 | |
| Link Offset(ft) | 0 | |
| Crosswalk Width(ft) | 16 | |
| Two way Left Turn Lane | Yes | |
| Headway Factor | 1.00 | 1.00 |
| Turning Speed (mph) | | 9 |
| Turn Type | NA | |
| Protected Phases | 6 | |
| Permitted Phases | | |
| Detector Phase | 6 | |
| Switch Phase | | |
| Minimum Initial (s) | 10.0 | |
| Minimum Split (s) | 27.8 | |
| Total Split (s) | 30.8 | |
| Total Split (%) | 29.8% | |
| Maximum Green (s) | 25.0 | |
| Yellow Time (s) | 4.8 | |
| All-Red Time (s) | 1.0 | |
| Lost Time Adjust (s) | 0.0 | |
| Total Lost Time (s) | 5.8 | |
| Lead/Lag | Lag | |
| Lead-Lag Optimize? | Yes | |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL |
|-------------------------|------|------|-----|------|------|------|-----|------|------|-----|------|------|
| Vehicle Extension (s) | 0.2 | 0.2 | | 0.2 | 0.2 | 0.2 | | 0.2 | 0.2 | | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | | 0.1 | 0.1 | 0.1 | | 0.1 | 0.1 | | 0.1 | 0.1 |
| Recall Mode | None | None | | None | None | None | | None | Min | | None | None |
| Walk Time (s) | | 7.0 | | | | 7.0 | | | 7.0 | | | |
| Flash Dont Walk (s) | | 24.0 | | | | 24.0 | | | 15.0 | | | |
| Pedestrian Calls (#/hr) | | 2 | | | | 0 | | | 0 | | | |
| Act Effct Green (s) | 16.4 | 16.2 | | | 14.0 | 16.2 | | 12.8 | 29.0 | | | 12.8 |
| Actuated g/C Ratio | 0.31 | 0.31 | | | 0.27 | 0.31 | | 0.24 | 0.55 | | | 0.24 |
| v/c Ratio | 0.07 | 0.13 | | | 0.06 | 0.06 | | 0.08 | 0.35 | | | 0.18 |
| Control Delay | 24.8 | 8.9 | | | 29.4 | 11.1 | | 29.6 | 18.8 | | | 28.9 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | | | 0.0 |
| Total Delay | 24.8 | 8.9 | | | 29.4 | 11.1 | | 29.6 | 18.8 | | | 28.9 |
| LOS | C | A | | | C | B | | C | B | | | C |
| Approach Delay | | 14.4 | | | | 20.8 | | | 19.3 | | | |
| Approach LOS | | B | | | | C | | | B | | | |

Intersection Summary

| | |
|-----------------------------------|------------------------|
| Area Type: | Other |
| Cycle Length: | 103.4 |
| Actuated Cycle Length: | 52.4 |
| Natural Cycle: | 95 |
| Control Type: | Actuated-Uncoordinated |
| Maximum v/c Ratio: | 0.35 |
| Intersection Signal Delay: | 18.4 |
| Intersection LOS: | B |
| Intersection Capacity Utilization | 45.5% |
| ICU Level of Service | A |
| Analysis Period (min) | 15 |

Splits and Phases: 4: SR 113 & Regency Pkwy/Industrial Wy

| | | | |
|--------|--------|--------|--------|
| | | | |
| 18.7 s | 30.8 s | 18.7 s | 35.2 s |
| | | | |
| 18.7 s | 30.8 s | 18.7 s | 35.2 s |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term AM Peak Hour



| Lane Group | SBT | SBR |
|-------------------------|------|-----|
| Vehicle Extension (s) | 0.2 | |
| Minimum Gap (s) | 1.0 | |
| Time Before Reduce (s) | 1.0 | |
| Time To Reduce (s) | 0.1 | |
| Recall Mode | Min | |
| Walk Time (s) | 7.0 | |
| Flash Dont Walk (s) | 15.0 | |
| Pedestrian Calls (#/hr) | 1 | |
| Act Effct Green (s) | 32.2 | |
| Actuated g/C Ratio | 0.61 | |
| v/c Ratio | 0.20 | |
| Control Delay | 15.6 | |
| Queue Delay | 0.0 | |
| Total Delay | 15.6 | |
| LOS | B | |
| Approach Delay | 17.6 | |
| Approach LOS | B | |
| Intersection Summary | | |

Independence at Dixon TIA

1: SR 113/I-80 EB Ramps & I-80 WB Ramps/Auction Ln

Near-Term AM Peak Hour

| Intersection | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 2.2 | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL | SBT | SBR |
| Lane Configurations | | ↖ | ↗ | | ↖ | | ↖ | ↗ | | | | ↖ | |
| Traffic Vol, veh/h | 7 | 0 | 431 | 1 | 2 | 0 | 157 | 397 | 1 | 1 | 1 | 164 | 13 |
| Future Vol, veh/h | 7 | 0 | 431 | 1 | 2 | 0 | 157 | 397 | 1 | 1 | 1 | 164 | 13 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | Free | - | - | None | - | - | None | - | - | - | None |
| Storage Length | - | - | 0 | - | - | - | 0 | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | - | 0 | - |
| Peak Hour Factor | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| Heavy Vehicles, % | 29 | 0 | 11 | 100 | 100 | 0 | 21 | 15 | 100 | 0 | 0 | 20 | 13 |
| Mvmt Flow | 8 | 0 | 501 | 1 | 2 | 0 | 183 | 462 | 1 | 1 | 1 | 191 | 15 |

| Major/Minor | Minor2 | | Minor1 | | Major1 | | Major2 | | | | | | |
|----------------------|--------|------|--------|------|--------|-----|--------|---|---|---|------|---|---|
| Conflicting Flow All | 1031 | 1032 | - | 1030 | 1039 | 463 | 206 | 0 | 0 | - | 463 | 0 | 0 |
| Stage 1 | 201 | 203 | - | 829 | 829 | - | - | - | - | - | - | - | - |
| Stage 2 | 830 | 829 | - | 201 | 210 | - | - | - | - | - | - | - | - |
| Critical Hdwy | 7.39 | 6.5 | - | 8.1 | 7.5 | 6.2 | 4.31 | - | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.761 | 4 | - | 4.4 | 4.9 | 3.3 | 2.389 | - | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 188 | 235 | 0 | 142 | 158 | 603 | 1260 | - | - | - | 1109 | - | - |
| Stage 1 | 743 | 737 | 0 | 254 | 274 | - | - | - | - | - | - | - | - |
| Stage 2 | 328 | 388 | 0 | 621 | 578 | - | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | | | - | - |
| Mov Cap-1 Maneuver | 165 | 201 | - | 126 | 135 | 603 | 1260 | - | - | ~ | ~ | - | - |
| Mov Cap-2 Maneuver | 165 | 201 | - | 126 | 135 | - | - | - | - | - | - | - | - |
| Stage 1 | 635 | 737 | - | 217 | 234 | - | - | - | - | - | - | - | - |
| Stage 2 | 278 | 332 | - | 621 | 578 | - | - | - | - | - | - | - | - |

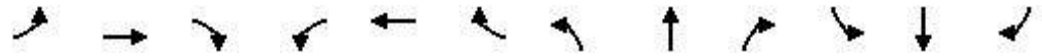
| Approach | EB | | WB | | NB | | SB | |
|----------------------|------|--|----|--|-----|--|----|--|
| HCM Control Delay, s | 27.9 | | 33 | | 2.4 | | | |
| HCM LOS | D | | D | | | | | |

| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | EBLn2 | WBLn1 | SBL | SBT | SBR |
|-----------------------|-------|-----|-----|-------|-------|-------|-----|-----|-----|
| Capacity (veh/h) | 1260 | - | - | 165 | - | 132 | ~ | - | - |
| HCM Lane V/C Ratio | 0.145 | - | - | 0.049 | - | 0.026 | ~ | - | - |
| HCM Control Delay (s) | 8.3 | - | - | 27.9 | 0 | 33 | - | - | - |
| HCM Lane LOS | A | - | - | D | A | D | - | - | - |
| HCM 95th %tile Q(veh) | 0.5 | - | - | 0.2 | - | 0.1 | ~ | - | - |

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 77 | 16 | 32 | 92 | 7 | 40 | 141 | 514 | 133 | 117 | 464 | 83 |
| v/c Ratio | 0.10 | 0.03 | 0.06 | 0.11 | 0.01 | 0.08 | 0.32 | 0.44 | 0.20 | 0.14 | 0.39 | 0.15 |
| Control Delay | 30.7 | 23.6 | 0.2 | 30.4 | 23.8 | 0.3 | 33.6 | 27.3 | 6.8 | 30.6 | 26.8 | 8.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 30.7 | 23.6 | 0.2 | 30.4 | 23.8 | 0.3 | 33.6 | 27.3 | 6.8 | 30.6 | 26.8 | 8.3 |
| Queue Length 50th (ft) | 14 | 6 | 0 | 17 | 3 | 0 | 55 | 112 | 0 | 22 | 97 | 0 |
| Queue Length 95th (ft) | 45 | 21 | 0 | 52 | 13 | 0 | 150 | 218 | 43 | 63 | 201 | 36 |
| Internal Link Dist (ft) | | 520 | | | 616 | | | 607 | | | 887 | |
| Turn Bay Length (ft) | 150 | | 160 | 195 | | 195 | 200 | | 320 | 235 | | 135 |
| Base Capacity (vph) | 1018 | 1078 | 1029 | 1037 | 1196 | 928 | 538 | 1830 | 978 | 956 | 1830 | 833 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.08 | 0.01 | 0.03 | 0.09 | 0.01 | 0.04 | 0.26 | 0.28 | 0.14 | 0.12 | 0.25 | 0.10 |

Intersection Summary

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|-------------------------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 222 | 62 | 49 | 62 | 33 | 55 | 119 | 549 | 82 | 494 |
| v/c Ratio | 0.57 | 0.15 | 0.12 | 0.61 | 0.07 | 0.15 | 0.39 | 0.69 | 0.29 | 0.60 |
| Control Delay | 37.9 | 26.9 | 0.6 | 60.0 | 25.8 | 1.6 | 37.0 | 31.0 | 35.7 | 28.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 37.9 | 26.9 | 0.6 | 60.0 | 25.8 | 1.6 | 37.0 | 31.0 | 35.7 | 28.8 |
| Queue Length 50th (ft) | 86 | 23 | 0 | 24 | 12 | 0 | 47 | 112 | 31 | 96 |
| Queue Length 95th (ft) | #287 | 62 | 0 | #131 | 38 | 4 | 134 | 224 | 101 | 205 |
| Internal Link Dist (ft) | | 357 | | | 279 | | | 1083 | | 607 |
| Turn Bay Length (ft) | 275 | | | 180 | | 230 | 290 | | 285 | |
| Base Capacity (vph) | 437 | 1010 | 833 | 109 | 1010 | 684 | 436 | 1477 | 380 | 1500 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.51 | 0.06 | 0.06 | 0.57 | 0.03 | 0.08 | 0.27 | 0.37 | 0.22 | 0.33 |

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy























Near-Term AM Peak Hour



| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
|-----------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 35 | 66 | 25 | 22 | 33 | 636 | 67 | 392 |
| v/c Ratio | 0.07 | 0.13 | 0.06 | 0.06 | 0.08 | 0.35 | 0.18 | 0.20 |
| Control Delay | 24.8 | 8.9 | 29.4 | 11.1 | 29.6 | 18.8 | 28.9 | 15.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 24.8 | 8.9 | 29.4 | 11.1 | 29.6 | 18.8 | 28.9 | 15.6 |
| Queue Length 50th (ft) | 7 | 2 | 5 | 0 | 7 | 81 | 15 | 24 |
| Queue Length 95th (ft) | 49 | 32 | 39 | 18 | 47 | 245 | 81 | 146 |
| Internal Link Dist (ft) | | 656 | | 824 | | 393 | | 1786 |
| Turn Bay Length (ft) | 150 | | 250 | | 115 | | 190 | |
| Base Capacity (vph) | 636 | 1072 | 540 | 822 | 615 | 2104 | 567 | 2078 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.06 | 0.06 | 0.05 | 0.03 | 0.05 | 0.30 | 0.12 | 0.19 |
| Intersection Summary | | | | | | | | |

Independence at Dixon TIA
2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term PM Peak Hour

| |  |  |  |  |  |  |  |  |  |  |  |  |
|----------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL |
| Lane Configurations |  |  |  | |  |  |  | |  |  |  |  |
| Traffic Volume (vph) | 132 | 11 | 87 | 1 | 245 | 18 | 139 | 25 | 105 | 538 | 184 | 171 |
| Future Volume (vph) | 132 | 11 | 87 | 1 | 245 | 18 | 139 | 25 | 105 | 538 | 184 | 171 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 160 | | 195 | | 195 | | 200 | | 320 | 235 |
| Storage Lanes | 2 | | 1 | | 2 | | 1 | | 1 | | 1 | 2 |
| Taper Length (ft) | 25 | | | | 25 | | | | 25 | | | 25 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.97 |
| Ped Bike Factor | | | 0.99 | | | | | | | | 0.98 | |
| Frt | | | 0.850 | | | | 0.850 | | | | 0.850 | |
| Flt Protected | 0.950 | | | | 0.950 | | | | 0.950 | | | 0.950 |
| Satd. Flow (prot) | 2968 | 1652 | 1553 | 0 | 3273 | 1900 | 1442 | 0 | 1776 | 3139 | 1583 | 3155 |
| Flt Permitted | 0.950 | | | | 0.950 | | | | 0.950 | | | 0.950 |
| Satd. Flow (perm) | 2968 | 1652 | 1532 | 0 | 3273 | 1900 | 1442 | 0 | 1776 | 3139 | 1558 | 3155 |
| Right Turn on Red | | | Yes | | | | Yes | | | | Yes | |
| Satd. Flow (RTOR) | | | 91 | | | | 145 | | | | 192 | |
| Link Speed (mph) | | 35 | | | | 35 | | | | 45 | | |
| Link Distance (ft) | | 600 | | | | 696 | | | | 687 | | |
| Travel Time (s) | | 11.7 | | | | 13.6 | | | | 10.4 | | |
| Confl. Peds. (#/hr) | | | 1 | | | | | | | | | 3 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | 1 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (%) | 18% | 15% | 4% | 0% | 7% | 0% | 12% | 0% | 2% | 15% | 2% | 11% |
| Adj. Flow (vph) | 138 | 11 | 91 | 1 | 255 | 19 | 145 | 26 | 109 | 560 | 192 | 178 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 138 | 11 | 91 | 0 | 256 | 19 | 145 | 0 | 135 | 560 | 192 | 178 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | R NA | Left | Left | Right | R NA | Left | Left | Right | Left |
| Median Width(ft) | | 24 | | | | 24 | | | | 24 | | |
| Link Offset(ft) | | 0 | | | | 0 | | | | 0 | | |
| Crosswalk Width(ft) | | 16 | | | | 16 | | | | 16 | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 9 | 15 | | 9 | 9 | 15 | | 9 | 15 |
| Turn Type | Prot | NA | Perm | Prot | Prot | NA | Perm | Prot | Prot | NA | Perm | Prot |
| Protected Phases | 7 | 4 | | 3 | 3 | 8 | | 5 | 5 | 2 | | 1 |
| Permitted Phases | | | 4 | | | | 8 | | | | 2 | |
| Detector Phase | 7 | 4 | 4 | 3 | 3 | 8 | 8 | 5 | 5 | 2 | 2 | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 13.0 | 12.0 | 12.0 | 13.0 | 13.0 | 12.0 | 12.0 | 12.0 | 12.0 | 10.0 | 10.0 | 13.0 |
| Minimum Split (s) | 16.7 | 41.6 | 41.6 | 16.0 | 16.0 | 41.6 | 41.6 | 15.7 | 15.7 | 36.8 | 36.8 | 16.7 |
| Total Split (s) | 20.7 | 41.6 | 41.6 | 18.7 | 18.7 | 41.6 | 41.6 | 18.7 | 18.7 | 36.8 | 36.8 | 18.7 |
| Total Split (%) | 17.3% | 34.7% | 34.7% | 15.6% | 15.6% | 34.7% | 34.7% | 15.6% | 15.6% | 30.7% | 30.7% | 15.6% |
| Maximum Green (s) | 17.0 | 37.0 | 37.0 | 15.7 | 15.7 | 37.0 | 37.0 | 15.0 | 15.0 | 31.0 | 31.0 | 15.0 |
| Yellow Time (s) | 3.7 | 4.1 | 4.1 | 3.0 | 3.0 | 4.1 | 4.1 | 3.7 | 3.7 | 4.8 | 4.8 | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | 1.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 3.7 | 4.6 | 4.6 | | 3.0 | 4.6 | 4.6 | | 3.7 | 5.8 | 5.8 | 3.7 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term PM Peak Hour



| Lane Group | SBT | SBR |
|----------------------------|-------|-------|
| Lane Configurations | ↑↑ | ↑ |
| Traffic Volume (vph) | 403 | 131 |
| Future Volume (vph) | 403 | 131 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Storage Length (ft) | | 135 |
| Storage Lanes | | 1 |
| Taper Length (ft) | | |
| Lane Util. Factor | 0.95 | 1.00 |
| Ped Bike Factor | | |
| Frt | | 0.850 |
| Flt Protected | | |
| Satd. Flow (prot) | 3139 | 1369 |
| Flt Permitted | | |
| Satd. Flow (perm) | 3139 | 1369 |
| Right Turn on Red | | Yes |
| Satd. Flow (RTOR) | | 136 |
| Link Speed (mph) | 45 | |
| Link Distance (ft) | 967 | |
| Travel Time (s) | 14.7 | |
| Confl. Peds. (#/hr) | | |
| Confl. Bikes (#/hr) | | |
| Peak Hour Factor | 0.96 | 0.96 |
| Heavy Vehicles (%) | 15% | 18% |
| Adj. Flow (vph) | 420 | 136 |
| Shared Lane Traffic (%) | | |
| Lane Group Flow (vph) | 420 | 136 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Right |
| Median Width(ft) | 24 | |
| Link Offset(ft) | 0 | |
| Crosswalk Width(ft) | 16 | |
| Two way Left Turn Lane | | |
| Headway Factor | 1.00 | 1.00 |
| Turning Speed (mph) | | 9 |
| Turn Type | NA | Perm |
| Protected Phases | 6 | |
| Permitted Phases | | 6 |
| Detector Phase | 6 | 6 |
| Switch Phase | | |
| Minimum Initial (s) | 10.0 | 10.0 |
| Minimum Split (s) | 38.8 | 38.8 |
| Total Split (s) | 38.8 | 38.8 |
| Total Split (%) | 32.4% | 32.4% |
| Maximum Green (s) | 33.0 | 33.0 |
| Yellow Time (s) | 4.8 | 4.8 |
| All-Red Time (s) | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |
| Total Lost Time (s) | 5.8 | 5.8 |
| Lead/Lag | Lag | Lag |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term PM Peak Hour

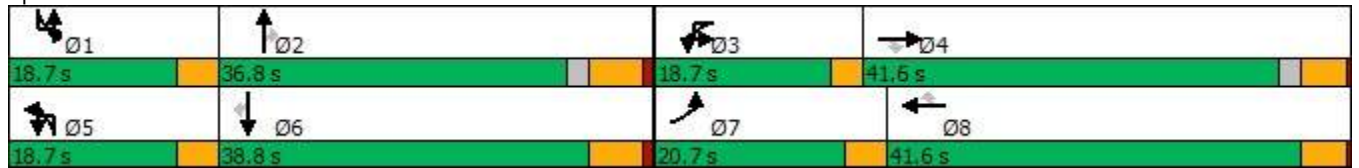


| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 2.0 | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 | 3.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.2 | 1.2 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | None | Min | Min | None |
| Walk Time (s) | | 7.0 | 7.0 | | | 7.0 | 7.0 | | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | | 30.0 | 30.0 | | | 30.0 | 30.0 | | | 24.0 | 24.0 | |
| Pedestrian Calls (#/hr) | | 1 | 1 | | | 0 | 0 | | | 3 | 3 | |
| Act Effect Green (s) | 13.5 | 16.4 | 16.4 | | 17.9 | 16.2 | 16.2 | | 12.9 | 17.1 | 17.1 | 13.5 |
| Actuated g/C Ratio | 0.17 | 0.21 | 0.21 | | 0.23 | 0.21 | 0.21 | | 0.16 | 0.22 | 0.22 | 0.17 |
| v/c Ratio | 0.27 | 0.03 | 0.23 | | 0.34 | 0.05 | 0.35 | | 0.47 | 0.82 | 0.39 | 0.33 |
| Control Delay | 34.1 | 25.7 | 7.8 | | 32.5 | 25.6 | 7.3 | | 39.4 | 40.8 | 7.1 | 34.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.1 | 25.7 | 7.8 | | 32.5 | 25.6 | 7.3 | | 39.4 | 40.8 | 7.1 | 34.3 |
| LOS | C | C | A | | C | C | A | | D | D | A | C |
| Approach Delay | | 23.7 | | | | 23.5 | | | | 33.3 | | |
| Approach LOS | | C | | | | C | | | | C | | |

Intersection Summary

Area Type: Other
 Cycle Length: 119.8
 Actuated Cycle Length: 78.7
 Natural Cycle: 115
 Control Type: Actuated-Uncoordinated
 Maximum v/c Ratio: 0.82
 Intersection Signal Delay: 28.8
 Intersection LOS: C
 Intersection Capacity Utilization 62.9%
 ICU Level of Service B
 Analysis Period (min) 15

Splits and Phases: 2: SR 113 & Dorset Dr/E. Dorset Dr



Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

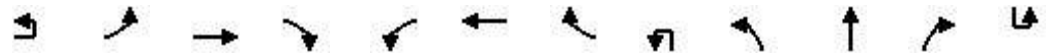
Near-Term PM Peak Hour



| Lane Group | SBT | SBR |
|-------------------------|------|------|
| Lead-Lag Optimize? | Yes | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 |
| Minimum Gap (s) | 3.0 | 3.0 |
| Time Before Reduce (s) | 1.2 | 1.2 |
| Time To Reduce (s) | 0.1 | 0.1 |
| Recall Mode | Min | Min |
| Walk Time (s) | 7.0 | 7.0 |
| Flash Dont Walk (s) | 26.0 | 26.0 |
| Pedestrian Calls (#/hr) | 0 | 0 |
| Act Effct Green (s) | 17.7 | 17.7 |
| Actuated g/C Ratio | 0.22 | 0.22 |
| v/c Ratio | 0.60 | 0.33 |
| Control Delay | 31.9 | 7.9 |
| Queue Delay | 0.0 | 0.0 |
| Total Delay | 31.9 | 7.9 |
| LOS | C | A |
| Approach Delay | 28.0 | |
| Approach LOS | C | |
| Intersection Summary | | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term PM Peak Hour



| Lane Group | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 16 | 196 | 45 | 74 | 119 | 57 | 74 | 65 | 72 | 481 | 62 | 9 |
| Future Volume (vph) | 16 | 196 | 45 | 74 | 119 | 57 | 74 | 65 | 72 | 481 | 62 | 9 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | | 275 | | 0 | 180 | | 230 | | 290 | | 0 | |
| Storage Lanes | | 1 | | 1 | 1 | | 1 | | 1 | | 0 | |
| Taper Length (ft) | | 25 | | | 25 | | | | 25 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 | 0.95 |
| Ped Bike Factor | | | | 0.99 | | | | | | 1.00 | | |
| Frt | | | | 0.850 | | | 0.850 | | | 0.983 | | |
| Flt Protected | | 0.950 | | | 0.950 | | | | 0.950 | | | |
| Satd. Flow (prot) | 0 | 1756 | 1900 | 1495 | 1687 | 1900 | 1196 | 0 | 1724 | 3176 | 0 | 0 |
| Flt Permitted | | 0.950 | | | 0.950 | | | | 0.950 | | | |
| Satd. Flow (perm) | 0 | 1756 | 1900 | 1476 | 1687 | 1900 | 1196 | 0 | 1724 | 3176 | 0 | 0 |
| Right Turn on Red | | | | Yes | | | Yes | | | | Yes | |
| Satd. Flow (RTOR) | | | | 104 | | | 104 | | | 13 | | |
| Link Speed (mph) | | | 35 | | | 45 | | | | 45 | | |
| Link Distance (ft) | | | 437 | | | 359 | | | | 1163 | | |
| Travel Time (s) | | | 8.5 | | | 5.4 | | | | 17.6 | | |
| Confl. Peds. (#/hr) | | | | 1 | | | | | | | 3 | |
| Confl. Bikes (#/hr) | | | | 1 | | | | | | | | |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (%) | 0% | 3% | 0% | 8% | 7% | 0% | 35% | 0% | 9% | 12% | 8% | 0% |
| Adj. Flow (vph) | 17 | 211 | 48 | 80 | 128 | 61 | 80 | 70 | 77 | 517 | 67 | 10 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 228 | 48 | 80 | 128 | 61 | 80 | 0 | 147 | 584 | 0 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | R NA | Left | Left | Right | Left | Left | Right | R NA | Left | Left | Right | R NA |
| Median Width(ft) | | | 12 | | | 12 | | | | 12 | | |
| Link Offset(ft) | | | 0 | | | 0 | | | | 0 | | |
| Crosswalk Width(ft) | | | 16 | | | 16 | | | | 16 | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 9 | 15 | | 9 | 15 | | 9 | 9 | 15 | | 9 | 9 |
| Turn Type | Prot | Prot | NA | Perm | Prot | NA | Perm | Prot | Prot | NA | | Prot |
| Protected Phases | 7 | 7 | 4 | | 3 | 8 | | 5 | 5 | 2 | | 1 |
| Permitted Phases | | | | 4 | | | 8 | | | | | |
| Detector Phase | 7 | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 5 | 2 | | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 10.0 | 10.0 | 10.0 | | 11.0 |
| Minimum Split (s) | 14.7 | 14.7 | 36.2 | 36.2 | 14.7 | 36.2 | 36.2 | 13.7 | 13.7 | 33.8 | | 14.7 |
| Total Split (s) | 18.7 | 18.7 | 36.2 | 36.2 | 18.7 | 36.2 | 36.2 | 18.7 | 18.7 | 33.8 | | 18.7 |
| Total Split (%) | 17.4% | 17.4% | 33.7% | 33.7% | 17.4% | 33.7% | 33.7% | 17.4% | 17.4% | 31.5% | | 17.4% |
| Maximum Green (s) | 15.0 | 15.0 | 32.0 | 32.0 | 15.0 | 32.0 | 32.0 | 15.0 | 15.0 | 28.0 | | 15.0 |
| Yellow Time (s) | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 4.8 | | 3.7 |
| All-Red Time (s) | 0.0 | 0.0 | 0.5 | 0.5 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | | 0.0 |
| Lost Time Adjust (s) | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Lost Time (s) | | 3.7 | 4.2 | 4.2 | 3.7 | 4.2 | 4.2 | | 3.7 | 5.8 | | |
| Lead/Lag | Lead | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lead | Lag | | Lead |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term PM Peak Hour



| Lane Group | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|
| Lane Configurations | | | |
| Traffic Volume (vph) | 65 | 521 | 169 |
| Future Volume (vph) | 65 | 521 | 169 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 |
| Storage Length (ft) | 285 | | 0 |
| Storage Lanes | 1 | | 0 |
| Taper Length (ft) | 25 | | |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | | | |
| Frt | | 0.963 | |
| Flt Protected | 0.950 | | |
| Satd. Flow (prot) | 1548 | 3188 | 0 |
| Flt Permitted | 0.950 | | |
| Satd. Flow (perm) | 1548 | 3188 | 0 |
| Right Turn on Red | | | Yes |
| Satd. Flow (RTOR) | | 39 | |
| Link Speed (mph) | | 45 | |
| Link Distance (ft) | | 687 | |
| Travel Time (s) | | 10.4 | |
| Confl. Peds. (#/hr) | | | |
| Confl. Bikes (#/hr) | | | |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (%) | 19% | 12% | 0% |
| Adj. Flow (vph) | 70 | 560 | 182 |
| Shared Lane Traffic (%) | | | |
| Lane Group Flow (vph) | 80 | 742 | 0 |
| Enter Blocked Intersection | No | No | No |
| Lane Alignment | Left | Left | Right |
| Median Width(ft) | | 12 | |
| Link Offset(ft) | | 0 | |
| Crosswalk Width(ft) | | 16 | |
| Two way Left Turn Lane | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 |
| Turn Type | Prot | NA | |
| Protected Phases | 1 | 6 | |
| Permitted Phases | | | |
| Detector Phase | 1 | 6 | |
| Switch Phase | | | |
| Minimum Initial (s) | 11.0 | 10.0 | |
| Minimum Split (s) | 14.7 | 33.8 | |
| Total Split (s) | 18.7 | 33.8 | |
| Total Split (%) | 17.4% | 31.5% | |
| Maximum Green (s) | 15.0 | 28.0 | |
| Yellow Time (s) | 3.7 | 4.8 | |
| All-Red Time (s) | 0.0 | 1.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | |
| Total Lost Time (s) | 3.7 | 5.8 | |
| Lead/Lag | Lead | Lag | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term PM Peak Hour



| Lane Group | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
|-------------------------|------|------|------|------|------|------|------|------|------|------|-----|------|
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 | | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | None | Min | | None |
| Walk Time (s) | | | 7.0 | 7.0 | | 7.0 | 7.0 | | | 7.0 | | |
| Flash Dont Walk (s) | | | 25.0 | 25.0 | | 25.0 | 25.0 | | | 21.0 | | |
| Pedestrian Calls (#/hr) | | | 1 | 1 | | 0 | 0 | | | 3 | | |
| Act Effect Green (s) | | 14.8 | 17.0 | 17.0 | 12.4 | 14.8 | 14.8 | | 11.8 | 24.3 | | |
| Actuated g/C Ratio | | 0.20 | 0.23 | 0.23 | 0.17 | 0.20 | 0.20 | | 0.16 | 0.32 | | |
| v/c Ratio | | 0.66 | 0.11 | 0.19 | 0.46 | 0.16 | 0.25 | | 0.54 | 0.56 | | |
| Control Delay | | 43.5 | 26.8 | 4.6 | 40.6 | 29.3 | 5.5 | | 43.1 | 27.0 | | |
| Queue Delay | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Delay | | 43.5 | 26.8 | 4.6 | 40.6 | 29.3 | 5.5 | | 43.1 | 27.0 | | |
| LOS | | D | C | A | D | C | A | | D | C | | |
| Approach Delay | | | 32.5 | | | 27.6 | | | | 30.3 | | |
| Approach LOS | | | C | | | C | | | | C | | |

Intersection Summary

Area Type: Other
 Cycle Length: 107.4
 Actuated Cycle Length: 74.9
 Natural Cycle: 100
 Control Type: Actuated-Uncoordinated
 Maximum v/c Ratio: 0.85
 Intersection Signal Delay: 33.0
 Intersection LOS: C
 Intersection Capacity Utilization 62.0%
 ICU Level of Service B
 Analysis Period (min) 15

Splits and Phases: 3: SR 113 & N. Lincoln St/Vaughn Rd

| | | | |
|--------|--------|--------|--------|
| | | | |
| 18.7 s | 33.8 s | 18.7 s | 36.2 s |
| | | | |
| 18.7 s | 33.8 s | 18.7 s | 36.2 s |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term PM Peak Hour



| Lane Group | SBL | SBT | SBR |
|-----------------------------|------|------|-----|
| Lead-Lag Optimize? | Yes | Yes | |
| Vehicle Extension (s) | 0.2 | 0.2 | |
| Minimum Gap (s) | 1.0 | 3.0 | |
| Time Before Reduce (s) | 1.0 | 1.0 | |
| Time To Reduce (s) | 0.1 | 0.1 | |
| Recall Mode | None | Min | |
| Walk Time (s) | | 7.0 | |
| Flash Dont Walk (s) | | 21.0 | |
| Pedestrian Calls (#/hr) | | 0 | |
| Act Effct Green (s) | 12.1 | 19.8 | |
| Actuated g/C Ratio | 0.16 | 0.26 | |
| v/c Ratio | 0.32 | 0.85 | |
| Control Delay | 38.8 | 37.1 | |
| Queue Delay | 0.0 | 0.0 | |
| Total Delay | 38.8 | 37.1 | |
| LOS | D | D | |
| Approach Delay | | 37.3 | |
| Approach LOS | | D | |
| Intersection Summary | | | |

Independence at Dixon TIA
4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term PM Peak Hour



| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 25 | 3 | 35 | 1 | 53 | 6 | 57 | 35 | 560 | 17 | 18 | 18 |
| Future Volume (vph) | 25 | 3 | 35 | 1 | 53 | 6 | 57 | 35 | 560 | 17 | 18 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 0 | | 250 | | 0 | 115 | | 0 | | 190 |
| Storage Lanes | 1 | | 0 | | 1 | | 0 | 1 | | 0 | | 1 |
| Taper Length (ft) | 25 | | | | 25 | | | 25 | | | | 25 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 |
| Ped Bike Factor | | 0.99 | | | | 0.99 | | | | | | |
| Frt | | 0.862 | | | | 0.864 | | | 0.996 | | | |
| Flt Protected | 0.950 | | | | 0.950 | | | 0.950 | | | | 0.950 |
| Satd. Flow (prot) | 1597 | 1528 | 0 | 0 | 1472 | 1190 | 0 | 1687 | 3349 | 0 | 0 | 1626 |
| Flt Permitted | 0.950 | | | | 0.950 | | | 0.950 | | | | 0.950 |
| Satd. Flow (perm) | 1597 | 1528 | 0 | 0 | 1472 | 1190 | 0 | 1687 | 3349 | 0 | 0 | 1626 |
| Right Turn on Red | | | Yes | | | | Yes | | | Yes | | |
| Satd. Flow (RTOR) | | 36 | | | | 59 | | | 3 | | | |
| Link Speed (mph) | | 30 | | | | 30 | | | 30 | | | |
| Link Distance (ft) | | 736 | | | | 904 | | | 473 | | | |
| Travel Time (s) | | 16.7 | | | | 20.5 | | | 10.8 | | | |
| Confl. Peds. (#/hr) | | | 1 | | | | 1 | | | | | |
| Confl. Bikes (#/hr) | | 1 | | | | | | | | | | |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (%) | 13% | 29% | 4% | 0% | 23% | 0% | 40% | 7% | 7% | 19% | 0% | 22% |
| Adj. Flow (vph) | 26 | 3 | 36 | 1 | 55 | 6 | 59 | 36 | 583 | 18 | 19 | 19 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 26 | 39 | 0 | 0 | 56 | 65 | 0 | 36 | 601 | 0 | 0 | 38 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | R NA | Left | Left | Right | Left | Left | Right | R NA | Left |
| Median Width(ft) | | 12 | | | | 12 | | | 12 | | | |
| Link Offset(ft) | | 0 | | | | 0 | | | 0 | | | |
| Crosswalk Width(ft) | | 16 | | | | 16 | | | 16 | | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 9 | 15 | | 9 | 15 | | 9 | 9 | 15 |
| Turn Type | Prot | NA | | Prot | Prot | NA | | Prot | NA | | Prot | Prot |
| Protected Phases | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 1 |
| Permitted Phases | | | | | | | | | | | | |
| Detector Phase | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | | 11.0 | 11.0 | 11.0 | | 10.0 | 10.0 | | 10.0 | 10.0 |
| Minimum Split (s) | 14.7 | 35.2 | | 14.7 | 14.7 | 35.2 | | 13.7 | 27.8 | | 13.7 | 13.7 |
| Total Split (s) | 18.7 | 35.2 | | 18.7 | 18.7 | 35.2 | | 18.7 | 30.8 | | 18.7 | 18.7 |
| Total Split (%) | 18.1% | 34.0% | | 18.1% | 18.1% | 34.0% | | 18.1% | 29.8% | | 18.1% | 18.1% |
| Maximum Green (s) | 15.0 | 31.0 | | 15.0 | 15.0 | 31.0 | | 15.0 | 25.0 | | 15.0 | 15.0 |
| Yellow Time (s) | 3.7 | 3.7 | | 3.7 | 3.7 | 3.7 | | 3.7 | 4.8 | | 3.7 | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | | 0.0 | 0.0 | 0.5 | | 0.0 | 1.0 | | 0.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | | | 0.0 |
| Total Lost Time (s) | 3.7 | 4.2 | | | 3.7 | 4.2 | | 3.7 | 5.8 | | | 3.7 |
| Lead/Lag | Lead | Lag | | Lead | Lead | Lag | | Lead | Lag | | Lead | Lead |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term PM Peak Hour



| Lane Group | SBT | SBR |
|----------------------------|-------|-------|
| Lane Configurations | ↑↑ | |
| Traffic Volume (vph) | 600 | 40 |
| Future Volume (vph) | 600 | 40 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Storage Length (ft) | | 0 |
| Storage Lanes | | 0 |
| Taper Length (ft) | | |
| Lane Util. Factor | 0.95 | 0.95 |
| Ped Bike Factor | 1.00 | |
| Frt | 0.991 | |
| Flt Protected | | |
| Satd. Flow (prot) | 3248 | 0 |
| Flt Permitted | | |
| Satd. Flow (perm) | 3248 | 0 |
| Right Turn on Red | | Yes |
| Satd. Flow (RTOR) | 6 | |
| Link Speed (mph) | 45 | |
| Link Distance (ft) | 1866 | |
| Travel Time (s) | 28.3 | |
| Confl. Peds. (#/hr) | | 4 |
| Confl. Bikes (#/hr) | | |
| Peak Hour Factor | 0.96 | 0.96 |
| Heavy Vehicles (%) | 10% | 9% |
| Adj. Flow (vph) | 625 | 42 |
| Shared Lane Traffic (%) | | |
| Lane Group Flow (vph) | 667 | 0 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Right |
| Median Width(ft) | 12 | |
| Link Offset(ft) | 0 | |
| Crosswalk Width(ft) | 16 | |
| Two way Left Turn Lane | Yes | |
| Headway Factor | 1.00 | 1.00 |
| Turning Speed (mph) | | 9 |
| Turn Type | NA | |
| Protected Phases | 6 | |
| Permitted Phases | | |
| Detector Phase | 6 | |
| Switch Phase | | |
| Minimum Initial (s) | 10.0 | |
| Minimum Split (s) | 27.8 | |
| Total Split (s) | 30.8 | |
| Total Split (%) | 29.8% | |
| Maximum Green (s) | 25.0 | |
| Yellow Time (s) | 4.8 | |
| All-Red Time (s) | 1.0 | |
| Lost Time Adjust (s) | 0.0 | |
| Total Lost Time (s) | 5.8 | |
| Lead/Lag | Lag | |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term PM Peak Hour

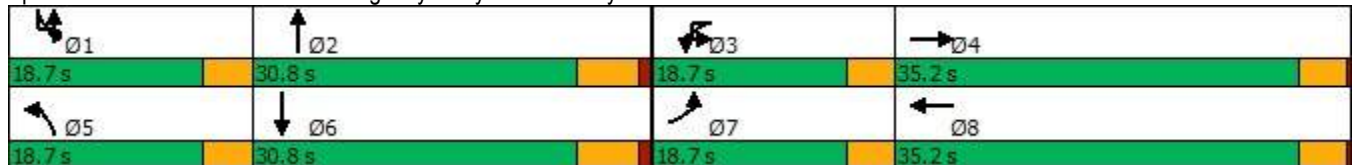


| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL |
|-------------------------|------|------|-----|------|------|------|------|------|------|-----|------|------|
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | | Yes | Yes | | Yes | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | | 0.2 | 0.2 | 0.2 | | 0.2 | 0.2 | | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | | 0.1 | 0.1 | 0.1 | | 0.1 | 0.1 | | 0.1 | 0.1 |
| Recall Mode | None | None | | None | None | None | | None | Min | | None | None |
| Walk Time (s) | | 7.0 | | | | 7.0 | | | 7.0 | | | |
| Flash Dont Walk (s) | | 24.0 | | | | 24.0 | | | 15.0 | | | |
| Pedestrian Calls (#/hr) | | 1 | | | | 1 | | | 0 | | | |
| Act Effct Green (s) | 14.3 | 16.6 | | 14.3 | 19.6 | | 13.0 | 30.7 | | | | 13.0 |
| Actuated g/C Ratio | 0.27 | 0.31 | | 0.27 | 0.37 | | 0.24 | 0.57 | | | | 0.24 |
| v/c Ratio | 0.06 | 0.08 | | 0.14 | 0.14 | | 0.09 | 0.31 | | | | 0.10 |
| Control Delay | 29.8 | 9.7 | | 29.0 | 8.7 | | 30.2 | 18.1 | | | | 30.2 |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | | | 0.0 |
| Total Delay | 29.8 | 9.7 | | 29.0 | 8.7 | | 30.2 | 18.1 | | | | 30.2 |
| LOS | C | A | | C | A | | C | B | | | | C |
| Approach Delay | | 17.7 | | | 18.1 | | | 18.8 | | | | |
| Approach LOS | | B | | | B | | | B | | | | |

Intersection Summary

Area Type: Other
 Cycle Length: 103.4
 Actuated Cycle Length: 53.6
 Natural Cycle: 95
 Control Type: Actuated-Uncoordinated
 Maximum v/c Ratio: 0.36
 Intersection Signal Delay: 18.9 Intersection LOS: B
 Intersection Capacity Utilization 48.1% ICU Level of Service A
 Analysis Period (min) 15

Splits and Phases: 4: SR 113 & Regency Pkwy/Industrial Wy



Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term PM Peak Hour



| Lane Group | SBT | SBR |
|-------------------------|------|-----|
| Lead-Lag Optimize? | Yes | |
| Vehicle Extension (s) | 0.2 | |
| Minimum Gap (s) | 1.0 | |
| Time Before Reduce (s) | 1.0 | |
| Time To Reduce (s) | 0.1 | |
| Recall Mode | Min | |
| Walk Time (s) | 7.0 | |
| Flash Dont Walk (s) | 15.0 | |
| Pedestrian Calls (#/hr) | 4 | |
| Act Effct Green (s) | 30.7 | |
| Actuated g/C Ratio | 0.57 | |
| v/c Ratio | 0.36 | |
| Control Delay | 18.7 | |
| Queue Delay | 0.0 | |
| Total Delay | 18.7 | |
| LOS | B | |
| Approach Delay | 19.3 | |
| Approach LOS | B | |
| Intersection Summary | | |

Independence at Dixon TIA

1: SR 113/I-80 EB Ramps & I-80 WB Ramps/Auction Ln

Near-Term PM Peak Hour

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 3.1 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↔ | ↔ | | ↔ | | ↔ | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 6 | 0 | 534 | 2 | 0 | 1 | 304 | 504 | 2 | 1 | 232 | 16 |
| Future Vol, veh/h | 6 | 0 | 534 | 2 | 0 | 1 | 304 | 504 | 2 | 1 | 232 | 16 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | Free | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 0 | - | - | - | 0 | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, % | 29 | 0 | 11 | 100 | 100 | 0 | 21 | 15 | 100 | 0 | 20 | 13 |
| Mvmt Flow | 6 | 0 | 574 | 2 | 0 | 1 | 327 | 542 | 2 | 1 | 249 | 17 |

| Major/Minor | Minor2 | | Minor1 | | Major1 | | Major2 | | | | | |
|----------------------|--------|------|--------|------|--------|-----|--------|---|---|------|---|---|
| Conflicting Flow All | 1458 | 1458 | - | 1457 | 1465 | 543 | 266 | 0 | 0 | 544 | 0 | 0 |
| Stage 1 | 260 | 260 | - | 1197 | 1197 | - | - | - | - | - | - | - |
| Stage 2 | 1198 | 1198 | - | 260 | 268 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.39 | 6.5 | - | 8.1 | 7.5 | 6.2 | 4.31 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.761 | 4 | - | 4.4 | 4.9 | 3.3 | 2.389 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 93 | 131 | 0 | 66 | 80 | 544 | 1195 | - | - | 1035 | - | - |
| Stage 1 | 689 | 697 | 0 | 147 | 171 | - | - | - | - | - | - | - |
| Stage 2 | 200 | 261 | 0 | 572 | 540 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | - | - | - |
| Mov Cap-1 Maneuver | 73 | 95 | - | 52 | 58 | 544 | 1195 | - | - | 1035 | - | - |
| Mov Cap-2 Maneuver | 73 | 95 | - | 52 | 58 | - | - | - | - | - | - | - |
| Stage 1 | 500 | 696 | - | 107 | 124 | - | - | - | - | - | - | - |
| Stage 2 | 145 | 189 | - | 571 | 539 | - | - | - | - | - | - | - |

| Approach | EB | | WB | | NB | | SB | |
|----------------------|----|--|------|--|-----|--|----|--|
| HCM Control Delay, s | 59 | | 55.9 | | 3.4 | | 0 | |
| HCM LOS | F | | F | | | | | |

| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | EBLn2 | WBLn1 | SBL | SBT | SBR |
|-----------------------|-------|-----|-----|-------|-------|-------|-------|-----|-----|
| Capacity (veh/h) | 1195 | - | - | 73 | - | 74 | 1035 | - | - |
| HCM Lane V/C Ratio | 0.274 | - | - | 0.088 | - | 0.044 | 0.001 | - | - |
| HCM Control Delay (s) | 9.1 | - | - | 59 | 0 | 55.9 | 8.5 | 0 | - |
| HCM Lane LOS | A | - | - | F | A | F | A | A | - |
| HCM 95th %tile Q(veh) | 1.1 | - | - | 0.3 | - | 0.1 | 0 | - | - |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term PM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 138 | 11 | 91 | 256 | 19 | 145 | 135 | 560 | 192 | 178 | 420 | 136 |
| v/c Ratio | 0.27 | 0.03 | 0.23 | 0.34 | 0.05 | 0.35 | 0.47 | 0.82 | 0.39 | 0.33 | 0.60 | 0.33 |
| Control Delay | 34.1 | 25.7 | 7.8 | 32.5 | 25.6 | 7.3 | 39.4 | 40.8 | 7.1 | 34.3 | 31.9 | 7.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.1 | 25.7 | 7.8 | 32.5 | 25.6 | 7.3 | 39.4 | 40.8 | 7.1 | 34.3 | 31.9 | 7.9 |
| Queue Length 50th (ft) | 26 | 4 | 0 | 52 | 7 | 0 | 54 | 124 | 0 | 35 | 86 | 0 |
| Queue Length 95th (ft) | 80 | 19 | 36 | 135 | 26 | 44 | 161 | 252 | 54 | 100 | 191 | 49 |
| Internal Link Dist (ft) | | 520 | | | 616 | | | 607 | | | 887 | |
| Turn Bay Length (ft) | 150 | | 160 | 195 | | 195 | 200 | | 320 | 235 | | 135 |
| Base Capacity (vph) | 665 | 850 | 832 | 820 | 933 | 782 | 351 | 1366 | 786 | 624 | 1366 | 673 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.21 | 0.01 | 0.11 | 0.31 | 0.02 | 0.19 | 0.38 | 0.41 | 0.24 | 0.29 | 0.31 | 0.20 |

Intersection Summary

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term PM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|-------------------------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 228 | 48 | 80 | 128 | 61 | 80 | 147 | 584 | 80 | 742 |
| v/c Ratio | 0.66 | 0.11 | 0.19 | 0.46 | 0.16 | 0.25 | 0.54 | 0.56 | 0.32 | 0.85 |
| Control Delay | 43.5 | 26.8 | 4.6 | 40.6 | 29.3 | 5.5 | 43.1 | 27.0 | 38.8 | 37.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 43.5 | 26.8 | 4.6 | 40.6 | 29.3 | 5.5 | 43.1 | 27.0 | 38.8 | 37.1 |
| Queue Length 50th (ft) | 96 | 18 | 0 | 54 | 25 | 0 | 64 | 123 | 33 | 157 |
| Queue Length 95th (ft) | #305 | 53 | 22 | 145 | 63 | 23 | 164 | 243 | 101 | #345 |
| Internal Link Dist (ft) | | 357 | | | 279 | | | 1083 | | 607 |
| Turn Bay Length (ft) | 275 | | | 180 | | 230 | 290 | | 285 | |
| Base Capacity (vph) | 379 | 876 | 736 | 364 | 876 | 607 | 372 | 1301 | 334 | 1309 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.60 | 0.05 | 0.11 | 0.35 | 0.07 | 0.13 | 0.40 | 0.45 | 0.24 | 0.57 |

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term PM Peak Hour



| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
|-----------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 26 | 39 | 56 | 65 | 36 | 601 | 38 | 667 |
| v/c Ratio | 0.06 | 0.08 | 0.14 | 0.14 | 0.09 | 0.31 | 0.10 | 0.36 |
| Control Delay | 29.8 | 9.7 | 29.0 | 8.7 | 30.2 | 18.1 | 30.2 | 18.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 29.8 | 9.7 | 29.0 | 8.7 | 30.2 | 18.1 | 30.2 | 18.7 |
| Queue Length 50th (ft) | 7 | 1 | 14 | 1 | 9 | 78 | 10 | 90 |
| Queue Length 95th (ft) | 39 | 23 | 70 | 31 | 50 | 228 | 53 | 258 |
| Internal Link Dist (ft) | | 656 | | 824 | | 393 | | 1786 |
| Turn Bay Length (ft) | 150 | | 250 | | 115 | | 190 | |
| Base Capacity (vph) | 581 | 1043 | 536 | 822 | 614 | 2083 | 592 | 2021 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.04 | 0.04 | 0.10 | 0.08 | 0.06 | 0.29 | 0.06 | 0.33 |
| Intersection Summary | | | | | | | | |

Independence at Dixon TIA

2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term Plus Project AM Peak Hour

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 67 | 14 | 28 | 83 | 6 | 35 | 35 | 88 | 481 | 126 | 1 | 101 |
| Future Volume (vph) | 67 | 14 | 28 | 83 | 6 | 35 | 35 | 88 | 481 | 126 | 1 | 101 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 160 | 195 | | 195 | | 200 | | 320 | | 235 |
| Storage Lanes | 2 | | 1 | 2 | | 1 | | 1 | | 1 | | 2 |
| Taper Length (ft) | 25 | | | 25 | | | | 25 | | | | 25 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.95 | 0.97 |
| Ped Bike Factor | | | 0.99 | | | 0.99 | | | | | | |
| Frt | | | 0.850 | | | 0.850 | | | | 0.850 | | |
| Flt Protected | 0.950 | | | 0.950 | | | | 0.950 | | | | 0.950 |
| Satd. Flow (prot) | 2968 | 1652 | 1553 | 3273 | 1900 | 1442 | 0 | 1780 | 3139 | 1583 | 0 | 3157 |
| Flt Permitted | 0.950 | | | 0.950 | | | | 0.950 | | | | 0.950 |
| Satd. Flow (perm) | 2968 | 1652 | 1531 | 3273 | 1900 | 1423 | 0 | 1780 | 3139 | 1583 | 0 | 3157 |
| Right Turn on Red | | | Yes | | | Yes | | | | Yes | | |
| Satd. Flow (RTOR) | | | 87 | | | 87 | | | | 145 | | |
| Link Speed (mph) | | 35 | | | 35 | | | | 45 | | | |
| Link Distance (ft) | | 600 | | | 696 | | | | 687 | | | |
| Travel Time (s) | | 11.7 | | | 13.6 | | | | 10.4 | | | |
| Confl. Peds. (#/hr) | | | 2 | | | 1 | | | | | | |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Heavy Vehicles (%) | 18% | 15% | 4% | 7% | 0% | 12% | 0% | 2% | 15% | 2% | 0% | 11% |
| Adj. Flow (vph) | 77 | 16 | 32 | 95 | 7 | 40 | 40 | 101 | 553 | 145 | 1 | 116 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 77 | 16 | 32 | 95 | 7 | 40 | 0 | 141 | 553 | 145 | 0 | 117 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | R NA | Left | Left | Right | R NA | Left |
| Median Width(ft) | | 24 | | | 24 | | | | 24 | | | |
| Link Offset(ft) | | 0 | | | 0 | | | | 0 | | | |
| Crosswalk Width(ft) | | 16 | | | 16 | | | | 16 | | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 15 | | 9 | 9 | 15 | | 9 | 9 | 15 |
| Turn Type | Prot | NA | Perm | Prot | NA | Perm | Prot | Prot | NA | Perm | Prot | Prot |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 5 | 2 | | 1 | 1 |
| Permitted Phases | | | 4 | | | 8 | | | | 2 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 5 | 2 | 2 | 1 | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 13.0 | 12.0 | 12.0 | 13.0 | 12.0 | 12.0 | 12.0 | 12.0 | 10.0 | 10.0 | 13.0 | 13.0 |
| Minimum Split (s) | 16.7 | 41.6 | 41.6 | 16.0 | 41.6 | 41.6 | 15.7 | 15.7 | 36.8 | 36.8 | 16.7 | 16.7 |
| Total Split (s) | 20.7 | 41.6 | 41.6 | 18.7 | 41.6 | 41.6 | 18.7 | 18.7 | 36.8 | 36.8 | 18.7 | 18.7 |
| Total Split (%) | 17.3% | 34.7% | 34.7% | 15.6% | 34.7% | 34.7% | 15.6% | 15.6% | 30.7% | 30.7% | 15.6% | 15.6% |
| Maximum Green (s) | 17.0 | 37.0 | 37.0 | 15.7 | 37.0 | 37.0 | 15.0 | 15.0 | 31.0 | 31.0 | 15.0 | 15.0 |
| Yellow Time (s) | 3.7 | 4.1 | 4.1 | 3.0 | 4.1 | 4.1 | 3.7 | 3.7 | 4.8 | 4.8 | 3.7 | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | 0.5 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | 1.0 | 0.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 |
| Total Lost Time (s) | 3.7 | 4.6 | 4.6 | 3.0 | 4.6 | 4.6 | | 3.7 | 5.8 | 5.8 | | 3.7 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term Plus Project AM Peak Hour



| Lane Group | SBT | SBR |
|----------------------------|-------|-------|
| Lane Configurations | ↑↑ | ↑ |
| Traffic Volume (vph) | 416 | 72 |
| Future Volume (vph) | 416 | 72 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Storage Length (ft) | | 135 |
| Storage Lanes | | 1 |
| Taper Length (ft) | | |
| Lane Util. Factor | 0.95 | 1.00 |
| Ped Bike Factor | | |
| Frt | | 0.850 |
| Flt Protected | | |
| Satd. Flow (prot) | 3139 | 1369 |
| Flt Permitted | | |
| Satd. Flow (perm) | 3139 | 1369 |
| Right Turn on Red | | Yes |
| Satd. Flow (RTOR) | | 83 |
| Link Speed (mph) | 45 | |
| Link Distance (ft) | 967 | |
| Travel Time (s) | 14.7 | |
| Confl. Peds. (#/hr) | | |
| Peak Hour Factor | 0.87 | 0.87 |
| Heavy Vehicles (%) | 15% | 18% |
| Adj. Flow (vph) | 478 | 83 |
| Shared Lane Traffic (%) | | |
| Lane Group Flow (vph) | 478 | 83 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Right |
| Median Width(ft) | 24 | |
| Link Offset(ft) | 0 | |
| Crosswalk Width(ft) | 16 | |
| Two way Left Turn Lane | | |
| Headway Factor | 1.00 | 1.00 |
| Turning Speed (mph) | | 9 |
| Turn Type | NA | Perm |
| Protected Phases | 6 | |
| Permitted Phases | | 6 |
| Detector Phase | 6 | 6 |
| Switch Phase | | |
| Minimum Initial (s) | 10.0 | 10.0 |
| Minimum Split (s) | 38.8 | 38.8 |
| Total Split (s) | 38.8 | 38.8 |
| Total Split (%) | 32.4% | 32.4% |
| Maximum Green (s) | 33.0 | 33.0 |
| Yellow Time (s) | 4.8 | 4.8 |
| All-Red Time (s) | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |
| Total Lost Time (s) | 5.8 | 5.8 |
| Lead/Lag | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term Plus Project AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU | SBL |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 | 3.0 | 1.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.2 | 1.2 | 1.0 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | Min | Min | None | None |
| Walk Time (s) | | 7.0 | 7.0 | | 7.0 | 7.0 | | | 7.0 | 7.0 | | |
| Flash Dont Walk (s) | | 30.0 | 30.0 | | 30.0 | 30.0 | | | 24.0 | 24.0 | | |
| Pedestrian Calls (#/hr) | | 2 | 2 | | 1 | 1 | | | 0 | 0 | | |
| Act Effct Green (s) | 15.4 | 17.7 | 17.7 | 15.6 | 17.3 | 17.3 | | 14.6 | 25.4 | 25.4 | | 15.4 |
| Actuated g/C Ratio | 0.23 | 0.27 | 0.27 | 0.23 | 0.26 | 0.26 | | 0.22 | 0.38 | 0.38 | | 0.23 |
| v/c Ratio | 0.11 | 0.04 | 0.07 | 0.12 | 0.01 | 0.09 | | 0.36 | 0.46 | 0.21 | | 0.16 |
| Control Delay | 31.5 | 24.4 | 0.3 | 31.2 | 24.5 | 0.4 | | 35.0 | 27.3 | 6.5 | | 31.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 |
| Total Delay | 31.5 | 24.4 | 0.3 | 31.2 | 24.5 | 0.4 | | 35.0 | 27.3 | 6.5 | | 31.3 |
| LOS | C | C | A | C | C | A | | C | C | A | | C |
| Approach Delay | | 22.6 | | | 22.2 | | | | 25.0 | | | |
| Approach LOS | | C | | | C | | | | C | | | |

Intersection Summary

| | |
|-----------------------------------|------------------------|
| Area Type: | Other |
| Cycle Length: | 119.8 |
| Actuated Cycle Length: | 66.6 |
| Natural Cycle: | 115 |
| Control Type: | Actuated-Uncoordinated |
| Maximum v/c Ratio: | 0.61 |
| Intersection Signal Delay: | 25.5 |
| Intersection LOS: | C |
| Intersection Capacity Utilization | 61.0% |
| ICU Level of Service | B |
| Analysis Period (min) | 15 |

Splits and Phases: 2: SR 113 & Dorset Dr/E. Dorset Dr



Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term Plus Project AM Peak Hour



| Lane Group | SBT | SBR |
|-------------------------|------|------|
| Vehicle Extension (s) | 0.2 | 0.2 |
| Minimum Gap (s) | 3.0 | 3.0 |
| Time Before Reduce (s) | 1.2 | 1.2 |
| Time To Reduce (s) | 0.1 | 0.1 |
| Recall Mode | Min | Min |
| Walk Time (s) | 7.0 | 7.0 |
| Flash Dont Walk (s) | 26.0 | 26.0 |
| Pedestrian Calls (#/hr) | 0 | 0 |
| Act Effct Green (s) | 16.7 | 16.7 |
| Actuated g/C Ratio | 0.25 | 0.25 |
| v/c Ratio | 0.61 | 0.20 |
| Control Delay | 29.6 | 8.7 |
| Queue Delay | 0.0 | 0.0 |
| Total Delay | 29.6 | 8.7 |
| LOS | C | A |
| Approach Delay | 27.4 | |
| Approach LOS | C | |
| Intersection Summary | | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project AM Peak Hour

| Lane Group | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
|----------------------------|-------|-------|-------|-------|--------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 29 | 218 | 59 | 47 | 1 | 58 | 31 | 52 | 76 | 37 | 451 | 92 |
| Future Volume (vph) | 29 | 218 | 59 | 47 | 1 | 58 | 31 | 52 | 76 | 37 | 451 | 92 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | | 275 | | 0 | | 180 | | 230 | | 290 | | 0 |
| Storage Lanes | | 1 | | 1 | | 1 | | 1 | | 1 | | 0 |
| Taper Length (ft) | | 25 | | | | 25 | | | | 25 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | | | | 0.99 | | | | | | | 1.00 | |
| Frt | | | | 0.850 | | | | 0.850 | | | 0.975 | |
| Flt Protected | | 0.950 | | | | 0.950 | | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1759 | 1900 | 1495 | 0 | 1689 | 1900 | 1196 | 0 | 1753 | 3154 | 0 |
| Flt Permitted | | 0.950 | | | | 0.234 | | | | 0.950 | | |
| Satd. Flow (perm) | 0 | 1759 | 1900 | 1476 | 0 | 416 | 1900 | 1196 | 0 | 1753 | 3154 | 0 |
| Right Turn on Red | | | | Yes | | | | Yes | | | | Yes |
| Satd. Flow (RTOR) | | | | 104 | | | | 104 | | | | 22 |
| Link Speed (mph) | | | 35 | | | | 45 | | | | 45 | |
| Link Distance (ft) | | | 437 | | | | 359 | | | | 1163 | |
| Travel Time (s) | | | 8.5 | | | | 5.4 | | | | 17.6 | |
| Confl. Peds. (#/hr) | | | | 1 | | | | | | | | 3 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.92 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (%) | 0% | 3% | 0% | 8% | 0% | 7% | 0% | 35% | 0% | 9% | 12% | 8% |
| Adj. Flow (vph) | 31 | 229 | 62 | 49 | 1 | 61 | 33 | 55 | 80 | 39 | 475 | 97 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 260 | 62 | 49 | 0 | 62 | 33 | 55 | 0 | 119 | 572 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | R NA | Left | Left | Right | R NA | Left | Left | Right | R NA | Left | Left | Right |
| Median Width(ft) | | | 12 | | | | 12 | | | | 12 | |
| Link Offset(ft) | | | 0 | | | | 0 | | | | 0 | |
| Crosswalk Width(ft) | | | 16 | | | | 16 | | | | 16 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 9 | 15 | | 9 | 9 | 15 | | 9 | 9 | 15 | | 9 |
| Turn Type | Prot | Prot | NA | Perm | custom | Prot | NA | Perm | Prot | Prot | NA | |
| Protected Phases | 7 | 7 | 4 | | | 3 | 8 | | 5 | 5 | 2 | |
| Permitted Phases | | | | 4 | 3 | | | 8 | | | | |
| Detector Phase | 7 | 7 | 4 | 4 | 3 | 3 | 8 | 8 | 5 | 5 | 2 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 10.0 | 10.0 | 10.0 | |
| Minimum Split (s) | 14.7 | 14.7 | 36.2 | 36.2 | 14.7 | 14.7 | 36.2 | 36.2 | 13.7 | 13.7 | 33.8 | |
| Total Split (s) | 18.7 | 18.7 | 36.2 | 36.2 | 18.7 | 18.7 | 36.2 | 36.2 | 18.7 | 18.7 | 33.8 | |
| Total Split (%) | 17.4% | 17.4% | 33.7% | 33.7% | 17.4% | 17.4% | 33.7% | 33.7% | 17.4% | 17.4% | 31.5% | |
| Maximum Green (s) | 15.0 | 15.0 | 32.0 | 32.0 | 15.0 | 15.0 | 32.0 | 32.0 | 15.0 | 15.0 | 28.0 | |
| Yellow Time (s) | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 4.8 | |
| All-Red Time (s) | 0.0 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 3.7 | 4.2 | 4.2 | | | 3.7 | 4.2 | | 3.7 | 5.8 | |
| Lead/Lag | Lead | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead | Lead | Lag | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project AM Peak Hour



| Lane Group | SBU | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|-------|
| Lane Configurations | | | | |
| Traffic Volume (vph) | 3 | 75 | 414 | 70 |
| Future Volume (vph) | 3 | 75 | 414 | 70 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | | 285 | | 0 |
| Storage Lanes | | 1 | | 0 |
| Taper Length (ft) | | 25 | | |
| Lane Util. Factor | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | | | | |
| Frt | | | 0.978 | |
| Flt Protected | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1526 | 3202 | 0 |
| Flt Permitted | | 0.950 | | |
| Satd. Flow (perm) | 0 | 1526 | 3202 | 0 |
| Right Turn on Red | | | | Yes |
| Satd. Flow (RTOR) | | | 17 | |
| Link Speed (mph) | | | 45 | |
| Link Distance (ft) | | | 687 | |
| Travel Time (s) | | | 10.4 | |
| Confl. Peds. (#/hr) | | | | |
| Confl. Bikes (#/hr) | | | | |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (%) | 0% | 19% | 12% | 0% |
| Adj. Flow (vph) | 3 | 79 | 436 | 74 |
| Shared Lane Traffic (%) | | | | |
| Lane Group Flow (vph) | 0 | 82 | 510 | 0 |
| Enter Blocked Intersection | No | No | No | No |
| Lane Alignment | R NA | Left | Left | Right |
| Median Width(ft) | | | 12 | |
| Link Offset(ft) | | | 0 | |
| Crosswalk Width(ft) | | | 16 | |
| Two way Left Turn Lane | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 9 | 15 | | 9 |
| Turn Type | Prot | Prot | NA | |
| Protected Phases | 1 | 1 | 6 | |
| Permitted Phases | | | | |
| Detector Phase | 1 | 1 | 6 | |
| Switch Phase | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | 10.0 | |
| Minimum Split (s) | 14.7 | 14.7 | 33.8 | |
| Total Split (s) | 18.7 | 18.7 | 33.8 | |
| Total Split (%) | 17.4% | 17.4% | 31.5% | |
| Maximum Green (s) | 15.0 | 15.0 | 28.0 | |
| Yellow Time (s) | 3.7 | 3.7 | 4.8 | |
| All-Red Time (s) | 0.0 | 0.0 | 1.0 | |
| Lost Time Adjust (s) | | 0.0 | 0.0 | |
| Total Lost Time (s) | | 3.7 | 5.8 | |
| Lead/Lag | Lead | Lead | Lag | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project AM Peak Hour



| Lane Group | EBU | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | None | None | None | Min |
| Walk Time (s) | | | 7.0 | 7.0 | | | 7.0 | 7.0 | | | | 7.0 |
| Flash Dont Walk (s) | | | 25.0 | 25.0 | | | 25.0 | 25.0 | | | | 21.0 |
| Pedestrian Calls (#/hr) | | | 1 | 1 | | | 0 | 0 | | | | 3 |
| Act Effct Green (s) | | 17.1 | 15.3 | 15.3 | | 17.1 | 15.3 | 15.3 | | 12.0 | 16.6 | |
| Actuated g/C Ratio | | 0.25 | 0.22 | 0.22 | | 0.25 | 0.22 | 0.22 | | 0.17 | 0.24 | |
| v/c Ratio | | 0.60 | 0.15 | 0.12 | | 0.61 | 0.08 | 0.16 | | 0.39 | 0.74 | |
| Control Delay | | 38.1 | 27.1 | 0.6 | | 61.3 | 26.3 | 1.7 | | 37.4 | 32.6 | |
| Queue Delay | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Delay | | 38.1 | 27.1 | 0.6 | | 61.3 | 26.3 | 1.7 | | 37.4 | 32.6 | |
| LOS | | D | C | A | | E | C | A | | D | C | |
| Approach Delay | | | 31.3 | | | | 31.7 | | | | | 33.4 |
| Approach LOS | | | C | | | | C | | | | | C |

Intersection Summary

Area Type: Other
 Cycle Length: 107.4
 Actuated Cycle Length: 69.5
 Natural Cycle: 100
 Control Type: Actuated-Uncoordinated
 Maximum v/c Ratio: 0.74
 Intersection Signal Delay: 31.9
 Intersection LOS: C
 Intersection Capacity Utilization 63.2%
 ICU Level of Service B
 Analysis Period (min) 15

Splits and Phases: 3: SR 113 & N. Lincoln St/Vaughn Rd

| | | | |
|--------|--------|--------|--------|
| Ø1 | Ø2 | Ø3 | Ø4 |
| 18.7 s | 33.8 s | 18.7 s | 36.2 s |
| Ø5 | Ø6 | Ø7 | Ø8 |
| 18.7 s | 33.8 s | 18.7 s | 36.2 s |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project AM Peak Hour



| Lane Group | SBU | SBL | SBT | SBR |
|-----------------------------|------|------|------|-----|
| Lead-Lag Optimize? | Yes | Yes | Yes | |
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | |
| Minimum Gap (s) | 1.0 | 1.0 | 3.0 | |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | |
| Recall Mode | None | None | Min | |
| Walk Time (s) | | | 7.0 | |
| Flash Dont Walk (s) | | | 21.0 | |
| Pedestrian Calls (#/hr) | | | 0 | |
| Act Effct Green (s) | | 12.8 | 17.0 | |
| Actuated g/C Ratio | | 0.18 | 0.24 | |
| v/c Ratio | | 0.29 | 0.64 | |
| Control Delay | | 36.1 | 29.6 | |
| Queue Delay | | 0.0 | 0.0 | |
| Total Delay | | 36.1 | 29.6 | |
| LOS | | D | C | |
| Approach Delay | | | 30.5 | |
| Approach LOS | | | C | |
| Intersection Summary | | | | |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term Plus Project AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 32 | 7 | 53 | 1 | 22 | 1 | 19 | 30 | 542 | 46 | 17 | 45 |
| Future Volume (vph) | 32 | 7 | 53 | 1 | 22 | 1 | 19 | 30 | 542 | 46 | 17 | 45 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 0 | | 250 | | 0 | 115 | | 0 | | 190 |
| Storage Lanes | 1 | | 0 | | 1 | | 0 | 1 | | 0 | | 1 |
| Taper Length (ft) | 25 | | | | 25 | | | 25 | | | | 25 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 |
| Ped Bike Factor | | 0.99 | | | | | | | | | | |
| Frt | | 0.868 | | | | | 0.857 | | 0.988 | | | |
| Flt Protected | 0.950 | | | | 0.950 | | | 0.950 | | | | 0.950 |
| Satd. Flow (prot) | 1597 | 1523 | 0 | 0 | 1479 | 1178 | 0 | 1687 | 3304 | 0 | 0 | 1555 |
| Flt Permitted | 0.950 | | | | 0.950 | | | 0.950 | | | | 0.950 |
| Satd. Flow (perm) | 1597 | 1523 | 0 | 0 | 1479 | 1178 | 0 | 1687 | 3304 | 0 | 0 | 1555 |
| Right Turn on Red | | | Yes | | | | Yes | | | Yes | | |
| Satd. Flow (RTOR) | | 58 | | | | 21 | | | 8 | | | |
| Link Speed (mph) | | 30 | | | | 30 | | | 30 | | | |
| Link Distance (ft) | | 736 | | | | 904 | | | 473 | | | |
| Travel Time (s) | | 16.7 | | | | 20.5 | | | 10.8 | | | |
| Confl. Bikes (#/hr) | | 1 | 2 | | | | | | | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 13% | 29% | 4% | 0% | 23% | 0% | 40% | 7% | 7% | 19% | 0% | 22% |
| Adj. Flow (vph) | 35 | 8 | 58 | 1 | 24 | 1 | 21 | 33 | 589 | 50 | 18 | 49 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 35 | 66 | 0 | 0 | 25 | 22 | 0 | 33 | 639 | 0 | 0 | 67 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | R NA | Left | Left | Right | Left | Left | Right | R NA | Left |
| Median Width(ft) | | 12 | | | | 12 | | | 12 | | | |
| Link Offset(ft) | | 0 | | | | 0 | | | 0 | | | |
| Crosswalk Width(ft) | | 16 | | | | 16 | | | 16 | | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 9 | 15 | | 9 | 15 | | 9 | 9 | 15 |
| Turn Type | Prot | NA | | Prot | Prot | NA | | Prot | NA | | Prot | Prot |
| Protected Phases | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 1 |
| Permitted Phases | | | | | | | | | | | | |
| Detector Phase | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | | 11.0 | 11.0 | 11.0 | | 10.0 | 10.0 | | 10.0 | 10.0 |
| Minimum Split (s) | 14.7 | 35.2 | | 14.7 | 14.7 | 35.2 | | 13.7 | 27.8 | | 13.7 | 13.7 |
| Total Split (s) | 18.7 | 35.2 | | 18.7 | 18.7 | 35.2 | | 18.7 | 30.8 | | 18.7 | 18.7 |
| Total Split (%) | 18.1% | 34.0% | | 18.1% | 18.1% | 34.0% | | 18.1% | 29.8% | | 18.1% | 18.1% |
| Maximum Green (s) | 15.0 | 31.0 | | 15.0 | 15.0 | 31.0 | | 15.0 | 25.0 | | 15.0 | 15.0 |
| Yellow Time (s) | 3.7 | 3.7 | | 3.7 | 3.7 | 3.7 | | 3.7 | 4.8 | | 3.7 | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | | 0.0 | 0.0 | 0.5 | | 0.0 | 1.0 | | 0.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | | | 0.0 |
| Total Lost Time (s) | 3.7 | 4.2 | | | 3.7 | 4.2 | | 3.7 | 5.8 | | | 3.7 |
| Lead/Lag | Lead | Lag | | Lead | Lead | Lag | | Lead | Lag | | Lead | Lead |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | | Yes | Yes | | Yes | Yes |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term Plus Project AM Peak Hour



| Lane Group | SBT | SBR |
|----------------------------|-------|-------|
| Lane Configurations | ↑↑ | |
| Traffic Volume (vph) | 352 | 18 |
| Future Volume (vph) | 352 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Storage Length (ft) | | 0 |
| Storage Lanes | | 0 |
| Taper Length (ft) | | |
| Lane Util. Factor | 0.95 | 0.95 |
| Ped Bike Factor | 1.00 | |
| Frt | 0.993 | |
| Flt Protected | | |
| Satd. Flow (prot) | 3257 | 0 |
| Flt Permitted | | |
| Satd. Flow (perm) | 3257 | 0 |
| Right Turn on Red | | Yes |
| Satd. Flow (RTOR) | 5 | |
| Link Speed (mph) | 45 | |
| Link Distance (ft) | 1866 | |
| Travel Time (s) | 28.3 | |
| Confl. Bikes (#/hr) | | 1 |
| Peak Hour Factor | 0.92 | 0.92 |
| Heavy Vehicles (%) | 10% | 9% |
| Adj. Flow (vph) | 383 | 20 |
| Shared Lane Traffic (%) | | |
| Lane Group Flow (vph) | 403 | 0 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Right |
| Median Width(ft) | 12 | |
| Link Offset(ft) | 0 | |
| Crosswalk Width(ft) | 16 | |
| Two way Left Turn Lane | Yes | |
| Headway Factor | 1.00 | 1.00 |
| Turning Speed (mph) | | 9 |
| Turn Type | NA | |
| Protected Phases | 6 | |
| Permitted Phases | | |
| Detector Phase | 6 | |
| Switch Phase | | |
| Minimum Initial (s) | 10.0 | |
| Minimum Split (s) | 27.8 | |
| Total Split (s) | 30.8 | |
| Total Split (%) | 29.8% | |
| Maximum Green (s) | 25.0 | |
| Yellow Time (s) | 4.8 | |
| All-Red Time (s) | 1.0 | |
| Lost Time Adjust (s) | 0.0 | |
| Total Lost Time (s) | 5.8 | |
| Lead/Lag | Lag | |
| Lead-Lag Optimize? | Yes | |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term Plus Project AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL |
|-------------------------|------|------|-----|------|------|------|-----|------|------|-----|------|------|
| Vehicle Extension (s) | 0.2 | 0.2 | | 0.2 | 0.2 | 0.2 | | 0.2 | 0.2 | | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | | 0.1 | 0.1 | 0.1 | | 0.1 | 0.1 | | 0.1 | 0.1 |
| Recall Mode | None | None | | None | None | None | | None | Min | | None | None |
| Walk Time (s) | | 7.0 | | | | 7.0 | | | 7.0 | | | |
| Flash Dont Walk (s) | | 24.0 | | | | 24.0 | | | 15.0 | | | |
| Pedestrian Calls (#/hr) | | 2 | | | | 0 | | | 0 | | | |
| Act Effct Green (s) | 16.4 | 16.2 | | | 14.0 | 16.2 | | 12.8 | 29.1 | | | 12.8 |
| Actuated g/C Ratio | 0.31 | 0.31 | | | 0.27 | 0.31 | | 0.24 | 0.55 | | | 0.24 |
| v/c Ratio | 0.07 | 0.13 | | | 0.06 | 0.06 | | 0.08 | 0.35 | | | 0.18 |
| Control Delay | 24.8 | 8.9 | | | 29.4 | 11.1 | | 29.6 | 18.8 | | | 29.0 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | | | 0.0 |
| Total Delay | 24.8 | 8.9 | | | 29.4 | 11.1 | | 29.6 | 18.8 | | | 29.0 |
| LOS | C | A | | | C | B | | C | B | | | C |
| Approach Delay | | 14.4 | | | | 20.9 | | | 19.3 | | | |
| Approach LOS | | B | | | | C | | | B | | | |

Intersection Summary

| | |
|-----------------------------------|------------------------|
| Area Type: | Other |
| Cycle Length: | 103.4 |
| Actuated Cycle Length: | 52.5 |
| Natural Cycle: | 95 |
| Control Type: | Actuated-Uncoordinated |
| Maximum v/c Ratio: | 0.35 |
| Intersection Signal Delay: | 18.3 |
| Intersection LOS: | B |
| Intersection Capacity Utilization | 45.6% |
| ICU Level of Service | A |
| Analysis Period (min) | 15 |

Splits and Phases: 4: SR 113 & Regency Pkwy/Industrial Wy

| | | | |
|--------|--------|--------|--------|
| | | | |
| 18.7 s | 30.8 s | 18.7 s | 35.2 s |
| | | | |
| 18.7 s | 30.8 s | 18.7 s | 35.2 s |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term Plus Project AM Peak Hour



| Lane Group | SBT | SBR |
|-------------------------|------|-----|
| Vehicle Extension (s) | 0.2 | |
| Minimum Gap (s) | 1.0 | |
| Time Before Reduce (s) | 1.0 | |
| Time To Reduce (s) | 0.1 | |
| Recall Mode | Min | |
| Walk Time (s) | 7.0 | |
| Flash Dont Walk (s) | 15.0 | |
| Pedestrian Calls (#/hr) | 1 | |
| Act Effct Green (s) | 32.3 | |
| Actuated g/C Ratio | 0.62 | |
| v/c Ratio | 0.20 | |
| Control Delay | 15.6 | |
| Queue Delay | 0.0 | |
| Total Delay | 15.6 | |
| LOS | B | |
| Approach Delay | 17.5 | |
| Approach LOS | B | |
| Intersection Summary | | |

Independence at Dixon TIA

1: SR 113/I-80 EB Ramps & I-80 WB Ramps/Auction Ln

Near-Term Plus Project AM Peak Hour

| Intersection | | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 2.3 | | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL | SBT | SBR |
| Lane Configurations | | ↖ | ↗ | | ↕ | | ↖ | ↗ | | | | ↕ | |
| Traffic Vol, veh/h | 7 | 0 | 437 | 1 | 2 | 0 | 174 | 414 | 1 | 1 | 1 | 170 | 13 |
| Future Vol, veh/h | 7 | 0 | 437 | 1 | 2 | 0 | 174 | 414 | 1 | 1 | 1 | 170 | 13 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | Free | - | - | None | - | - | None | - | - | - | None |
| Storage Length | - | - | 0 | - | - | - | 0 | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | - | 0 | - |
| Peak Hour Factor | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| Heavy Vehicles, % | 29 | 0 | 11 | 100 | 100 | 0 | 21 | 15 | 100 | 0 | 0 | 20 | 13 |
| Mvmt Flow | 8 | 0 | 508 | 1 | 2 | 0 | 202 | 481 | 1 | 1 | 1 | 198 | 15 |

| Major/Minor | Minor2 | | Minor1 | | Major1 | | Major2 | | | | | | |
|----------------------|--------|------|--------|------|--------|-----|--------|---|---|---|------|---|---|
| Conflicting Flow All | 1095 | 1096 | - | 1094 | 1103 | 482 | 213 | 0 | 0 | - | 482 | 0 | 0 |
| Stage 1 | 208 | 210 | - | 886 | 886 | - | - | - | - | - | - | - | - |
| Stage 2 | 887 | 886 | - | 208 | 217 | - | - | - | - | - | - | - | - |
| Critical Hdwy | 7.39 | 6.5 | - | 8.1 | 7.5 | 6.2 | 4.31 | - | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.761 | 4 | - | 4.4 | 4.9 | 3.3 | 2.389 | - | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 170 | 215 | 0 | 127 | 143 | 588 | 1252 | - | - | - | 1091 | - | - |
| Stage 1 | 736 | 732 | 0 | 233 | 255 | - | - | - | - | - | - | - | - |
| Stage 2 | 304 | 365 | 0 | 615 | 573 | - | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | | | - | - |
| Mov Cap-1 Maneuver | 147 | 180 | - | 111 | 120 | 588 | 1252 | - | - | ~ | ~ | - | - |
| Mov Cap-2 Maneuver | 147 | 180 | - | 111 | 120 | - | - | - | - | - | - | - | - |
| Stage 1 | 618 | 732 | - | 195 | 214 | - | - | - | - | - | - | - | - |
| Stage 2 | 252 | 306 | - | 615 | 573 | - | - | - | - | - | - | - | - |

| Approach | EB | | WB | | NB | | SB | |
|----------------------|------|--|------|--|-----|--|----|--|
| HCM Control Delay, s | 30.9 | | 36.7 | | 2.5 | | | |
| HCM LOS | D | | E | | | | | |

| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | EBLn2 | WBLn1 | SBL | SBT | SBR |
|-----------------------|-------|-----|-----|-------|-------|-------|-----|-----|-----|
| Capacity (veh/h) | 1252 | - | - | 147 | - | 117 | ~ | - | - |
| HCM Lane V/C Ratio | 0.162 | - | - | 0.055 | - | 0.03 | ~ | - | - |
| HCM Control Delay (s) | 8.4 | - | - | 30.9 | 0 | 36.7 | - | - | - |
| HCM Lane LOS | A | - | - | D | A | E | - | - | - |
| HCM 95th %tile Q(veh) | 0.6 | - | - | 0.2 | - | 0.1 | ~ | - | - |

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

Independence at Dixon TIA
 5: Project Dwy 1 & N. Lincoln St

Near-Term Plus Project AM Peak Hour

| Intersection | | | | | | |
|--------------------------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.6 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ↑↑ | | | ↑↑ | | ↑ |
| Traffic Vol, veh/h | 302 | 5 | 0 | 167 | 0 | 35 |
| Future Vol, veh/h | 302 | 5 | 0 | 167 | 0 | 35 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | - | 0 |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 328 | 5 | 0 | 182 | 0 | 38 |

| Major/Minor | Major1 | Major2 | Minor1 | | | |
|----------------------|--------|--------|--------|---|---|------|
| Conflicting Flow All | 0 | 0 | - | - | - | 167 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | - | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | - | - | - | 3.32 |
| Pot Cap-1 Maneuver | - | - | 0 | - | 0 | 848 |
| Stage 1 | - | - | 0 | - | 0 | - |
| Stage 2 | - | - | 0 | - | 0 | - |
| Platoon blocked, % | - | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | - | - | - | 848 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |

| Approach | EB | WB | NB |
|----------------------|----|----|-----|
| HCM Control Delay, s | 0 | 0 | 9.4 |
| HCM LOS | | | A |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBT |
|-----------------------|-------|-----|-----|-----|
| Capacity (veh/h) | 848 | - | - | - |
| HCM Lane V/C Ratio | 0.045 | - | - | - |
| HCM Control Delay (s) | 9.4 | - | - | - |
| HCM Lane LOS | A | - | - | - |
| HCM 95th %tile Q(veh) | 0.1 | - | - | - |

Independence at Dixon TIA
6: SR 113 & Project Dwy 2

Near-Term Plus Project AM Peak Hour

| Intersection | | | | | | |
|--------------------------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.5 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 23 | 10 | 3 | 634 | 505 | 15 |
| Future Vol, veh/h | 23 | 10 | 3 | 634 | 505 | 15 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 100 | - | - | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 25 | 11 | 3 | 689 | 549 | 16 |

| Major/Minor | Minor2 | Major1 | | Major2 | |
|----------------------|--------|--------|------|--------|---|
| Conflicting Flow All | 908 | 283 | 565 | 0 | 0 |
| Stage 1 | 557 | - | - | - | - |
| Stage 2 | 351 | - | - | - | - |
| Critical Hdwy | 6.84 | 6.94 | 4.14 | - | - |
| Critical Hdwy Stg 1 | 5.84 | - | - | - | - |
| Critical Hdwy Stg 2 | 5.84 | - | - | - | - |
| Follow-up Hdwy | 3.52 | 3.32 | 2.22 | - | - |
| Pot Cap-1 Maneuver | 275 | 714 | 1003 | - | - |
| Stage 1 | 537 | - | - | - | - |
| Stage 2 | 684 | - | - | - | - |
| Platoon blocked, % | | | | - | - |
| Mov Cap-1 Maneuver | 274 | 714 | 1003 | - | - |
| Mov Cap-2 Maneuver | 274 | - | - | - | - |
| Stage 1 | 535 | - | - | - | - |
| Stage 2 | 684 | - | - | - | - |

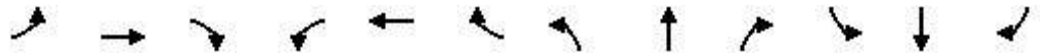
| Approach | EB | NB | SB |
|----------------------|----|----|----|
| HCM Control Delay, s | 17 | 0 | 0 |
| HCM LOS | C | | |

| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | SBT | SBR |
|-----------------------|-------|-----|-------|-----|-----|
| Capacity (veh/h) | 1003 | - | 337 | - | - |
| HCM Lane V/C Ratio | 0.003 | - | 0.106 | - | - |
| HCM Control Delay (s) | 8.6 | - | 17 | - | - |
| HCM Lane LOS | A | - | C | - | - |
| HCM 95th %tile Q(veh) | 0 | - | 0.4 | - | - |

Independence at Dixon TIA

2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term Plus Project AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 77 | 16 | 32 | 95 | 7 | 40 | 141 | 553 | 145 | 117 | 478 | 83 |
| v/c Ratio | 0.11 | 0.04 | 0.07 | 0.12 | 0.01 | 0.09 | 0.36 | 0.46 | 0.21 | 0.16 | 0.61 | 0.20 |
| Control Delay | 31.5 | 24.4 | 0.3 | 31.2 | 24.5 | 0.4 | 35.0 | 27.3 | 6.5 | 31.3 | 29.6 | 8.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 31.5 | 24.4 | 0.3 | 31.2 | 24.5 | 0.4 | 35.0 | 27.3 | 6.5 | 31.3 | 29.6 | 8.7 |
| Queue Length 50th (ft) | 14 | 6 | 0 | 18 | 3 | 0 | 56 | 122 | 0 | 22 | 100 | 0 |
| Queue Length 95th (ft) | 46 | 22 | 0 | 54 | 13 | 0 | 153 | 235 | 44 | 64 | 206 | 36 |
| Internal Link Dist (ft) | | 520 | | | 616 | | | 607 | | | 887 | |
| Turn Bay Length (ft) | 150 | | 160 | 195 | | 195 | 200 | | 320 | 235 | | 135 |
| Base Capacity (vph) | 898 | 1069 | 1021 | 915 | 1186 | 921 | 475 | 1815 | 976 | 843 | 1815 | 826 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.09 | 0.01 | 0.03 | 0.10 | 0.01 | 0.04 | 0.30 | 0.30 | 0.15 | 0.14 | 0.26 | 0.10 |

Intersection Summary

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project AM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|-------------------------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 260 | 62 | 49 | 62 | 33 | 55 | 119 | 572 | 82 | 510 |
| v/c Ratio | 0.60 | 0.15 | 0.12 | 0.61 | 0.08 | 0.16 | 0.39 | 0.74 | 0.29 | 0.64 |
| Control Delay | 38.1 | 27.1 | 0.6 | 61.3 | 26.3 | 1.7 | 37.4 | 32.6 | 36.1 | 29.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 38.1 | 27.1 | 0.6 | 61.3 | 26.3 | 1.7 | 37.4 | 32.6 | 36.1 | 29.6 |
| Queue Length 50th (ft) | 102 | 23 | 0 | 24 | 12 | 0 | 47 | 118 | 31 | 101 |
| Queue Length 95th (ft) | #350 | 62 | 0 | #133 | 38 | 4 | 134 | 235 | 101 | 213 |
| Internal Link Dist (ft) | | 357 | | | 279 | | | 1083 | | 607 |
| Turn Bay Length (ft) | 275 | | | 180 | | 230 | 290 | | 285 | |
| Base Capacity (vph) | 431 | 995 | 822 | 102 | 995 | 675 | 430 | 1457 | 374 | 1476 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.60 | 0.06 | 0.06 | 0.61 | 0.03 | 0.08 | 0.28 | 0.39 | 0.22 | 0.35 |

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term Plus Project AM Peak Hour



| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
|-----------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 35 | 66 | 25 | 22 | 33 | 639 | 67 | 403 |
| v/c Ratio | 0.07 | 0.13 | 0.06 | 0.06 | 0.08 | 0.35 | 0.18 | 0.20 |
| Control Delay | 24.8 | 8.9 | 29.4 | 11.1 | 29.6 | 18.8 | 29.0 | 15.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 24.8 | 8.9 | 29.4 | 11.1 | 29.6 | 18.8 | 29.0 | 15.6 |
| Queue Length 50th (ft) | 7 | 2 | 5 | 0 | 7 | 82 | 15 | 24 |
| Queue Length 95th (ft) | 49 | 32 | 39 | 18 | 47 | 246 | 81 | 150 |
| Internal Link Dist (ft) | | 656 | | 824 | | 393 | | 1786 |
| Turn Bay Length (ft) | 150 | | 250 | | 115 | | 190 | |
| Base Capacity (vph) | 635 | 1072 | 538 | 821 | 614 | 2103 | 566 | 2081 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.06 | 0.06 | 0.05 | 0.03 | 0.05 | 0.30 | 0.12 | 0.19 |
| Intersection Summary | | | | | | | | |

Independence at Dixon TIA
2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term Plus Project PM Peak Hour

| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 132 | 11 | 87 | 1 | 255 | 18 | 139 | 25 | 105 | 560 | 191 | 171 |
| Future Volume (vph) | 132 | 11 | 87 | 1 | 255 | 18 | 139 | 25 | 105 | 560 | 191 | 171 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 160 | | 195 | | 195 | | 200 | | 320 | 235 |
| Storage Lanes | 2 | | 1 | | 2 | | 1 | | 1 | | 1 | 2 |
| Taper Length (ft) | 25 | | | | 25 | | | | 25 | | | 25 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 | 0.97 |
| Ped Bike Factor | | | 0.99 | | | | | | | | 0.98 | |
| Frt | | | 0.850 | | | | 0.850 | | | | 0.850 | |
| Flt Protected | 0.950 | | | | 0.950 | | | | 0.950 | | | 0.950 |
| Satd. Flow (prot) | 2968 | 1652 | 1553 | 0 | 3273 | 1900 | 1442 | 0 | 1776 | 3139 | 1583 | 3155 |
| Flt Permitted | 0.950 | | | | 0.950 | | | | 0.950 | | | 0.950 |
| Satd. Flow (perm) | 2968 | 1652 | 1532 | 0 | 3273 | 1900 | 1442 | 0 | 1776 | 3139 | 1558 | 3155 |
| Right Turn on Red | | | Yes | | | | Yes | | | | Yes | |
| Satd. Flow (RTOR) | | | 91 | | | | 145 | | | | 199 | |
| Link Speed (mph) | | 35 | | | | 35 | | | | 45 | | |
| Link Distance (ft) | | 600 | | | | 696 | | | | 687 | | |
| Travel Time (s) | | 11.7 | | | | 13.6 | | | | 10.4 | | |
| Confl. Peds. (#/hr) | | | 1 | | | | | | | | | 3 |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | 1 |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (%) | 18% | 15% | 4% | 0% | 7% | 0% | 12% | 0% | 2% | 15% | 2% | 11% |
| Adj. Flow (vph) | 138 | 11 | 91 | 1 | 266 | 19 | 145 | 26 | 109 | 583 | 199 | 178 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 138 | 11 | 91 | 0 | 267 | 19 | 145 | 0 | 135 | 583 | 199 | 178 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | R NA | Left | Left | Right | R NA | Left | Left | Right | Left |
| Median Width(ft) | | 24 | | | | 24 | | | | 24 | | |
| Link Offset(ft) | | 0 | | | | 0 | | | | 0 | | |
| Crosswalk Width(ft) | | 16 | | | | 16 | | | | 16 | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 9 | 15 | | 9 | 9 | 15 | | 9 | 15 |
| Turn Type | Prot | NA | Perm | Prot | Prot | NA | Perm | Prot | Prot | NA | Perm | Prot |
| Protected Phases | 7 | 4 | | 3 | 3 | 8 | | 5 | 5 | 2 | | 1 |
| Permitted Phases | | | 4 | | | | 8 | | | | 2 | |
| Detector Phase | 7 | 4 | 4 | 3 | 3 | 8 | 8 | 5 | 5 | 2 | 2 | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 13.0 | 12.0 | 12.0 | 13.0 | 13.0 | 12.0 | 12.0 | 12.0 | 12.0 | 10.0 | 10.0 | 13.0 |
| Minimum Split (s) | 16.7 | 41.6 | 41.6 | 16.0 | 16.0 | 41.6 | 41.6 | 15.7 | 15.7 | 36.8 | 36.8 | 16.7 |
| Total Split (s) | 20.7 | 41.6 | 41.6 | 18.7 | 18.7 | 41.6 | 41.6 | 18.7 | 18.7 | 36.8 | 36.8 | 18.7 |
| Total Split (%) | 17.3% | 34.7% | 34.7% | 15.6% | 15.6% | 34.7% | 34.7% | 15.6% | 15.6% | 30.7% | 30.7% | 15.6% |
| Maximum Green (s) | 17.0 | 37.0 | 37.0 | 15.7 | 15.7 | 37.0 | 37.0 | 15.0 | 15.0 | 31.0 | 31.0 | 15.0 |
| Yellow Time (s) | 3.7 | 4.1 | 4.1 | 3.0 | 3.0 | 4.1 | 4.1 | 3.7 | 3.7 | 4.8 | 4.8 | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | 1.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 3.7 | 4.6 | 4.6 | | 3.0 | 4.6 | 4.6 | | 3.7 | 5.8 | 5.8 | 3.7 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead | Lead | Lag | Lag | Lead |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term Plus Project PM Peak Hour



| Lane Group | SBT | SBR |
|----------------------------|-------|-------|
| Lane Configurations | ↑↑ | ↑ |
| Traffic Volume (vph) | 435 | 131 |
| Future Volume (vph) | 435 | 131 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Storage Length (ft) | | 135 |
| Storage Lanes | | 1 |
| Taper Length (ft) | | |
| Lane Util. Factor | 0.95 | 1.00 |
| Ped Bike Factor | | |
| Frt | | 0.850 |
| Flt Protected | | |
| Satd. Flow (prot) | 3139 | 1369 |
| Flt Permitted | | |
| Satd. Flow (perm) | 3139 | 1369 |
| Right Turn on Red | | Yes |
| Satd. Flow (RTOR) | | 136 |
| Link Speed (mph) | 45 | |
| Link Distance (ft) | 967 | |
| Travel Time (s) | 14.7 | |
| Confl. Peds. (#/hr) | | |
| Confl. Bikes (#/hr) | | |
| Peak Hour Factor | 0.96 | 0.96 |
| Heavy Vehicles (%) | 15% | 18% |
| Adj. Flow (vph) | 453 | 136 |
| Shared Lane Traffic (%) | | |
| Lane Group Flow (vph) | 453 | 136 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Right |
| Median Width(ft) | 24 | |
| Link Offset(ft) | 0 | |
| Crosswalk Width(ft) | 16 | |
| Two way Left Turn Lane | | |
| Headway Factor | 1.00 | 1.00 |
| Turning Speed (mph) | | 9 |
| Turn Type | NA | Perm |
| Protected Phases | 6 | |
| Permitted Phases | | 6 |
| Detector Phase | 6 | 6 |
| Switch Phase | | |
| Minimum Initial (s) | 10.0 | 10.0 |
| Minimum Split (s) | 38.8 | 38.8 |
| Total Split (s) | 38.8 | 38.8 |
| Total Split (%) | 32.4% | 32.4% |
| Maximum Green (s) | 33.0 | 33.0 |
| Yellow Time (s) | 4.8 | 4.8 |
| All-Red Time (s) | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |
| Total Lost Time (s) | 5.8 | 5.8 |
| Lead/Lag | Lag | Lag |

Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term Plus Project PM Peak Hour

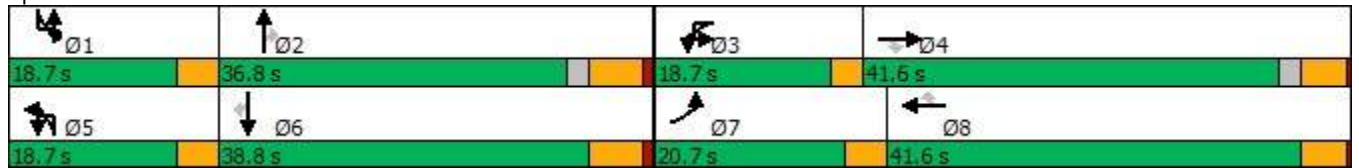


| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBL |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 2.0 | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 | 3.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.2 | 1.2 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | None | Min | Min | None |
| Walk Time (s) | | 7.0 | 7.0 | | | 7.0 | 7.0 | | | 7.0 | 7.0 | |
| Flash Dont Walk (s) | | 30.0 | 30.0 | | | 30.0 | 30.0 | | | 24.0 | 24.0 | |
| Pedestrian Calls (#/hr) | | 1 | 1 | | | 0 | 0 | | | 3 | 3 | |
| Act Effect Green (s) | 13.5 | 16.4 | 16.4 | | 17.9 | 16.2 | 16.2 | | 12.9 | 17.6 | 17.6 | 13.5 |
| Actuated g/C Ratio | 0.17 | 0.21 | 0.21 | | 0.23 | 0.20 | 0.20 | | 0.16 | 0.22 | 0.22 | 0.17 |
| v/c Ratio | 0.27 | 0.03 | 0.23 | | 0.36 | 0.05 | 0.35 | | 0.47 | 0.84 | 0.40 | 0.33 |
| Control Delay | 34.3 | 26.0 | 7.8 | | 32.8 | 25.8 | 7.4 | | 39.8 | 41.5 | 7.0 | 34.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.3 | 26.0 | 7.8 | | 32.8 | 25.8 | 7.4 | | 39.8 | 41.5 | 7.0 | 34.6 |
| LOS | C | C | A | | C | C | A | | D | D | A | C |
| Approach Delay | | 23.9 | | | | 23.9 | | | | 33.7 | | |
| Approach LOS | | C | | | | C | | | | C | | |

Intersection Summary

Area Type: Other
 Cycle Length: 119.8
 Actuated Cycle Length: 79.3
 Natural Cycle: 115
 Control Type: Actuated-Uncoordinated
 Maximum v/c Ratio: 0.84
 Intersection Signal Delay: 29.3
 Intersection LOS: C
 Intersection Capacity Utilization 63.5%
 ICU Level of Service B
 Analysis Period (min) 15

Splits and Phases: 2: SR 113 & Dorset Dr/E. Dorset Dr



Independence at Dixon TIA
 2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term Plus Project PM Peak Hour



| Lane Group | SBT | SBR |
|-------------------------|------|------|
| Lead-Lag Optimize? | Yes | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 |
| Minimum Gap (s) | 3.0 | 3.0 |
| Time Before Reduce (s) | 1.2 | 1.2 |
| Time To Reduce (s) | 0.1 | 0.1 |
| Recall Mode | Min | Min |
| Walk Time (s) | 7.0 | 7.0 |
| Flash Dont Walk (s) | 26.0 | 26.0 |
| Pedestrian Calls (#/hr) | 0 | 0 |
| Act Effct Green (s) | 18.2 | 18.2 |
| Actuated g/C Ratio | 0.23 | 0.23 |
| v/c Ratio | 0.63 | 0.32 |
| Control Delay | 32.5 | 7.8 |
| Queue Delay | 0.0 | 0.0 |
| Total Delay | 32.5 | 7.8 |
| LOS | C | A |
| Approach Delay | 28.6 | |
| Approach LOS | C | |
| Intersection Summary | | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project PM Peak Hour



| Lane Group | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 25 | 210 | 45 | 74 | 119 | 57 | 74 | 65 | 72 | 495 | 62 | 9 |
| Future Volume (vph) | 25 | 210 | 45 | 74 | 119 | 57 | 74 | 65 | 72 | 495 | 62 | 9 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | | 275 | | 0 | 180 | | 230 | | 290 | | 0 | |
| Storage Lanes | | 1 | | 1 | 1 | | 1 | | 1 | | 0 | |
| Taper Length (ft) | | 25 | | | 25 | | | | 25 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 | 0.95 | 0.95 |
| Ped Bike Factor | | | | 0.99 | | | | | | 1.00 | | |
| Frt | | | | 0.850 | | | 0.850 | | | 0.983 | | |
| Flt Protected | | 0.950 | | | 0.950 | | | | 0.950 | | | |
| Satd. Flow (prot) | 0 | 1758 | 1900 | 1495 | 1687 | 1900 | 1196 | 0 | 1724 | 3176 | 0 | 0 |
| Flt Permitted | | 0.950 | | | 0.950 | | | | 0.950 | | | |
| Satd. Flow (perm) | 0 | 1758 | 1900 | 1476 | 1687 | 1900 | 1196 | 0 | 1724 | 3176 | 0 | 0 |
| Right Turn on Red | | | | Yes | | | Yes | | | | Yes | |
| Satd. Flow (RTOR) | | | | 104 | | | 104 | | | 12 | | |
| Link Speed (mph) | | | 35 | | | 45 | | | | 45 | | |
| Link Distance (ft) | | | 437 | | | 359 | | | | 1163 | | |
| Travel Time (s) | | | 8.5 | | | 5.4 | | | | 17.6 | | |
| Confl. Peds. (#/hr) | | | | 1 | | | | | | | 3 | |
| Confl. Bikes (#/hr) | | | 1 | | | | | | | | | |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (%) | 0% | 3% | 0% | 8% | 7% | 0% | 35% | 0% | 9% | 12% | 8% | 0% |
| Adj. Flow (vph) | 27 | 226 | 48 | 80 | 128 | 61 | 80 | 70 | 77 | 532 | 67 | 10 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 253 | 48 | 80 | 128 | 61 | 80 | 0 | 147 | 599 | 0 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | R NA | Left | Left | Right | Left | Left | Right | R NA | Left | Left | Right | R NA |
| Median Width(ft) | | | 12 | | | 12 | | | | 12 | | |
| Link Offset(ft) | | | 0 | | | 0 | | | | 0 | | |
| Crosswalk Width(ft) | | | 16 | | | 16 | | | | 16 | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 9 | 15 | | 9 | 15 | | 9 | 9 | 15 | | 9 | 9 |
| Turn Type | Prot | Prot | NA | Perm | Prot | NA | Perm | Prot | Prot | NA | | Prot |
| Protected Phases | 7 | 7 | 4 | | 3 | 8 | | 5 | 5 | 2 | | 1 |
| Permitted Phases | | | | 4 | | | 8 | | | | | |
| Detector Phase | 7 | 7 | 4 | 4 | 3 | 8 | 8 | 5 | 5 | 2 | | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 10.0 | 10.0 | 10.0 | | 11.0 |
| Minimum Split (s) | 14.7 | 14.7 | 36.2 | 36.2 | 14.7 | 36.2 | 36.2 | 13.7 | 13.7 | 33.8 | | 14.7 |
| Total Split (s) | 18.7 | 18.7 | 36.2 | 36.2 | 18.7 | 36.2 | 36.2 | 18.7 | 18.7 | 33.8 | | 18.7 |
| Total Split (%) | 17.4% | 17.4% | 33.7% | 33.7% | 17.4% | 33.7% | 33.7% | 17.4% | 17.4% | 31.5% | | 17.4% |
| Maximum Green (s) | 15.0 | 15.0 | 32.0 | 32.0 | 15.0 | 32.0 | 32.0 | 15.0 | 15.0 | 28.0 | | 15.0 |
| Yellow Time (s) | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 4.8 | | 3.7 |
| All-Red Time (s) | 0.0 | 0.0 | 0.5 | 0.5 | 0.0 | 0.5 | 0.5 | 0.0 | 0.0 | 1.0 | | 0.0 |
| Lost Time Adjust (s) | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Lost Time (s) | | 3.7 | 4.2 | 4.2 | 3.7 | 4.2 | 4.2 | | 3.7 | 5.8 | | |
| Lead/Lag | Lead | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lead | Lag | | Lead |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project PM Peak Hour



| Lane Group | SBL | SBT | SBR |
|----------------------------|-------|-------|-------|
| Lane Configurations | | | |
| Traffic Volume (vph) | 65 | 563 | 169 |
| Future Volume (vph) | 65 | 563 | 169 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 |
| Storage Length (ft) | 285 | | 0 |
| Storage Lanes | 1 | | 0 |
| Taper Length (ft) | 25 | | |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | | | |
| Frt | | 0.965 | |
| Flt Protected | 0.950 | | |
| Satd. Flow (prot) | 1548 | 3189 | 0 |
| Flt Permitted | 0.950 | | |
| Satd. Flow (perm) | 1548 | 3189 | 0 |
| Right Turn on Red | | | Yes |
| Satd. Flow (RTOR) | | 36 | |
| Link Speed (mph) | | 45 | |
| Link Distance (ft) | | 687 | |
| Travel Time (s) | | 10.4 | |
| Confl. Peds. (#/hr) | | | |
| Confl. Bikes (#/hr) | | | |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (%) | 19% | 12% | 0% |
| Adj. Flow (vph) | 70 | 605 | 182 |
| Shared Lane Traffic (%) | | | |
| Lane Group Flow (vph) | 80 | 787 | 0 |
| Enter Blocked Intersection | No | No | No |
| Lane Alignment | Left | Left | Right |
| Median Width(ft) | | 12 | |
| Link Offset(ft) | | 0 | |
| Crosswalk Width(ft) | | 16 | |
| Two way Left Turn Lane | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 |
| Turn Type | Prot | NA | |
| Protected Phases | 1 | 6 | |
| Permitted Phases | | | |
| Detector Phase | 1 | 6 | |
| Switch Phase | | | |
| Minimum Initial (s) | 11.0 | 10.0 | |
| Minimum Split (s) | 14.7 | 33.8 | |
| Total Split (s) | 18.7 | 33.8 | |
| Total Split (%) | 17.4% | 31.5% | |
| Maximum Green (s) | 15.0 | 28.0 | |
| Yellow Time (s) | 3.7 | 4.8 | |
| All-Red Time (s) | 0.0 | 1.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | |
| Total Lost Time (s) | 3.7 | 5.8 | |
| Lead/Lag | Lead | Lag | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project PM Peak Hour



| Lane Group | EBU | EBL | EBT | EBR | WBL | WBT | WBR | NBU | NBL | NBT | NBR | SBU |
|-------------------------|------|------|------|------|------|------|------|------|------|------|-----|------|
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 | | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 3.0 | | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 | | 0.1 |
| Recall Mode | None | None | None | None | None | None | None | None | None | Min | | None |
| Walk Time (s) | | | 7.0 | 7.0 | | 7.0 | 7.0 | | | 7.0 | | |
| Flash Dont Walk (s) | | | 25.0 | 25.0 | | 25.0 | 25.0 | | | 21.0 | | |
| Pedestrian Calls (#/hr) | | | 1 | 1 | | 0 | 0 | | | 3 | | |
| Act Effct Green (s) | | 15.9 | 18.2 | 18.2 | 12.2 | 14.7 | 14.7 | | 11.6 | 26.1 | | |
| Actuated g/C Ratio | | 0.20 | 0.23 | 0.23 | 0.16 | 0.19 | 0.19 | | 0.15 | 0.34 | | |
| v/c Ratio | | 0.71 | 0.11 | 0.19 | 0.48 | 0.17 | 0.26 | | 0.57 | 0.56 | | |
| Control Delay | | 46.2 | 27.4 | 4.5 | 42.2 | 30.2 | 5.6 | | 45.3 | 26.8 | | |
| Queue Delay | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | |
| Total Delay | | 46.2 | 27.4 | 4.5 | 42.2 | 30.2 | 5.6 | | 45.3 | 26.8 | | |
| LOS | | D | C | A | D | C | A | | D | C | | |
| Approach Delay | | | 35.0 | | | 28.6 | | | | 30.4 | | |
| Approach LOS | | | D | | | C | | | | C | | |

Intersection Summary

| | |
|------------------------------------|------------------------|
| Area Type: | Other |
| Cycle Length: | 107.4 |
| Actuated Cycle Length: | 77.8 |
| Natural Cycle: | 100 |
| Control Type: | Actuated-Uncoordinated |
| Maximum v/c Ratio: | 0.85 |
| Intersection Signal Delay: | 33.6 |
| Intersection LOS: | C |
| Intersection Capacity Utilization: | 63.2% |
| ICU Level of Service: | B |
| Analysis Period (min): | 15 |

Splits and Phases: 3: SR 113 & N. Lincoln St/Vaughn Rd

| | | | |
|--------|--------|--------|--------|
| | | | |
| 18.7 s | 33.8 s | 18.7 s | 36.2 s |
| | | | |
| 18.7 s | 33.8 s | 18.7 s | 36.2 s |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project PM Peak Hour



| Lane Group | SBL | SBT | SBR |
|-----------------------------|------|------|-----|
| Lead-Lag Optimize? | Yes | Yes | |
| Vehicle Extension (s) | 0.2 | 0.2 | |
| Minimum Gap (s) | 1.0 | 3.0 | |
| Time Before Reduce (s) | 1.0 | 1.0 | |
| Time To Reduce (s) | 0.1 | 0.1 | |
| Recall Mode | None | Min | |
| Walk Time (s) | | 7.0 | |
| Flash Dont Walk (s) | | 21.0 | |
| Pedestrian Calls (#/hr) | | 0 | |
| Act Effct Green (s) | 11.9 | 21.9 | |
| Actuated g/C Ratio | 0.15 | 0.28 | |
| v/c Ratio | 0.34 | 0.85 | |
| Control Delay | 40.2 | 37.0 | |
| Queue Delay | 0.0 | 0.0 | |
| Total Delay | 40.2 | 37.0 | |
| LOS | D | D | |
| Approach Delay | | 37.3 | |
| Approach LOS | | D | |
| Intersection Summary | | | |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term Plus Project PM Peak Hour



| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | | | |
| Traffic Volume (vph) | 25 | 3 | 35 | 1 | 53 | 6 | 57 | 35 | 570 | 17 | 18 | 18 |
| Future Volume (vph) | 25 | 3 | 35 | 1 | 53 | 6 | 57 | 35 | 570 | 17 | 18 | 18 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 150 | | 0 | | 250 | | 0 | 115 | | 0 | | 190 |
| Storage Lanes | 1 | | 0 | | 1 | | 0 | 1 | | 0 | | 1 |
| Taper Length (ft) | 25 | | | | 25 | | | 25 | | | | 25 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 |
| Ped Bike Factor | | 0.99 | | | | 0.99 | | | | | | |
| Frt | | 0.862 | | | | 0.864 | | | 0.996 | | | |
| Flt Protected | 0.950 | | | | 0.950 | | | 0.950 | | | | 0.950 |
| Satd. Flow (prot) | 1597 | 1528 | 0 | 0 | 1472 | 1190 | 0 | 1687 | 3349 | 0 | 0 | 1626 |
| Flt Permitted | 0.950 | | | | 0.950 | | | 0.950 | | | | 0.950 |
| Satd. Flow (perm) | 1597 | 1528 | 0 | 0 | 1472 | 1190 | 0 | 1687 | 3349 | 0 | 0 | 1626 |
| Right Turn on Red | | | Yes | | | | Yes | | | Yes | | |
| Satd. Flow (RTOR) | | 36 | | | | 59 | | | 3 | | | |
| Link Speed (mph) | | 30 | | | | 30 | | | 30 | | | |
| Link Distance (ft) | | 736 | | | | 904 | | | 473 | | | |
| Travel Time (s) | | 16.7 | | | | 20.5 | | | 10.8 | | | |
| Confl. Peds. (#/hr) | | | 1 | | | | 1 | | | | | |
| Confl. Bikes (#/hr) | | 1 | | | | | | | | | | |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (%) | 13% | 29% | 4% | 0% | 23% | 0% | 40% | 7% | 7% | 19% | 0% | 22% |
| Adj. Flow (vph) | 26 | 3 | 36 | 1 | 55 | 6 | 59 | 36 | 594 | 18 | 19 | 19 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 26 | 39 | 0 | 0 | 56 | 65 | 0 | 36 | 612 | 0 | 0 | 38 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | R NA | Left | Left | Right | Left | Left | Right | R NA | Left |
| Median Width(ft) | | 12 | | | | 12 | | | 12 | | | |
| Link Offset(ft) | | 0 | | | | 0 | | | 0 | | | |
| Crosswalk Width(ft) | | 16 | | | | 16 | | | 16 | | | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 | | 9 | 9 | 15 | | 9 | 15 | | 9 | 9 | 15 |
| Turn Type | Prot | NA | | Prot | Prot | NA | | Prot | NA | | Prot | Prot |
| Protected Phases | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 1 |
| Permitted Phases | | | | | | | | | | | | |
| Detector Phase | 7 | 4 | | 3 | 3 | 8 | | 5 | 2 | | 1 | 1 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 11.0 | 11.0 | | 11.0 | 11.0 | 11.0 | | 10.0 | 10.0 | | 10.0 | 10.0 |
| Minimum Split (s) | 14.7 | 35.2 | | 14.7 | 14.7 | 35.2 | | 13.7 | 27.8 | | 13.7 | 13.7 |
| Total Split (s) | 18.7 | 35.2 | | 18.7 | 18.7 | 35.2 | | 18.7 | 30.8 | | 18.7 | 18.7 |
| Total Split (%) | 18.1% | 34.0% | | 18.1% | 18.1% | 34.0% | | 18.1% | 29.8% | | 18.1% | 18.1% |
| Maximum Green (s) | 15.0 | 31.0 | | 15.0 | 15.0 | 31.0 | | 15.0 | 25.0 | | 15.0 | 15.0 |
| Yellow Time (s) | 3.7 | 3.7 | | 3.7 | 3.7 | 3.7 | | 3.7 | 4.8 | | 3.7 | 3.7 |
| All-Red Time (s) | 0.0 | 0.5 | | 0.0 | 0.0 | 0.5 | | 0.0 | 1.0 | | 0.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | | | 0.0 |
| Total Lost Time (s) | 3.7 | 4.2 | | | 3.7 | 4.2 | | 3.7 | 5.8 | | | 3.7 |
| Lead/Lag | Lead | Lag | | Lead | Lead | Lag | | Lead | Lag | | Lead | Lead |

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term Plus Project PM Peak Hour



| Lane Group | SBT | SBR |
|----------------------------|-------|-------|
| Lane Configurations | ↑↑ | |
| Traffic Volume (vph) | 607 | 40 |
| Future Volume (vph) | 607 | 40 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Storage Length (ft) | | 0 |
| Storage Lanes | | 0 |
| Taper Length (ft) | | |
| Lane Util. Factor | 0.95 | 0.95 |
| Ped Bike Factor | 1.00 | |
| Frt | 0.991 | |
| Flt Protected | | |
| Satd. Flow (prot) | 3248 | 0 |
| Flt Permitted | | |
| Satd. Flow (perm) | 3248 | 0 |
| Right Turn on Red | | Yes |
| Satd. Flow (RTOR) | 6 | |
| Link Speed (mph) | 45 | |
| Link Distance (ft) | 1866 | |
| Travel Time (s) | 28.3 | |
| Confl. Peds. (#/hr) | | 4 |
| Confl. Bikes (#/hr) | | |
| Peak Hour Factor | 0.96 | 0.96 |
| Heavy Vehicles (%) | 10% | 9% |
| Adj. Flow (vph) | 632 | 42 |
| Shared Lane Traffic (%) | | |
| Lane Group Flow (vph) | 674 | 0 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Right |
| Median Width(ft) | 12 | |
| Link Offset(ft) | 0 | |
| Crosswalk Width(ft) | 16 | |
| Two way Left Turn Lane | Yes | |
| Headway Factor | 1.00 | 1.00 |
| Turning Speed (mph) | | 9 |
| Turn Type | NA | |
| Protected Phases | 6 | |
| Permitted Phases | | |
| Detector Phase | 6 | |
| Switch Phase | | |
| Minimum Initial (s) | 10.0 | |
| Minimum Split (s) | 27.8 | |
| Total Split (s) | 30.8 | |
| Total Split (%) | 29.8% | |
| Maximum Green (s) | 25.0 | |
| Yellow Time (s) | 4.8 | |
| All-Red Time (s) | 1.0 | |
| Lost Time Adjust (s) | 0.0 | |
| Total Lost Time (s) | 5.8 | |
| Lead/Lag | Lag | |

Independence at Dixon TIA

4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term Plus Project PM Peak Hour

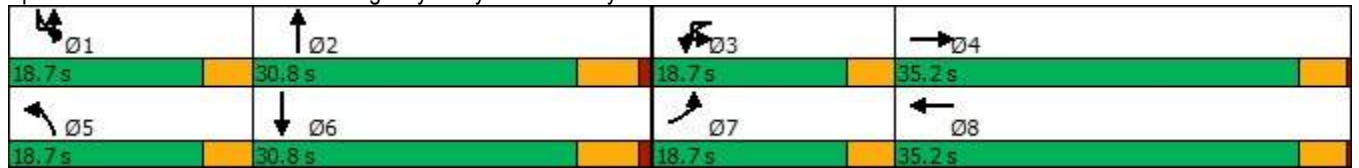


| Lane Group | EBL | EBT | EBR | WBU | WBL | WBT | WBR | NBL | NBT | NBR | SBU | SBL |
|-------------------------|------|------|-----|------|------|------|-----|------|------|-----|------|------|
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | | Yes | Yes | | Yes | Yes |
| Vehicle Extension (s) | 0.2 | 0.2 | | 0.2 | 0.2 | 0.2 | | 0.2 | 0.2 | | 0.2 | 0.2 |
| Minimum Gap (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time Before Reduce (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 |
| Time To Reduce (s) | 0.1 | 0.1 | | 0.1 | 0.1 | 0.1 | | 0.1 | 0.1 | | 0.1 | 0.1 |
| Recall Mode | None | None | | None | None | None | | None | Min | | None | None |
| Walk Time (s) | | 7.0 | | | | 7.0 | | | 7.0 | | | |
| Flash Dont Walk (s) | | 24.0 | | | | 24.0 | | | 15.0 | | | |
| Pedestrian Calls (#/hr) | | 1 | | | | 1 | | | 0 | | | |
| Act Effct Green (s) | 14.3 | 16.6 | | | 14.3 | 19.6 | | 13.0 | 30.8 | | | 13.0 |
| Actuated g/C Ratio | 0.27 | 0.31 | | | 0.27 | 0.36 | | 0.24 | 0.57 | | | 0.24 |
| v/c Ratio | 0.06 | 0.08 | | | 0.14 | 0.14 | | 0.09 | 0.32 | | | 0.10 |
| Control Delay | 29.9 | 9.7 | | | 29.1 | 8.7 | | 30.3 | 18.2 | | | 30.2 |
| Queue Delay | 0.0 | 0.0 | | | 0.0 | 0.0 | | 0.0 | 0.0 | | | 0.0 |
| Total Delay | 29.9 | 9.7 | | | 29.1 | 8.7 | | 30.3 | 18.2 | | | 30.2 |
| LOS | C | A | | | C | A | | C | B | | | C |
| Approach Delay | | 17.8 | | | | 18.1 | | | 18.8 | | | |
| Approach LOS | | B | | | | B | | | B | | | |

Intersection Summary

Area Type: Other
 Cycle Length: 103.4
 Actuated Cycle Length: 53.7
 Natural Cycle: 95
 Control Type: Actuated-Uncoordinated
 Maximum v/c Ratio: 0.36
 Intersection Signal Delay: 19.0
 Intersection LOS: B
 Intersection Capacity Utilization 48.3%
 ICU Level of Service A
 Analysis Period (min) 15

Splits and Phases: 4: SR 113 & Regency Pkwy/Industrial Wy



Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term Plus Project PM Peak Hour



| Lane Group | SBT | SBR |
|-------------------------|------|-----|
| Lead-Lag Optimize? | Yes | |
| Vehicle Extension (s) | 0.2 | |
| Minimum Gap (s) | 1.0 | |
| Time Before Reduce (s) | 1.0 | |
| Time To Reduce (s) | 0.1 | |
| Recall Mode | Min | |
| Walk Time (s) | 7.0 | |
| Flash Dont Walk (s) | 15.0 | |
| Pedestrian Calls (#/hr) | 4 | |
| Act Effct Green (s) | 30.8 | |
| Actuated g/C Ratio | 0.57 | |
| v/c Ratio | 0.36 | |
| Control Delay | 18.7 | |
| Queue Delay | 0.0 | |
| Total Delay | 18.7 | |
| LOS | B | |
| Approach Delay | 19.4 | |
| Approach LOS | B | |
| Intersection Summary | | |

Independence at Dixon TIA

1: SR 113/I-80 EB Ramps & I-80 WB Ramps/Auction Ln

Near-Term Plus Project PM Peak Hour

| Intersection | | | | | | | | | | | | |
|--------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Int Delay, s/veh | 3.2 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ↔ | ↔ | | ↔ | | ↔ | ↔ | | | ↔ | |
| Traffic Vol, veh/h | 6 | 0 | 550 | 2 | 0 | 1 | 315 | 515 | 2 | 1 | 248 | 16 |
| Future Vol, veh/h | 6 | 0 | 550 | 2 | 0 | 1 | 315 | 515 | 2 | 1 | 248 | 16 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | Free | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | 0 | - | - | - | 0 | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, % | 29 | 0 | 11 | 100 | 100 | 0 | 21 | 15 | 100 | 0 | 20 | 13 |
| Mvmt Flow | 6 | 0 | 591 | 2 | 0 | 1 | 339 | 554 | 2 | 1 | 267 | 17 |

| Major/Minor | Minor2 | | Minor1 | | Major1 | | Major2 | | | | | |
|----------------------|--------|------|--------|------|--------|-----|--------|---|---|------|---|---|
| Conflicting Flow All | 1512 | 1512 | - | 1511 | 1519 | 555 | 284 | 0 | 0 | 556 | 0 | 0 |
| Stage 1 | 278 | 278 | - | 1233 | 1233 | - | - | - | - | - | - | - |
| Stage 2 | 1234 | 1234 | - | 278 | 286 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.39 | 6.5 | - | 8.1 | 7.5 | 6.2 | 4.31 | - | - | 4.1 | - | - |
| Critical Hdwy Stg 1 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.39 | 5.5 | - | 7.1 | 6.5 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.761 | 4 | - | 4.4 | 4.9 | 3.3 | 2.389 | - | - | 2.2 | - | - |
| Pot Cap-1 Maneuver | 85 | 121 | 0 | 60 | 73 | 535 | 1177 | - | - | 1025 | - | - |
| Stage 1 | 673 | 684 | 0 | 139 | 164 | - | - | - | - | - | - | - |
| Stage 2 | 191 | 251 | 0 | 558 | 529 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | - | - | - |
| Mov Cap-1 Maneuver | 66 | 86 | - | 47 | 52 | 535 | 1177 | - | - | 1025 | - | - |
| Mov Cap-2 Maneuver | 66 | 86 | - | 47 | 52 | - | - | - | - | - | - | - |
| Stage 1 | 479 | 683 | - | 99 | 117 | - | - | - | - | - | - | - |
| Stage 2 | 136 | 179 | - | 557 | 528 | - | - | - | - | - | - | - |

| Approach | EB | | WB | | NB | | SB | |
|----------------------|------|--|------|--|-----|--|----|--|
| HCM Control Delay, s | 65.4 | | 60.6 | | 3.5 | | 0 | |
| HCM LOS | F | | F | | | | | |

| Minor Lane/Major Mvmt | NBL | NBT | NBR | EBLn1 | EBLn2 | WBLn1 | SBL | SBT | SBR |
|-----------------------|-------|-----|-----|-------|-------|-------|-------|-----|-----|
| Capacity (veh/h) | 1177 | - | - | 66 | - | 68 | 1025 | - | - |
| HCM Lane V/C Ratio | 0.288 | - | - | 0.098 | - | 0.047 | 0.001 | - | - |
| HCM Control Delay (s) | 9.3 | - | - | 65.4 | 0 | 60.6 | 8.5 | 0 | - |
| HCM Lane LOS | A | - | - | F | A | F | A | A | - |
| HCM 95th %tile Q(veh) | 1.2 | - | - | 0.3 | - | 0.1 | 0 | - | - |

Independence at Dixon TIA
 5: Project Dwy 1 & N. Lincoln St

Near-Term Plus Project PM Peak Hour

| Intersection | | | | | | |
|--------------------------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.3 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ↑↑ | | | ↑↑ | | ↑ |
| Traffic Vol, veh/h | 315 | 13 | 0 | 323 | 0 | 23 |
| Future Vol, veh/h | 315 | 13 | 0 | 323 | 0 | 23 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | - | 0 |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 342 | 14 | 0 | 351 | 0 | 25 |

| Major/Minor | Major1 | Major2 | Minor1 | | |
|----------------------|--------|--------|--------|---|------|
| Conflicting Flow All | 0 | 0 | - | - | 178 |
| Stage 1 | - | - | - | - | - |
| Stage 2 | - | - | - | - | - |
| Critical Hdwy | - | - | - | - | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - |
| Follow-up Hdwy | - | - | - | - | 3.32 |
| Pot Cap-1 Maneuver | - | - | 0 | - | 834 |
| Stage 1 | - | - | 0 | - | - |
| Stage 2 | - | - | 0 | - | - |
| Platoon blocked, % | - | - | - | - | - |
| Mov Cap-1 Maneuver | - | - | - | - | 834 |
| Mov Cap-2 Maneuver | - | - | - | - | - |
| Stage 1 | - | - | - | - | - |
| Stage 2 | - | - | - | - | - |

| Approach | EB | WB | NB |
|----------------------|----|----|-----|
| HCM Control Delay, s | 0 | 0 | 9.5 |
| HCM LOS | | | A |

| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBT |
|-----------------------|-------|-----|-----|-----|
| Capacity (veh/h) | 834 | - | - | - |
| HCM Lane V/C Ratio | 0.03 | - | - | - |
| HCM Control Delay (s) | 9.5 | - | - | - |
| HCM Lane LOS | A | - | - | - |
| HCM 95th %tile Q(veh) | 0.1 | - | - | - |

| Intersection | | | | | | |
|--------------------------|------|------|------|------|------|------|
| Int Delay, s/veh | 0.4 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | | | | | | |
| Traffic Vol, veh/h | 14 | 7 | 9 | 680 | 704 | 42 |
| Future Vol, veh/h | 14 | 7 | 9 | 680 | 704 | 42 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 100 | - | - | - |
| Veh in Median Storage, # | 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 15 | 8 | 10 | 739 | 765 | 46 |

| Major/Minor | Minor2 | Major1 | | Major2 | |
|----------------------|--------|--------|------|--------|---|
| Conflicting Flow All | 1178 | 406 | 811 | 0 | 0 |
| Stage 1 | 788 | - | - | - | - |
| Stage 2 | 390 | - | - | - | - |
| Critical Hdwy | 6.84 | 6.94 | 4.14 | - | - |
| Critical Hdwy Stg 1 | 5.84 | - | - | - | - |
| Critical Hdwy Stg 2 | 5.84 | - | - | - | - |
| Follow-up Hdwy | 3.52 | 3.32 | 2.22 | - | - |
| Pot Cap-1 Maneuver | 184 | 594 | 811 | - | - |
| Stage 1 | 409 | - | - | - | - |
| Stage 2 | 653 | - | - | - | - |
| Platoon blocked, % | | | | - | - |
| Mov Cap-1 Maneuver | 182 | 594 | 811 | - | - |
| Mov Cap-2 Maneuver | 182 | - | - | - | - |
| Stage 1 | 404 | - | - | - | - |
| Stage 2 | 653 | - | - | - | - |

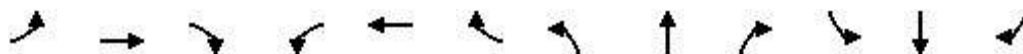
| Approach | EB | NB | SB |
|----------------------|------|-----|----|
| HCM Control Delay, s | 21.8 | 0.1 | 0 |
| HCM LOS | C | | |

| Minor Lane/Major Mvmt | NBL | NBT | EBLn1 | SBT | SBR |
|-----------------------|-------|-----|-------|-----|-----|
| Capacity (veh/h) | 811 | - | 237 | - | - |
| HCM Lane V/C Ratio | 0.012 | - | 0.096 | - | - |
| HCM Control Delay (s) | 9.5 | - | 21.8 | - | - |
| HCM Lane LOS | A | - | C | - | - |
| HCM 95th %tile Q(veh) | 0 | - | 0.3 | - | - |

Independence at Dixon TIA

2: SR 113 & Dorset Dr/E. Dorset Dr

Near-Term Plus Project PM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 138 | 11 | 91 | 267 | 19 | 145 | 135 | 583 | 199 | 178 | 453 | 136 |
| v/c Ratio | 0.27 | 0.03 | 0.23 | 0.36 | 0.05 | 0.35 | 0.47 | 0.84 | 0.40 | 0.33 | 0.63 | 0.32 |
| Control Delay | 34.3 | 26.0 | 7.8 | 32.8 | 25.8 | 7.4 | 39.8 | 41.5 | 7.0 | 34.6 | 32.5 | 7.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.3 | 26.0 | 7.8 | 32.8 | 25.8 | 7.4 | 39.8 | 41.5 | 7.0 | 34.6 | 32.5 | 7.8 |
| Queue Length 50th (ft) | 27 | 4 | 0 | 55 | 7 | 0 | 55 | 130 | 0 | 35 | 94 | 0 |
| Queue Length 95th (ft) | 81 | 19 | 36 | 140 | 26 | 43 | 161 | 264 | 56 | 100 | 207 | 49 |
| Internal Link Dist (ft) | | 520 | | | 616 | | | 607 | | | 887 | |
| Turn Bay Length (ft) | 150 | | 160 | 195 | | 195 | 200 | | 320 | 235 | | 135 |
| Base Capacity (vph) | 660 | 843 | 826 | 814 | 926 | 777 | 348 | 1355 | 786 | 619 | 1355 | 668 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.21 | 0.01 | 0.11 | 0.33 | 0.02 | 0.19 | 0.39 | 0.43 | 0.25 | 0.29 | 0.33 | 0.20 |

Intersection Summary

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project PM Peak Hour



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|-------------------------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 253 | 48 | 80 | 128 | 61 | 80 | 147 | 599 | 80 | 787 |
| v/c Ratio | 0.71 | 0.11 | 0.19 | 0.48 | 0.17 | 0.26 | 0.57 | 0.56 | 0.34 | 0.85 |
| Control Delay | 46.2 | 27.4 | 4.5 | 42.2 | 30.2 | 5.6 | 45.3 | 26.8 | 40.2 | 37.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 46.2 | 27.4 | 4.5 | 42.2 | 30.2 | 5.6 | 45.3 | 26.8 | 40.2 | 37.0 |
| Queue Length 50th (ft) | 113 | 19 | 0 | 57 | 26 | 0 | 67 | 127 | 35 | 171 |
| Queue Length 95th (ft) | #347 | 53 | 22 | 145 | 63 | 23 | 164 | 251 | 101 | #384 |
| Internal Link Dist (ft) | | 357 | | | 279 | | | 1083 | | 607 |
| Turn Bay Length (ft) | 275 | | | 180 | | 230 | 290 | | 285 | |
| Base Capacity (vph) | 358 | 825 | 700 | 343 | 825 | 578 | 351 | 1228 | 315 | 1235 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.71 | 0.06 | 0.11 | 0.37 | 0.07 | 0.14 | 0.42 | 0.49 | 0.25 | 0.64 |

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term Plus Project PM Peak Hour



| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
|-----------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 26 | 39 | 56 | 65 | 36 | 612 | 38 | 674 |
| v/c Ratio | 0.06 | 0.08 | 0.14 | 0.14 | 0.09 | 0.32 | 0.10 | 0.36 |
| Control Delay | 29.9 | 9.7 | 29.1 | 8.7 | 30.3 | 18.2 | 30.2 | 18.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 29.9 | 9.7 | 29.1 | 8.7 | 30.3 | 18.2 | 30.2 | 18.7 |
| Queue Length 50th (ft) | 7 | 1 | 14 | 1 | 9 | 81 | 10 | 91 |
| Queue Length 95th (ft) | 39 | 23 | 70 | 31 | 50 | 233 | 53 | 262 |
| Internal Link Dist (ft) | | 656 | | 824 | | 393 | | 1786 |
| Turn Bay Length (ft) | 150 | | 250 | | 115 | | 190 | |
| Base Capacity (vph) | 581 | 1041 | 535 | 821 | 614 | 2081 | 591 | 2019 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.04 | 0.04 | 0.10 | 0.08 | 0.06 | 0.29 | 0.06 | 0.33 |
| Intersection Summary | | | | | | | | |

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project AM Peak Hour - Improved



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|-------------------------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 260 | 62 | 49 | 62 | 33 | 55 | 119 | 572 | 82 | 510 |
| v/c Ratio | 0.61 | 0.13 | 0.11 | 0.60 | 0.08 | 0.15 | 0.40 | 0.70 | 0.29 | 0.60 |
| Control Delay | 36.3 | 24.9 | 0.6 | 61.5 | 28.5 | 0.9 | 38.9 | 30.4 | 36.3 | 27.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 36.3 | 24.9 | 0.6 | 61.5 | 28.5 | 0.9 | 38.9 | 30.4 | 36.3 | 27.3 |
| Queue Length 50th (ft) | 104 | 22 | 0 | 25 | 12 | 0 | 48 | 116 | 32 | 100 |
| Queue Length 95th (ft) | #268 | 58 | 2 | #127 | 42 | 0 | #152 | 222 | 100 | 194 |
| Internal Link Dist (ft) | | 357 | | | 279 | | | 1083 | | 607 |
| Turn Bay Length (ft) | 275 | | | 180 | | 230 | 290 | | 285 | |
| Base Capacity (vph) | 603 | 1186 | 960 | 104 | 1025 | 709 | 305 | 1540 | 283 | 1599 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.43 | 0.05 | 0.05 | 0.60 | 0.03 | 0.08 | 0.39 | 0.37 | 0.29 | 0.32 |

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Independence at Dixon TIA
 3: SR 113 & N. Lincoln St/Vaughn Rd

Near-Term Plus Project PM Peak Hour - Improved



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|-------------------------|------|------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 253 | 48 | 80 | 128 | 61 | 80 | 147 | 599 | 80 | 787 |
| v/c Ratio | 0.70 | 0.11 | 0.19 | 0.47 | 0.18 | 0.24 | 0.59 | 0.55 | 0.33 | 0.84 |
| Control Delay | 42.6 | 26.1 | 4.8 | 42.3 | 32.0 | 2.6 | 47.9 | 26.4 | 39.9 | 35.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 42.6 | 26.1 | 4.8 | 42.3 | 32.0 | 2.6 | 47.9 | 26.4 | 39.9 | 35.0 |
| Queue Length 50th (ft) | 114 | 19 | 0 | 57 | 26 | 0 | 67 | 128 | 35 | 174 |
| Queue Length 95th (ft) | #264 | 49 | 23 | #154 | 66 | 7 | #208 | 236 | 99 | 315 |
| Internal Link Dist (ft) | | 357 | | | 279 | | | 1083 | | 607 |
| Turn Bay Length (ft) | 275 | | | 180 | | 230 | 290 | | 285 | |
| Base Capacity (vph) | 507 | 1080 | 883 | 295 | 864 | 618 | 252 | 1348 | 242 | 1398 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.50 | 0.04 | 0.09 | 0.43 | 0.07 | 0.13 | 0.58 | 0.44 | 0.33 | 0.56 |

Intersection Summary

95th percentile volume exceeds capacity, queue may be longer.
 Queue shown is maximum after two cycles.

Independence at Dixon TIA
 4: SR 113 & Regency Pkwy/Industrial Wy

Near-Term Plus Project PM Peak Hour - Improved



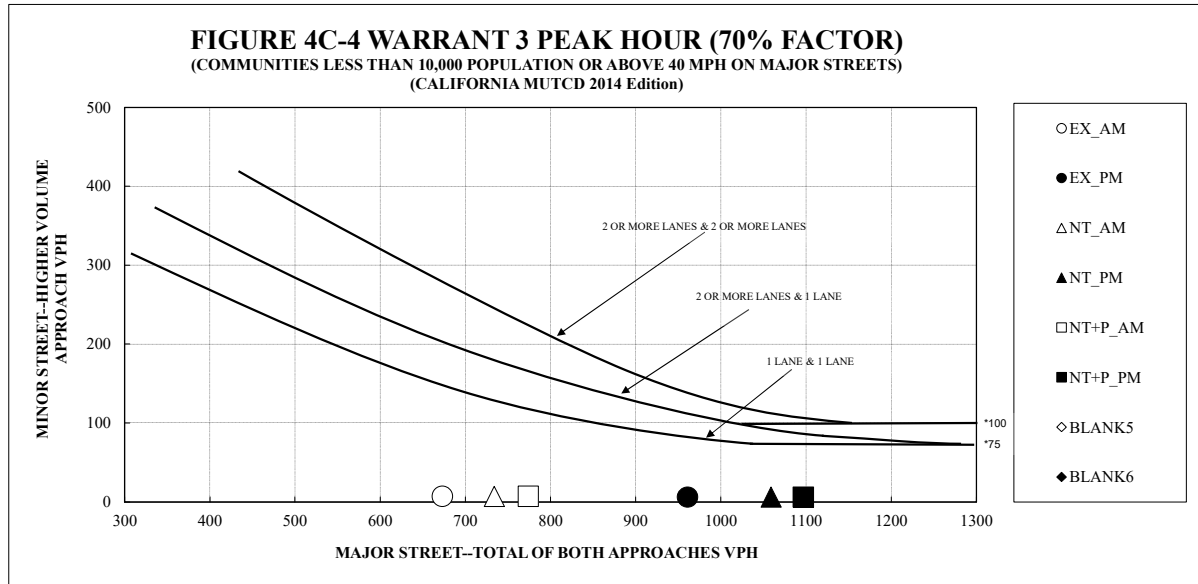
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
|-----------------------------|------|------|------|------|------|------|------|------|
| Lane Group Flow (vph) | 26 | 39 | 56 | 65 | 36 | 612 | 38 | 674 |
| v/c Ratio | 0.06 | 0.08 | 0.14 | 0.14 | 0.09 | 0.32 | 0.10 | 0.36 |
| Control Delay | 30.6 | 10.0 | 29.6 | 9.0 | 30.8 | 17.9 | 30.8 | 18.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 30.6 | 10.0 | 29.6 | 9.0 | 30.8 | 17.9 | 30.8 | 18.4 |
| Queue Length 50th (ft) | 6 | 1 | 14 | 1 | 9 | 81 | 10 | 91 |
| Queue Length 95th (ft) | 41 | 24 | 72 | 33 | 52 | 232 | 54 | 260 |
| Internal Link Dist (ft) | | 656 | | 824 | | 393 | | 1786 |
| Turn Bay Length (ft) | 150 | | 250 | | 115 | | 190 | |
| Base Capacity (vph) | 437 | 1045 | 404 | 824 | 422 | 2325 | 406 | 2256 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.06 | 0.04 | 0.14 | 0.08 | 0.09 | 0.26 | 0.09 | 0.30 |
| Intersection Summary | | | | | | | | |

Appendix C

Signal Warrant Worksheets

CA SIGNAL WARRANT 3 ANALYSIS

SCENARIOS: "AM/PM PEAK HOUR" CONDITIONS



Note: 100 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

| SCENARIO | APPROACH(ES) | | WARRANT MET? |
|----------|--------------|-------|--------------|
| | MAJOR | MINOR | |
| EX_AM | 673 | 7 | NO |
| EX_PM | 961 | 6 | NO |
| NT_AM | 734 | 7 | NO |
| NT_PM | 1059 | 6 | NO |
| NT+P_AM | 774 | 7 | NO |
| NT+P_PM | 1097 | 6 | NO |
| BLANK5 | 0 | 0 | |
| BLANK6 | 0 | 0 | |

Note: Major approach is the total of both approaches. Minor approach is the highest of both approaches.

Date: May 12, 2023 Intersection No.: **1**

Intersection: SR 113 & I-80 Ramps/Auction Ln

Number of lanes on MAJOR street: **1**

Number of lanes on MINOR street: **1**

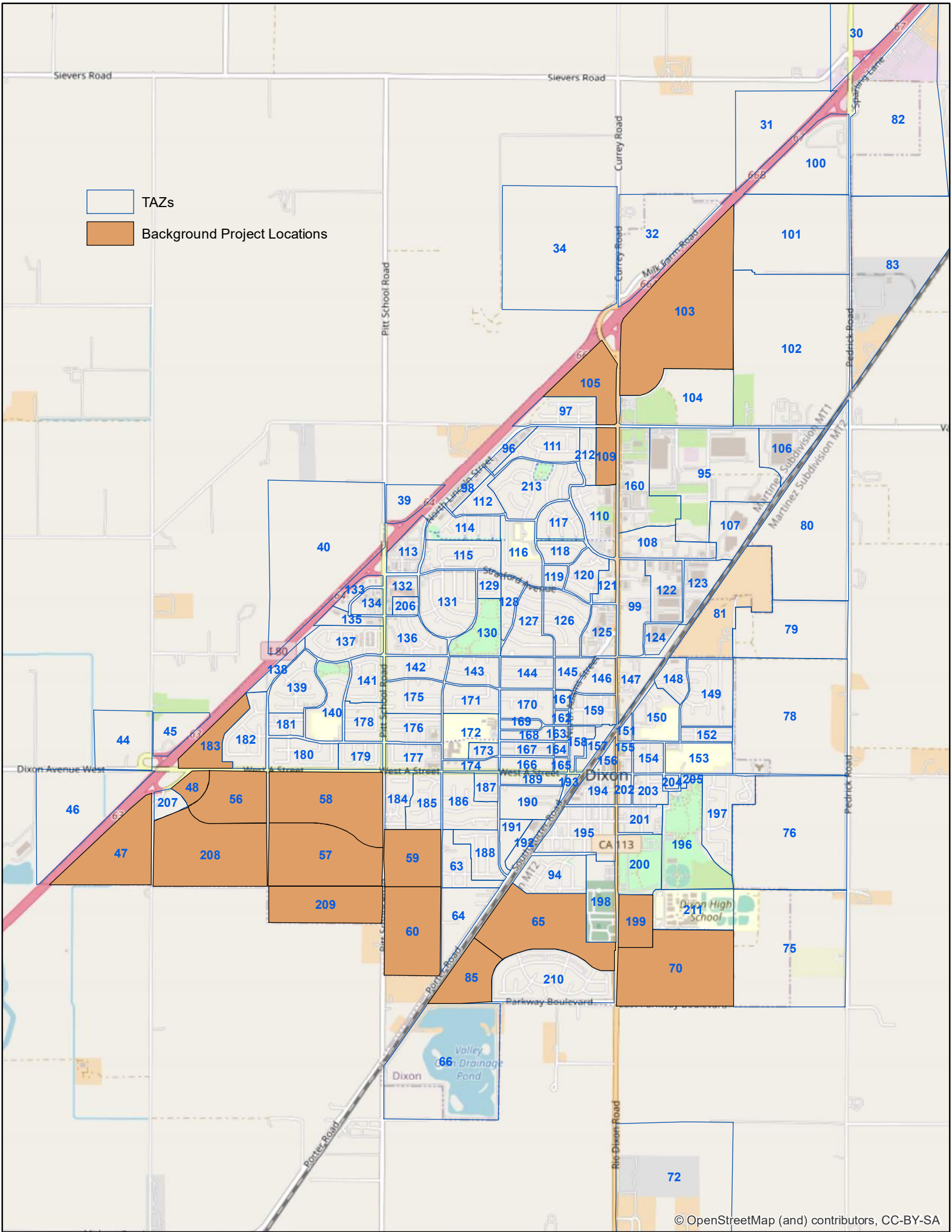


Appendix D

Background Projects Map

TAZs

Background Project Locations



Appendix E

Project Sight Distance Exhibits

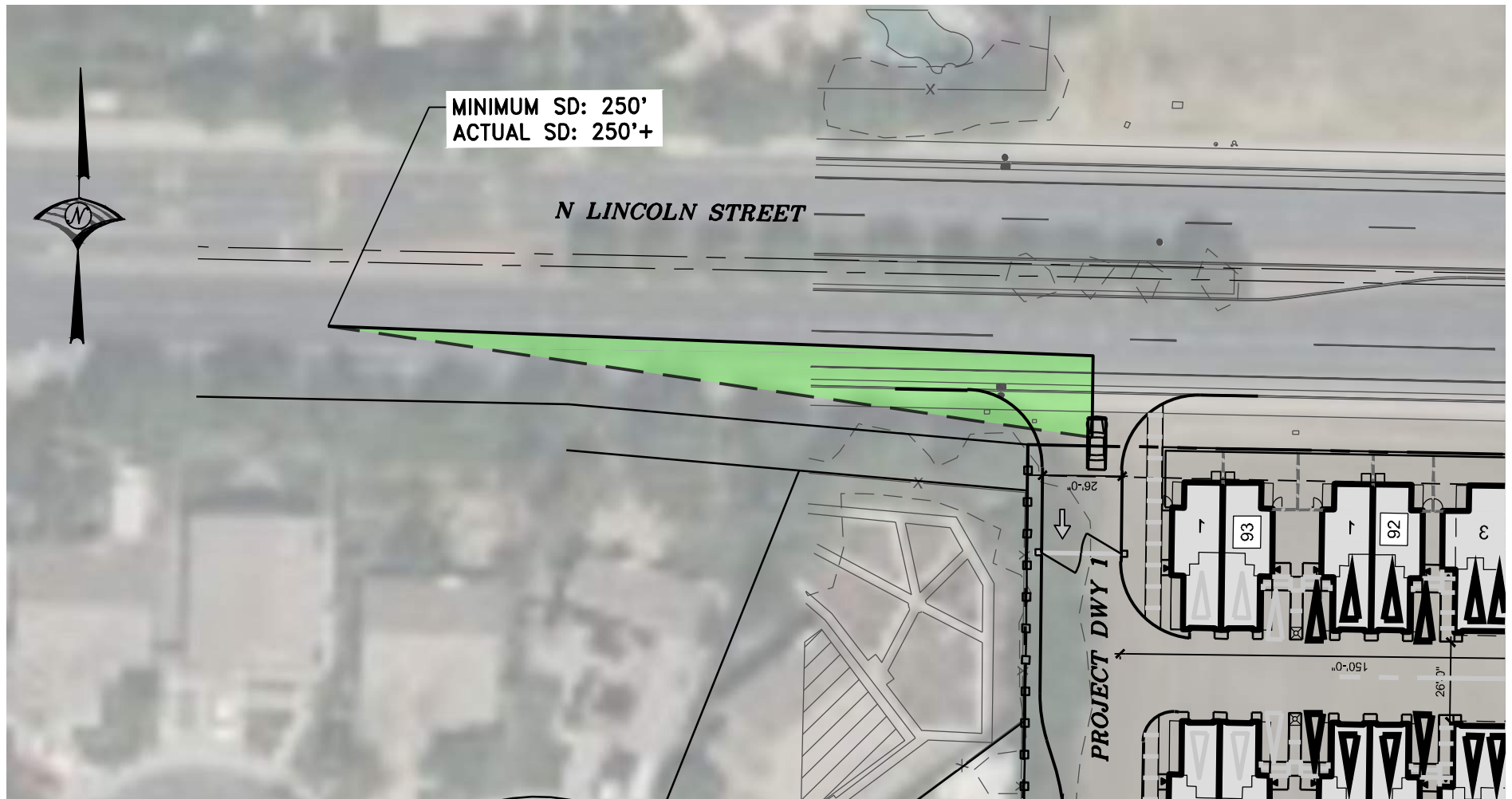
INDEPENDENCE AT DIXON

SIGHT DISTANCE - PROJECT DRIVEWAY 1 & N LINCOLN ST

DIXON

CALIFORNIA

MAY, 2023



50' 25' 0 50'



SCALE: 1" = 50'

LEGEND

- VISIBLE AREA 
- LINE OF SIGHT 



WOOD RODGERS
BUILDING RELATIONSHIPS ONE PROJECT AT A TIME
3301 C ST, BLDG. 100-B TEL 916.341.7760
SACRAMENTO, CA 95816 FAX 916.341.7767

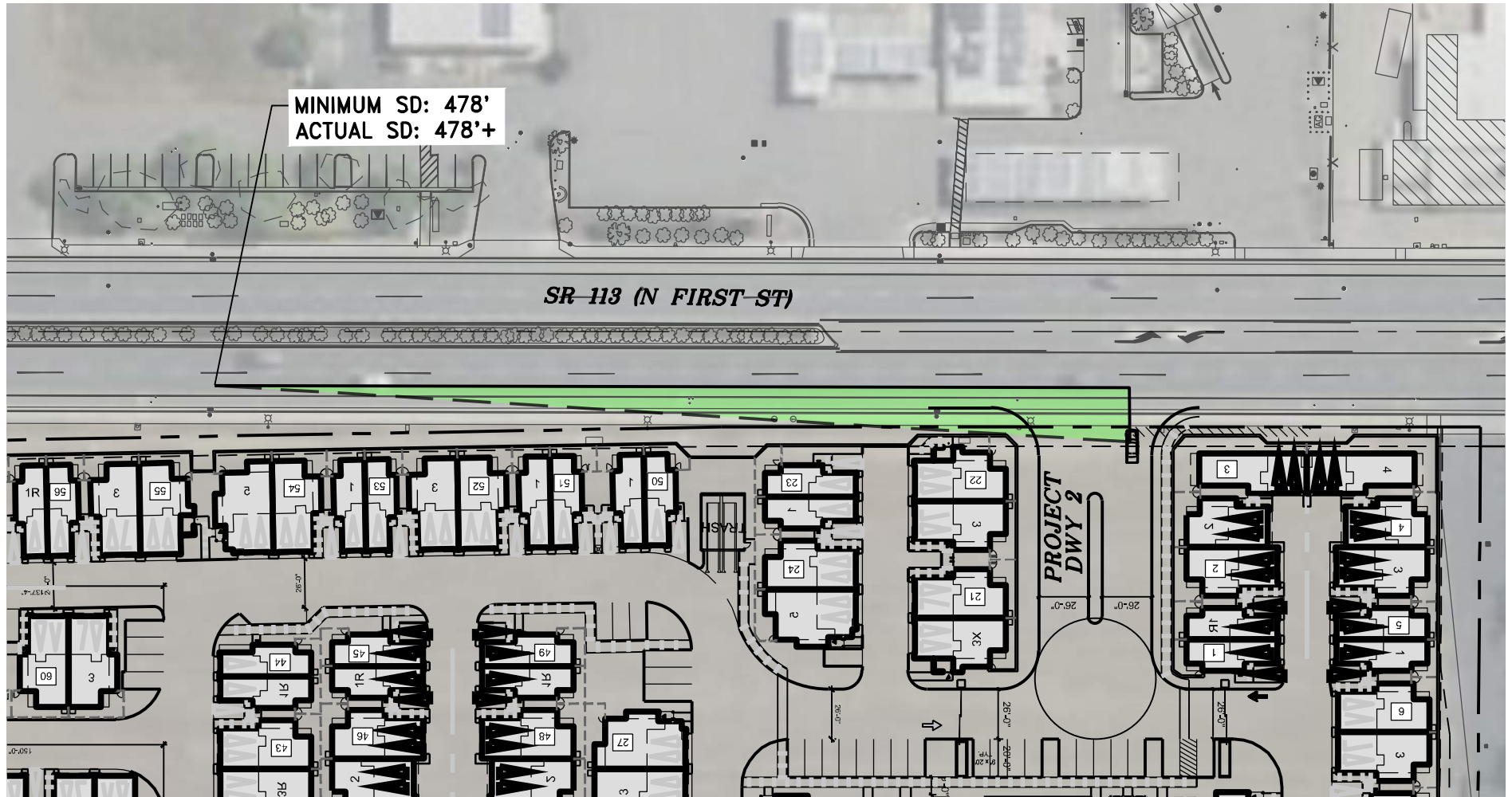
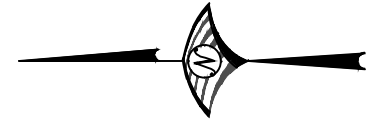
INDEPENDENCE AT DIXON

SIGHT DISTANCE - SR 113 & PROJECT DRIVEWAY 2

DIXON

CALIFORNIA

MAY, 2023



MINIMUM SD: 478'
ACTUAL SD: 478'+

SR 113 (N FIRST-ST)

PROJECT DWY 2



SCALE: 1" = 80'

LEGEND

- VISIBLE AREA
- LINE OF SIGHT

WOOD RODGERS
 BUILDING RELATIONSHIPS ONE PROJECT AT A TIME
 3301 C ST, BLDG. 100-B TEL 916.341.7760
 SACRAMENTO, CA 95816 FAX 916.341.7767

woodrogers.ca \ProductionData\Jobs-Plan\Jobs\3735_Durfee_Dixon\008_Durfee_Dixon_Traffic_Impact_Analysis\Traffic\Exhibits\Independence_Proj_Dwy_Sigh_Dist.dwg 5/17/2023 4:16 PM Nicole Scopitacci

Appendix F

SWITRS Collision History

| CASE_ID | ACCIDENT_YEAR | PROC_DATE | JURIS | COLLISION_DATE | COLLISION_TIME | OFFICER_ID | REPORTING_DISTRICT | DAY_OF_WEEK | CHP_SHIFT | POPULATION | |
|---------|---------------|-----------|-------|----------------|----------------|------------|--------------------|-------------|-----------|------------|---|
| 8688096 | 2018 | 20181018 | 4802 | 20180327 | 1915 | 1264 | | | 2 | 5 | 3 |
| 8709544 | 2018 | 20181029 | 4802 | 20180327 | 729 | 1259 | | | 2 | 5 | 3 |
| 8829121 | 2019 | 20190416 | 4802 | 20190308 | 1329 | 1211 | 4802 | | 5 | 5 | 3 |
| 8831759 | 2019 | 20200527 | 4802 | 20190107 | 1800 | 1281 SOLAN | | | 1 | 5 | 3 |
| 8860699 | 2018 | 20190624 | 4802 | 20181106 | 644 | 1229 | | | 2 | 5 | 3 |
| 9125926 | 2019 | 20200812 | 4802 | 20190821 | 1850 | 1291 | 4802 | | 3 | 5 | 3 |
| 9125932 | 2019 | 20200812 | 4802 | 20190916 | 2100 | 1261 FAIRF | | | 1 | 5 | 3 |
| 9125950 | 2019 | 20200820 | 4802 | 20190727 | 1630 | 1170 DIXON | | | 6 | 5 | 3 |
| 9125964 | 2019 | 20200923 | 4802 | 20191113 | 1930 | 1291 | | | 3 | 5 | 3 |
| 9130291 | 2019 | 20200923 | 4802 | 20190826 | 1313 | 1260 | | | 1 | 5 | 3 |
| 9132848 | 2020 | 20200826 | 4802 | 20200129 | 1830 | 1261 FAIRF | | | 3 | 5 | 3 |
| 9132864 | 2020 | 20200826 | 4802 | 20200302 | 1305 | 1276 | 4802 | | 1 | 5 | 3 |
| 9136495 | 2020 | 20200901 | 4802 | 20200403 | 1215 | 1302 | | | 5 | 5 | 3 |
| 9141971 | 2019 | 20200923 | 4802 | 20191130 | 1856 | 1276 | | | 6 | 5 | 3 |
| 9142225 | 2020 | 20201009 | 4802 | 20200610 | 1436 | 1291 | | | 3 | 5 | 3 |
| 9143242 | 2020 | 20200915 | 4802 | 20200225 | 1136 | 1229 | | | 2 | 5 | 3 |
| 9149463 | 2020 | 20201009 | 4802 | 20200621 | 1429 | 1315 | 4802 | | 7 | 5 | 3 |
| 9180024 | 2020 | 20201203 | 4802 | 20201019 | 1741 | 1258 | | | 1 | 5 | 3 |
| 9180025 | 2020 | 20201203 | 4802 | 20201002 | 750 | 1264 | 4802 | | 5 | 5 | 3 |
| 9192582 | 2020 | 20210127 | 4802 | 20201204 | 2020 | 1260 | | | 5 | 5 | 3 |
| 9225546 | 2020 | 20210304 | 4802 | 20201226 | 2222 | 1290 | | | 6 | 5 | 3 |
| 9267368 | 2021 | 20210616 | 4802 | 20210522 | 1742 | 1290 | | | 6 | 5 | 3 |
| 9276968 | 2021 | 20210608 | 4802 | 20210330 | 2310 | 1288 | 4802 | | 2 | 5 | 3 |
| 9276969 | 2021 | 20210608 | 4802 | 20210331 | 1701 | 1262 | | | 3 | 5 | 3 |
| 9303957 | 2021 | 20210913 | 4802 | 20210720 | 1147 | 1314 | | | 2 | 5 | 3 |
| 9312274 | 2021 | 20210913 | 4802 | 20210808 | 2122 | 1320 | 4802 | | 7 | 5 | 3 |
| 9386369 | 2021 | 20220112 | 4802 | 20211207 | 1609 | 1318 | 4802 | | 2 | 5 | 3 |
| 9386673 | 2021 | 20220105 | 4802 | 20211223 | 1849 | 1314 | | | 4 | 5 | 3 |
| 9409641 | 2022 | 20220315 | 4802 | 20220221 | 617 | 1260 | | | 1 | 5 | 3 |
| 9409645 | 2022 | 20220315 | 4802 | 20220208 | 2128 | 1290 | 4802 | | 2 | 5 | 3 |
| 9410138 | 2022 | 20220429 | 4802 | 20220129 | 1231 | 1291 FAIRF | | | 6 | 5 | 3 |
| 9414198 | 2022 | 20220318 | 4802 | 20220129 | 1230 | 1291 FAIRF | | | 6 | 5 | 3 |
| 9419821 | 2022 | 20220421 | 4802 | 20220313 | 906 | 1276 | | | 7 | 5 | 3 |
| 9419822 | 2022 | 20220421 | 4802 | 20220304 | 1434 | 1259 SOLAN | | | 5 | 5 | 3 |
| 9419830 | 2022 | 20220421 | 4802 | 20220311 | 931 | 1259 SOLAN | | | 5 | 5 | 3 |
| 9436946 | 2022 | 20220516 | 4802 | 20220418 | 1230 | 1260 | | | 1 | 5 | 3 |
| 9458212 | 2022 | 20220614 | 4802 | 20220416 | 1513 | 1291 FAIRF | | | 6 | 5 | 3 |
| 9479139 | 2022 | 20220819 | 4802 | 20220722 | 1949 | 1314 | | | 5 | 5 | 3 |
| 9479140 | 2022 | 20220817 | 4802 | 20220616 | 1609 | 1321 SOLAN | | | 4 | 5 | 3 |
| 9493257 | 2022 | 20220923 | 4802 | 20220824 | 1352 | 1290 | | | 3 | 5 | 3 |
| 9504959 | 2022 | 20221103 | 4802 | 20221020 | 1609 | 1299 FAIRF | | | 4 | 5 | 3 |
| 9533172 | 2022 | 20230119 | 4802 | 20221121 | 1638 | 1288 | 4802 | | 1 | 5 | 3 |
| 9535325 | 2022 | 20230211 | 4802 | 20221231 | 1715 | 1299 | | | 6 | 5 | 3 |
| 9546096 | 2022 | 20230209 | 4802 | 20221221 | 825 | 1277 | | | 3 | 5 | 3 |
| 9546100 | 2022 | 20230209 | 4802 | 20221206 | 1047 | 1260 | | | 2 | 5 | 3 |

| CASE_ID | CNTY_CITY_LOC | SPECIAL_COND | BEAT_TYPE | CHP_BEAT_TYPE | CITY_DIVISION_LAPD | CHP_BEAT_CLASS | BEAT_NUMBER | PRIMARY_RD | SECONDARY_RD |
|---------|---------------|--------------|-----------|---------------|--------------------|----------------|-------------|--------------------|------------------|
| 8688096 | 4802 | 0 | 0 | 0 | | 0 | 0 | 2 N 1ST ST | E DORSET DR |
| 8709544 | 4802 | 0 | 0 | 0 | | 0 | 0 | 2 N 1ST ST | RT 113 S |
| 8829121 | 4802 | 0 | 0 | 0 | | 0 | | NORTH 1ST ST | NORTH LINCOLN ST |
| 8831759 | 4802 | 0 | 0 | 0 | | 0 | 0 | 2 RT 113 | DORSET DR |
| 8860699 | 4802 | 0 | 0 | 0 | | 0 | 0 | DOREST DR | N 1ST ST |
| 9125926 | 4802 | 0 | 0 | 0 | | 0 | 0 | 2 NORTH 1ST ST | VAUGH RD |
| 9125932 | 4802 | 0 | 0 | 0 | | 0 | 0 | 2 NORTH 1ST ST | DORSET DR |
| 9125950 | 4802 | 0 | 0 | 0 | | 0 | 0 | 2 DORSET DR | N FIRST ST |
| 9125964 | 4802 | 0 | 0 | 0 | | 0 | 0 | 2 DORSET DR | N 1ST ST |
| 9130291 | 4802 | 0 | 0 | 0 | | 0 | 0 | VAUGHN RD | RT 113 S |
| 9132848 | 4802 | 0 | 0 | 0 | | 0 | 0 | 2 RT 113 | N 1ST ST |
| 9132864 | 4802 | 0 | 0 | 0 | | 0 | 0 | 32 N 1ST ST | VAUGHN RD |
| 9136495 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 N 1ST ST | N LINCOLN ST |
| 9141971 | 4802 | 0 | 0 | 0 | | 0 | 0 | NORTH 1ST ST | NORTH LINCOLN ST |
| 9142225 | 4802 | 0 | 0 | 0 | | 0 | 0 | N 1ST ST | DORSET DR |
| 9143242 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 NORTH LINCOLN ST | REGENCY PKWY |
| 9149463 | 4802 | 0 | 0 | 0 | | 0 DP2 | 0 | N 1ST ST | REGENCY PKWY |
| 9180024 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 N 1ST ST | N LINCOLN ST |
| 9180025 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 N 1ST ST | DORSET DR |
| 9192582 | 4802 | 0 | 0 | 0 | | 0 | 0 | N 1ST ST | E DORSET DR |
| 9225546 | 4802 | 0 | 0 | 0 | | 0 | 0 | N 1ST ST | N LINCOLN ST |
| 9267368 | 4802 | 0 | 0 | 0 | | 0 | 0 | N 1ST ST | VAUGHN RD |
| 9276968 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 NORTH LINCOLN ST | REGENCY PKWY |
| 9276969 | 4802 | 0 | 0 | 0 | | 0 | 0 | N LINCOLN ST | REGENCY PKWY |
| 9303957 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 NORTH 1ST ST | DORSET DR |
| 9312274 | 4802 | 0 | 0 | 0 | | 0 DP3 | 0 | N 1ST ST | INDUSTRIAL WY |
| 9386369 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 RT 113 | AUCTION LN |
| 9386673 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 NORTH 1ST ST | E DORSET DR |
| 9409641 | 4802 | 0 | 0 | 0 | | 0 | 0 | RT 113 | AUCTION LN |
| 9409645 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 N 1ST ST | VAUGHN RD |
| 9410138 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 VAUGHIN RD | N 1ST ST |
| 9414198 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 N 1ST ST | VAUGHN RD |
| 9419821 | 4802 | 0 | 0 | 0 | | 0 DP3 | 0 | RT 113 | E DORSET DR |
| 9419822 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 N 1ST ST | AUCTION LN |
| 9419830 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 N 1ST ST | AUCTION LN |
| 9436946 | 4802 | 0 | 0 | 0 | | 0 | 0 | N LINCOLN ST | N 1ST ST |
| 9458212 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 DORSET DR | NORTH 1ST ST |
| 9479139 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 N 1ST ST | E DORSET DR |
| 9479140 | 4802 | 0 | 0 | 0 | | 0 | 0 | 1 N 1ST ST | E DORSET DR |
| 9493257 | 4802 | 0 | 0 | 0 | | 0 | 0 | VAUGHN RD | N LINCOLN ST |
| 9504959 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 NORTH 1ST ST | DORSET DR |
| 9533172 | 4802 | 0 | 0 | 0 | | 0 | 0 | 2 N LINCOLN ST | LINCOLN CT |
| 9535325 | 4802 | 0 | 0 | 0 | | 0 | 0 | 3 N LINCOLN ST | REGENCY PKWY |
| 9546096 | 4802 | 0 | 0 | 0 | | 0 | 0 | N 1ST ST | AUCTION LN |
| 9546100 | 4802 | 0 | 0 | 0 | | 0 | 0 | N 1ST ST | AUCTION LN |

| CASE_ID | DISTANCE | DIRECTION | INTERSECTION | WEATHER_1 | WEATHER_2 | STATE_HWY_IND | CALTRANS_COUNTY | CALTRANS_DISTRICT | STATE_ROUTE | ROUTE_SUFFIX |
|---------|----------|-----------|--------------|-----------|-----------|---------------|-----------------|-------------------|-------------|--------------|
| 8688096 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |
| 8709544 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |
| 8829121 | 0 | | Y | B | - | N | | | | |
| 8831759 | 300 S | | N | A | - | Y | SOL | | 4 | 113 - |
| 8860699 | 157 E | | N | A | - | N | | | | |
| 9125926 | 0 | | Y | A | - | | | | | |
| 9125932 | 0 | | Y | A | - | | | | | |
| 9125950 | 120 E | | N | A | - | | | | | |
| 9125964 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |
| 9130291 | 40 E | | N | A | - | Y | SOL | | 4 | 113 - |
| 9132848 | 827 W | | N | A | - | Y | SOL | | 4 | 80 - |
| 9132864 | 200 N | | N | A | G | Y | SOL | | 4 | 113 - |
| 9136495 | 24 N | | N | A | - | Y | SOL | | 4 | 113 - |
| 9141971 | 185 N | | N | C | - | Y | SOL | | 4 | 113 - |
| 9142225 | 66 N | | N | A | - | Y | SOL | | 4 | 113 - |
| 9143242 | 0 | | Y | A | - | N | | | | |
| 9149463 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |
| 9180024 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |
| 9180025 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |
| 9192582 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |
| 9225546 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |
| 9267368 | 0 | | Y | A | - | N | | | | |
| 9276968 | 246 W | | N | A | G | | | | | |
| 9276969 | 0 | | Y | A | - | | | | | |
| 9303957 | 45 S | | N | A | - | N | | | | |
| 9312274 | 238 S | | N | A | - | Y | SOL | | 4 | 113 - |
| 9386369 | 58 W | | N | A | - | Y | SOL | | 4 | 113 - |
| 9386673 | 284 N | | N | B | - | N | | | | |
| 9409641 | 500 W | | N | A | - | Y | SOL | | 4 | 113 - |
| 9409645 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |
| 9410138 | 184 E | | N | A | - | N | | | | |
| 9414198 | 43 N | | N | A | - | Y | SOL | | 4 | 113 - |
| 9419821 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |
| 9419822 | 9 S | | N | A | - | Y | SOL | | 4 | 113 - |
| 9419830 | 240 N | | N | A | - | Y | SOL | | 4 | 80 - |
| 9436946 | 20 W | | N | A | - | N | | | | |
| 9458212 | 0 | | Y | A | - | N | | | | |
| 9479139 | 71 E | | N | A | - | N | | | | |
| 9479140 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |
| 9493257 | 247 E | | N | A | - | Y | SOL | | 4 | 113 - |
| 9504959 | 48 S | | N | A | - | N | | | | |
| 9533172 | 137 W | | N | A | - | N | | | | |
| 9535325 | 0 | | Y | B | C | | | | | |
| 9546096 | 0 | | Y | E | - | Y | SOL | | 4 | 113 - |
| 9546100 | 0 | | Y | A | - | Y | SOL | | 4 | 113 - |

| CASE_ID | POSTMILE_PREFIX | POSTMILE | LOCATION_TYPE | RAMP_INTERSECTION | SIDE_OF_HWY | TOW_AWAY | COLLISION_SEVERITY | NUMBER_KILLED | NUMBER_INJURED |
|---------|-----------------|----------|---------------|-------------------|-------------|----------|--------------------|---------------|----------------|
| 8688096 | - | 20.93 | H | - | N | N | | 0 | 0 |
| 8709544 | - | 19.64 | H | - | S | N | | 0 | 0 |
| 8829121 | | | | | | | | 0 | 0 |
| 8831759 | - | 20.87 | H | - | S | N | | 0 | 0 |
| 8860699 | | | | | | N | | 0 | 0 |
| 9125926 | | | | | | | | 0 | 0 |
| 9125932 | | | | | | | | 0 | 0 |
| 9125950 | | | | | | | | 0 | 0 |
| 9125964 | - | 20.944 | I | | 5 S | | | 0 | 0 |
| 9130291 | - | 20.8 | I | | 6 N | | | 0 | 0 |
| 9132848 | - | 38.437 | R | | 4 W | Y | | 0 | 0 |
| 9132864 | - | 20.84 | H | - | N | N | | 0 | 0 |
| 9136495 | - | 20.832 | H | - | S | Y | | 0 | 0 |
| 9141971 | - | 20.85 | H | - | S | | | 0 | 0 |
| 9142225 | - | 20.95 | H | - | N | Y | | 0 | 0 |
| 9143242 | | | | | | | | 0 | 0 |
| 9149463 | - | 20.23 | H | - | S | N | | 0 | 0 |
| 9180024 | - | 20.8 | I | | 5 S | N | | 0 | 0 |
| 9180025 | - | 20.87 | H | - | N | Y | | 0 | 0 |
| 9192582 | - | 20.944 | I | | 5 N | N | | 0 | 0 |
| 9225546 | - | 20.8 | I | | 5 S | Y | 4 | 0 | 1 |
| 9267368 | | | | | | N | | 0 | 0 |
| 9276968 | | | | | | | | 0 | 0 |
| 9276969 | | | | | | | | 0 | 0 |
| 9303957 | | | | | | Y | | 0 | 0 |
| 9312274 | - | 20.17 | H | - | N | Y | | 0 | 0 |
| 9386369 | - | 21.12 | I | | 5 S | Y | 4 | 0 | 2 |
| 9386673 | | | | | | N | | 0 | 0 |
| 9409641 | - | 21.23 | H | - | S | N | | 0 | 0 |
| 9409645 | - | 20.86 | H | - | S | N | | 0 | 0 |
| 9410138 | | | | | | N | | 0 | 0 |
| 9414198 | - | 20.81 | H | - | S | | | 0 | 0 |
| 9419821 | - | 20.944 | I | | 5 N | N | | 0 | 0 |
| 9419822 | - | 21.12 | I | | 5 N | Y | 4 | 0 | 1 |
| 9419830 | - | 38.18 | R | | 2 E | N | | 0 | 0 |
| 9436946 | | | | | | N | | 0 | 0 |
| 9458212 | | | | | | | 4 | 0 | 3 |
| 9479139 | | | | | | N | 4 | 0 | 4 |
| 9479140 | - | 20.944 | I | | 5 S | Y | 4 | 0 | 1 |
| 9493257 | - | 20.8 | I | | 6 N | N | | 0 | 0 |
| 9504959 | | | | | | N | | 0 | 0 |
| 9533172 | | | | | | N | | 0 | 0 |
| 9535325 | | | | | | | | 0 | 0 |
| 9546096 | - | 21.12 | I | | 5 N | | | 0 | 0 |
| 9546100 | - | 21.12 | I | | 5 S | | | 0 | 0 |

| CASE_ID | PARTY_COUNT | PRIMARY_COLL_FACTOR | PCF_CODE_OF_VIOL | PCF_VIOL_CATEGORY | PCF_VIOLATION | PCF_VIOL_SUBSECTION | HIT_AND_RUN | TYPE_OF_COLLISION |
|---------|-------------|---------------------|------------------|-------------------|---------------|---------------------|-------------|-------------------|
| 8688096 | 2 | A | - | | 3 | 22350 | N | C |
| 8709544 | 2 | A | - | | 3 | 22350 | N | C |
| 8829121 | 2 | A | - | | 8 | 22107 | N | B |
| 8831759 | 3 | A | - | | 3 | 22350 | N | C |
| 8860699 | 1 | A | - | | 3 | 22350 | N | E |
| 9125926 | 2 | A | - | | 3 | 22350 | N | C |
| 9125932 | 2 | A | - | | 9 | 21804 A | N | B |
| 9125950 | 2 | A | - | | 9 | 21804 A | N | D |
| 9125964 | 2 | A | - | | 12 | 21453 A | M | B |
| 9130291 | 2 | A | - | | 3 | 22350 | N | C |
| 9132848 | 2 | A | - | | 5 | 21650 | N | A |
| 9132864 | 2 | A | - | | 3 | 22350 | N | C |
| 9136495 | 2 | A | - | | 4 | 21703 | N | C |
| 9141971 | 2 | A | - | | 1 | 23152 A | N | C |
| 9142225 | 2 | A | - | | 8 | 22107 | N | C |
| 9143242 | 2 | A | - | | 8 | 22107 | M | C |
| 9149463 | 2 | A | - | | 3 | 22350 | N | C |
| 9180024 | 2 | A | - | | 12 | 21453 A | N | B |
| 9180025 | 2 | A | - | | 6 | 21750 A | N | B |
| 9192582 | 2 | A | - | | 9 | 21453 C | N | D |
| 9225546 | 2 | A | - | | 9 | 21453 C | N | A |
| 9267368 | 2 | A | - | | 8 | 22107 | N | B |
| 9276968 | 1 | D | - | | 0 | | N | B |
| 9276969 | 2 | A | - | | 9 | 21802 A | N | D |
| 9303957 | 2 | A | - | | 12 | 21453 A | N | D |
| 9312274 | 1 | A | - | | 1 | 23152 A | N | E |
| 9386369 | 2 | A | - | | 9 | 21801 A | N | A |
| 9386673 | 2 | A | - | | 8 | 22107 | M | B |
| 9409641 | 1 | A | - | | 3 | 22350 | N | E |
| 9409645 | 2 | D | - | | 0 | | N | C |
| 9410138 | 2 | A | - | | 5 | 21650 | N | A |
| 9414198 | 2 | A | - | | 3 | 22350 | N | C |
| 9419821 | 1 | A | - | | 8 | 22107 | N | E |
| 9419822 | 2 | A | - | | 9 | 21801 A | N | D |
| 9419830 | 2 | A | - | | 9 | 21801 A | N | D |
| 9436946 | 2 | A | - | | 21 | 22106 | N | H |
| 9458212 | 2 | B | - | | 22 | | N | D |
| 9479139 | 2 | A | - | | 3 | 22350 | N | C |
| 9479140 | 2 | A | - | | 9 | 21453 C | N | A |
| 9493257 | 2 | A | - | | 8 | 22107 | N | D |
| 9504959 | 2 | A | - | | 3 | 22350 | N | C |
| 9533172 | 2 | A | - | | 1 | 23152 A | N | A |
| 9535325 | 2 | A | - | | 8 | 22107 | M | D |
| 9546096 | 2 | A | - | | 9 | 21802 A | N | - |
| 9546100 | 2 | A | - | | 8 | 22107 | N | A |

| CASE_ID | MVIW | PED_ACTION | ROAD_SURFACE | ROAD_COND_1 | ROAD_COND_2 | LIGHTING | CONTROL_DEVICE | CHP_ROAD_TYPE | PEDESTRIAN_ACCIDENT |
|---------|------|------------|--------------|-------------|-------------|----------|----------------|---------------|---------------------|
| 8688096 | C | A | A | H | - | B | A | | 0 |
| 8709544 | C | A | A | - | - | A | D | | 0 |
| 8829121 | C | A | A | H | - | A | A | | 0 |
| 8831759 | C | A | A | H | - | C | D | | 0 |
| 8860699 | I | A | A | H | - | A | D | | 0 |
| 9125926 | C | A | A | H | - | A | A | | 0 |
| 9125932 | C | A | A | H | - | C | A | | 0 |
| 9125950 | C | A | A | H | - | A | D | | 0 |
| 9125964 | C | A | A | H | - | C | A | | 0 |
| 9130291 | C | A | A | H | - | A | A | | 0 |
| 9132848 | D | A | A | H | - | C | D | | 0 |
| 9132864 | C | A | A | H | - | A | D | | 0 |
| 9136495 | C | A | A | H | - | A | A | | 0 |
| 9141971 | C | A | B | H | - | C | A | | 0 |
| 9142225 | E | A | A | H | - | A | A | | 0 |
| 9143242 | C | A | A | H | - | A | A | | 0 |
| 9149463 | C | A | A | H | - | A | A | | 0 |
| 9180024 | C | A | A | H | - | A | A | | 0 |
| 9180025 | D | A | A | H | - | A | A | | 0 |
| 9192582 | C | A | A | H | - | C | D | | 0 |
| 9225546 | D | A | A | H | - | C | A | | 0 |
| 9267368 | C | A | A | H | - | A | A | | 0 |
| 9276968 | I | A | A | H | - | C | D | | 0 |
| 9276969 | C | A | A | H | - | A | A | | 0 |
| 9303957 | C | A | A | H | - | A | A | | 0 |
| 9312274 | I | A | A | H | - | C | D | | 0 |
| 9386369 | C | A | - | H | - | A | A | | 0 |
| 9386673 | C | A | B | H | - | C | D | | 0 |
| 9409641 | I | A | A | H | - | B | D | | 0 |
| 9409645 | C | A | A | H | - | B | A | | 0 |
| 9410138 | C | A | A | H | - | A | A | | 0 |
| 9414198 | C | A | A | H | - | A | A | | 0 |
| 9419821 | I | A | - | H | - | A | A | | 0 |
| 9419822 | C | A | A | H | - | A | D | | 0 |
| 9419830 | D | A | A | H | - | A | D | | 0 |
| 9436946 | C | A | A | H | - | A | A | | 0 |
| 9458212 | E | A | A | H | - | A | D | | 0 |
| 9479139 | C | A | A | H | - | A | A | | 0 |
| 9479140 | C | A | A | H | - | A | A | | 0 |
| 9493257 | C | A | A | H | - | A | A | | 0 |
| 9504959 | C | A | A | H | - | A | A | | 0 |
| 9533172 | E | A | A | H | - | A | D | | 0 |
| 9535325 | C | A | B | H | - | C | D | | 0 |
| 9546096 | C | A | A | H | - | A | A | | 0 |
| 9546100 | C | A | B | H | - | A | D | | 0 |

| CASE_ID | BICYCLE_ACCIDENT | MOTORCYCLE_ACCIDENT | TRUCK_ACCIDENT | NOT_PRIVATE_PROPERTY | ALCOHOL_INVOLVED | STWD_VEHTYPE_AT_FAULT |
|---------|------------------|---------------------|----------------|----------------------|------------------|-----------------------|
| 8688096 | | | Y | Y | | F |
| 8709544 | | | | Y | | A |
| 8829121 | | | | Y | | - |
| 8831759 | | | | Y | | A |
| 8860699 | | | | Y | | A |
| 9125926 | | | | Y | | A |
| 9125932 | | | | Y | Y | A |
| 9125950 | | | | Y | | A |
| 9125964 | | | | Y | | - |
| 9130291 | | Y | | Y | | G |
| 9132848 | | | | Y | Y | A |
| 9132864 | | | | Y | | D |
| 9136495 | | | | Y | | A |
| 9141971 | | | | Y | Y | A |
| 9142225 | | Y | | Y | | A |
| 9143242 | | | | Y | | - |
| 9149463 | | | | Y | Y | A |
| 9180024 | | | | Y | | A |
| 9180025 | | | | Y | | A |
| 9192582 | | | | Y | | A |
| 9225546 | | | | Y | | A |
| 9267368 | | | | Y | | A |
| 9276968 | | | | Y | | - |
| 9276969 | | | | Y | | A |
| 9303957 | | | | Y | | A |
| 9312274 | | | | Y | Y | A |
| 9386369 | | | | Y | | A |
| 9386673 | | | | Y | Y | - |
| 9409641 | | | | Y | | D |
| 9409645 | | | | Y | | - |
| 9410138 | | | | Y | | A |
| 9414198 | | | | Y | Y | A |
| 9419821 | | | | Y | | A |
| 9419822 | | | | Y | | A |
| 9419830 | | Y | | Y | | A |
| 9436946 | | Y | | Y | | F |
| 9458212 | | | | Y | | A |
| 9479139 | | Y | | Y | | A |
| 9479140 | | Y | | Y | | F |
| 9493257 | | | | Y | | A |
| 9504959 | | | | Y | | A |
| 9533172 | | | | Y | Y | A |
| 9535325 | | | | Y | | - |
| 9546096 | | | | Y | | B |
| 9546100 | | | | Y | | A |

| CASE_ID | CHP_VEHTYPE_AT_FAULT | COUNT_SEVERE_INJ | COUNT_VISIBLE_INJ | COUNT_COMPLAINT_PAIN | COUNT_PED_KILLED | COUNT_PED_INJURED | COUNT_BICYCLIST_KILLED |
|-----------|----------------------|------------------|-------------------|----------------------|------------------|-------------------|------------------------|
| 8688096 | | 27 | 0 | 0 | 0 | 0 | 0 |
| 8709544 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 8829121 | | | 0 | 0 | 0 | 0 | 0 |
| 8831759 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 8860699 | | 7 | 0 | 0 | 0 | 0 | 0 |
| 9125926 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9125932 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9125950 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9125964 | | | 0 | 0 | 0 | 0 | 0 |
| 9130291 | | 24 | 0 | 0 | 0 | 0 | 0 |
| 9132848 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9132864 | | 22 | 0 | 0 | 0 | 0 | 0 |
| 9136495 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9141971 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9142225 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9143242 | | | 0 | 0 | 0 | 0 | 0 |
| 9149463 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9180024 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9180025 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9192582 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9225546 | | 1 | 0 | 0 | 1 | 0 | 0 |
| 9267368 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9276968 - | | | 0 | 0 | 0 | 0 | 0 |
| 9276969 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9303957 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9312274 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9386369 | | 1 | 0 | 0 | 2 | 0 | 0 |
| 9386673 | | 99 | 0 | 0 | 0 | 0 | 0 |
| 9409641 | | 23 | 0 | 0 | 0 | 0 | 0 |
| 9409645 - | | | 0 | 0 | 0 | 0 | 0 |
| 9410138 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9414198 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9419821 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9419822 | | 1 | 0 | 0 | 1 | 0 | 0 |
| 9419830 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9436946 | | 26 | 0 | 0 | 0 | 0 | 0 |
| 9458212 | | 1 | 0 | 0 | 3 | 0 | 0 |
| 9479139 | | 1 | 0 | 0 | 4 | 0 | 0 |
| 9479140 | | 26 | 0 | 0 | 1 | 0 | 0 |
| 9493257 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9504959 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9533172 | | 1 | 0 | 0 | 0 | 0 | 0 |
| 9535325 | | 99 | 0 | 0 | 0 | 0 | 0 |
| 9546096 | | 8 | 0 | 0 | 0 | 0 | 0 |
| 9546100 | | 1 | 0 | 0 | 0 | 0 | 0 |

| CASE_ID | COUNT_BICYCLIST_INJURED | COUNT_MC_KILLED | COUNT_MC_INJURED | PRIMARY_RAMP | SECONDARY_RAMP | LATITUDE | LONGITUDE |
|---------|-------------------------|-----------------|------------------|--------------|----------------|----------|-----------|
| 8688096 | 0 | 0 | 0 | 0 - | - | | |
| 8709544 | 0 | 0 | 0 | 0 - | - | | |
| 8829121 | 0 | 0 | 0 | 0 - | - | | |
| 8831759 | 0 | 0 | 0 | 0 - | - | | |
| 8860699 | 0 | 0 | 0 | 0 - | - | | |
| 9125926 | 0 | 0 | 0 | 0 - | - | | |
| 9125932 | 0 | 0 | 0 | 0 - | - | 38.46927 | 121.82249 |
| 9125950 | 0 | 0 | 0 | 0 - | - | | |
| 9125964 | 0 | 0 | 0 | 0 - | - | 38.46927 | 121.82246 |
| 9130291 | 0 | 0 | 0 | 0 - | - | | |
| 9132848 | 0 | 0 | 0 | 0 - | - | | |
| 9132864 | 0 | 0 | 0 | 0 - | - | | |
| 9136495 | 0 | 0 | 0 | 0 - | - | 38.46738 | 121.82246 |
| 9141971 | 0 | 0 | 0 | 0 - | - | 38.46738 | 121.82248 |
| 9142225 | 0 | 0 | 0 | 0 - | - | 38.46927 | 121.82246 |
| 9143242 | 0 | 0 | 0 | 0 - | - | 38.46739 | 121.82551 |
| 9149463 | 0 | 0 | 0 | 0 - | - | 38.45902 | 121.82251 |
| 9180024 | 0 | 0 | 0 | 0 - | - | 38.46738 | 121.82246 |
| 9180025 | 0 | 0 | 0 | 0 - | - | 38.46927 | 121.82246 |
| 9192582 | 0 | 0 | 0 | 0 - | - | | |
| 9225546 | 0 | 0 | 0 | 0 - | - | 38.46738 | 121.82246 |
| 9267368 | 0 | 0 | 0 | 0 - | - | | |
| 9276968 | 0 | 0 | 0 | 0 - | - | 38.46739 | 121.82548 |
| 9276969 | 0 | 0 | 0 | 0 - | - | 38.46739 | 121.82548 |
| 9303957 | 0 | 0 | 0 | 0 - | - | 38.46927 | 121.82246 |
| 9312274 | 0 | 0 | 0 | 0 - | - | 38.45902 | 121.82251 |
| 9386369 | 0 | 0 | 0 | 0 - | - | | |
| 9386673 | 0 | 0 | 0 | 0 - | - | | |
| 9409641 | 0 | 0 | 0 | 0 - | - | 38.47185 | 121.82228 |
| 9409645 | 0 | 0 | 0 | 0 - | - | 38.46738 | 121.82246 |
| 9410138 | 0 | 0 | 0 | 0 - | - | 38.46738 | 121.82229 |
| 9414198 | 0 | 0 | 0 | 0 - | - | | |
| 9419821 | 0 | 0 | 0 | 0 - | - | 38.46927 | 121.82246 |
| 9419822 | 0 | 0 | 0 | 0 - | - | | |
| 9419830 | 0 | 0 | 0 | 0 - | - | | |
| 9436946 | 0 | 0 | 0 | 0 - | - | 38.46738 | 121.82246 |
| 9458212 | 0 | 0 | 0 | 0 - | - | 38.46962 | 121.82328 |
| 9479139 | 0 | 0 | 0 | 0 - | - | | |
| 9479140 | 0 | 0 | 0 | 0 - | - | | |
| 9493257 | 0 | 0 | 0 | 0 - | - | 38.46738 | 121.822 |
| 9504959 | 0 | 0 | 0 | 0 - | - | 38.46927 | 121.82246 |
| 9533172 | 0 | 0 | 0 | 0 - | - | 38.45406 | 121.8359 |
| 9535325 | 0 | 0 | 0 | 0 - | - | 38.46739 | 121.82551 |
| 9546096 | 0 | 0 | 0 | 0 - | - | | |
| 9546100 | 0 | 0 | 0 | 0 - | - | | |